

# EBL 21 Double-diode output pentode

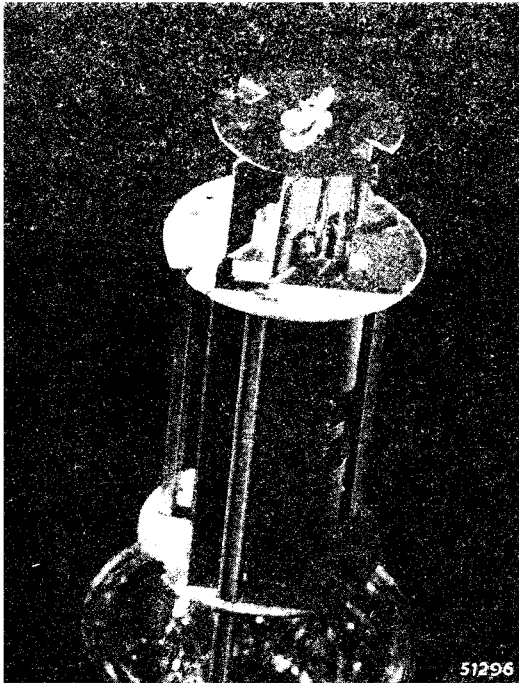


Fig. 1  
Internal assembly of the double diode pentode EBL 21.

a valve of this class when the diode-anode employed for the detection is sufficiently free from ripple to allow of adequate A.F. gain. In the design of the EBL 21 it was made a condition that an A.F. gain factor of 60 between the detector diode and the grid of the output pentode should be obtainable on normal feed by means of a mains-operated heater transformer<sup>1)</sup>. In this way the triode section of the ECH 21, coupled as A.F. amplifier, or the pentode EF 22, may be interposed between the diode and pentode sections of this valve, in the second instance with more or less intensive feedback. A great deal of care has accordingly been paid to the design of the diode section of the valve. Efficient screening and a careful choice of sequence in the electrode connections have resulted in a minimum of ripple voltages at the diode anode  $d_2$  used for detection.

The EBL 21 is also very suitable for Class AB push-pull output

<sup>1)</sup> This figure should be used for guidance only, since a higher gain is possible if greater ripple be permitted. When power is obtained from a vibrator, a gain factor of 15 should be regarded as the limit, since in this case a greater amount of ripple must be expected.

The EBL 21 is a double-diode output pentode. The sensitivity of the pentode system is extremely high; the mutual conductance is 9.5 mA/V. The maximum anode dissipation is 11 W.

Since the dimensions of the electrode system are considerably smaller than those of the earlier EBL 1, the heater current consumed is accordingly lower: at 6.3 V the heater current of the EBL 21 is only 0.8 A, as against 1.18 A in the case of the EBL 1. In many cases it will be possible, in order to increase the A.F. sensitivity of the receiver, to couple an A.F. amplifier between the diode and the pentode of the EBL 21; this is only possible for

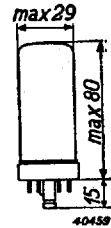


Fig. 2  
Dimensions in mm.

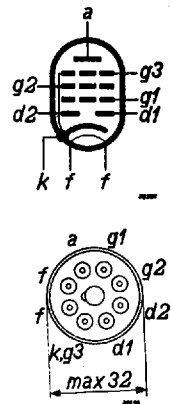


Fig. 3  
Arrangement and connections of the electrodes.

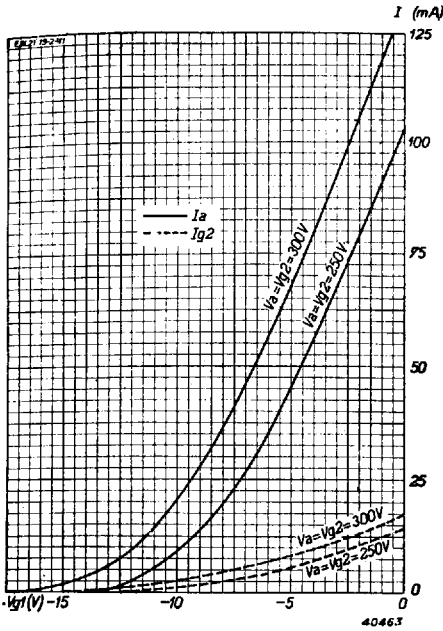


Fig. 4  
Anode and screen current as a function of grid bias at  $V_a = V_{g_2} = 250$  V and  $= 300$  V.

stages. Two of these valves in conjunction with a triode heptode ECH 21 coupled as A.F. amplifier and phase inverter give a very high quality output stage having an output of about 13 W. This is an ideal final stage for very high grade receivers. Moreover, 4 diodes of the EBL 21 are then available for employment, for instance, in a 3 diode circuit. To prevent interaction between the diode and pentode sections, the capacitances between the diode anodes and the anode and grid of the pentode have been suppressed as much as possible (see capacitance values included in the operating data). Technical data of this valve are given below:

**HEATER RATINGS**

Heating: indirect; alternating current; parallel supply.

Heater voltage. . . . .  $V_f = 6.3$  V

Heater current. . . . .  $I_f = 0.8$  A

**CAPACITANCES**

a) Pentode section

$C_{ag1} < 1.4$  pF

b) Diode sections

$C_{d1k} = 1.8$  pF

$C_{d2k} = 2.0$  pF

$C_{d1d2} < 0.15$  pF

c) Between diode and pentode

$C_{d1g1} < 0.1$  pF       $C_{d1a} < 0.06$  pF

$C_{d2g1} < 0.05$  pF       $C_{d2a} < 0.02$  pF

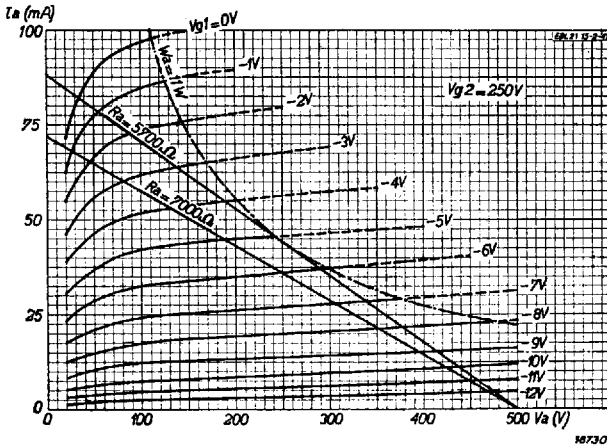


Fig. 5  
Anode current as a function of anode voltage at  $V_{g_2} = 250$  V, with grid bias as parameter. In the figure the load lines in respect of  $R_a = 5700$  Ohms (11 W operation) and  $R_a = 7000$  Ohms (9 W operation) are also shown.

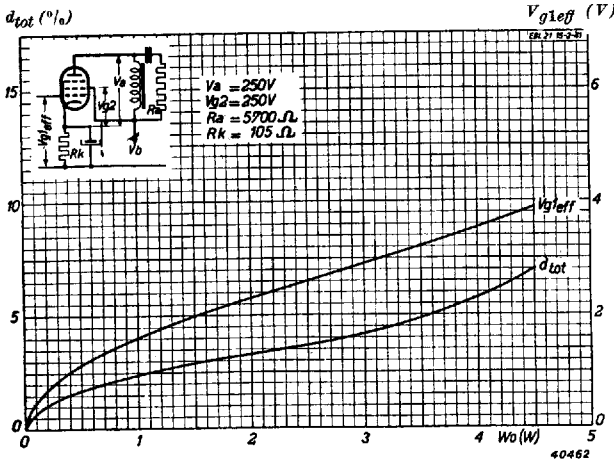


Fig. 6  
 Total distortion and required alternating grid voltage as a function of output power at  $V_a = V_{g2} = 250$  V and  $R_a = 5700$  Ohms (11 W operation).

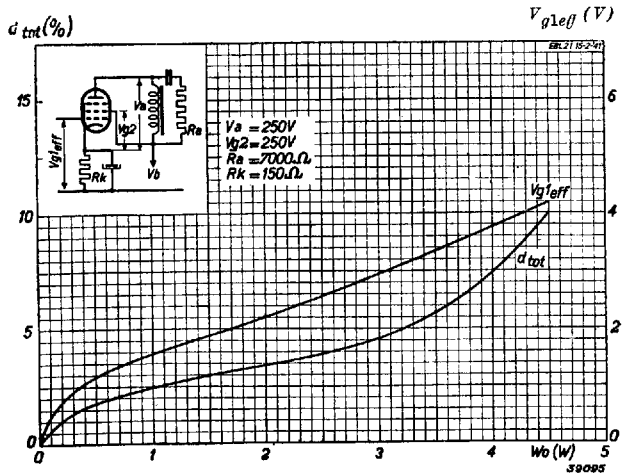


Fig. 7  
 Total distortion and required alternating grid voltage as a function of output power at  $V_a = V_{g2} = 250$  V and  $R_a = 7000$  Ohms (9 W operation).

**OPERATING DATA FOR THE PENTODE SECTION employed as single output valve.**

Anode voltage . . . . .	$V_a = 250$ V	250 V
Screen grid voltage . . . . .	$V_{g2} = 275$ V	250 V
Cathode resistance . . . . .	$R_k = 125$ Ohms	150 Ohms
Grid bias . . . . .	$V_{g1} = -6.2$ V	-6 V
Anode current . . . . .	$I_a = 44$ mA	36 mA
Screen grid current . . . . .	$I_{g2} = 5.8$ mA	4.5 mA
Mutual conductance . . . . .	$S = 9.5$ mA/V	9.0 mA/V
Internal resistance . . . . .	$R_i = 50,000$ Ohms	50,000 Ohms
Optimum load . . . . .	$R_a = 5700$ Ohms	7000 Ohms
Output power at max. modulation . . . . .	$W_o = 5.5$ W	4.5 W
Total distortion . . . . .	$d_{tot} = 10$ %	10 %
Required alternating grid voltage for max. modulation . . . . .	$V_{g1eff} = 4.5$ V	4.2 V
Sensitivity ( $W_o = 50$ mW) . . . . .	$V_{g1eff} = 0.30$ V	0.35 V
Gain factor: screen grid — grid 1 . . . . .	$\mu_{g2g1} = 23$	23

**OPERATING DATA for Class AB push-pull output (2 valves)**

Anode voltage . . . . .	$V_a = 300$ V
Screen grid voltage . . . . .	$V_{g2} = 300$ V
Cathode resistance . . . . .	$R_k = 130$ Ohms
Optimum load . . . . .	$R_{aa'} = 9000$ Ohms
Standing anode current . . . . .	$I_{a0} = 2 \times 30$ mA
Anode current at max. modulation . . . . .	$I_{amax} = 2 \times 36$ mA
Standing screen grid current . . . . .	$I_{g20} = 2 \times 3.8$ mA
Screen grid current at max. modulation . . . . .	$I_{g2max} = 2 \times 6.5$ mA
Max. output power . . . . .	$W_{omax} = 13.2$ W
Total distortion at max. output power . . . . .	$d_{tot} = 1.8$ %
Required alternating grid voltage, per grid . . . . .	$V_{g1eff} = 7.0$ V
Sensitivity ( $W_o = 50$ mA) . . . . .	$V_{g1eff} = 0.3$ V

**MAXIMUM RATINGS for the pentode section**

Anode voltage, in cold condition . . . . .	$V_{a0} = \text{max. } 550$ V
Anode voltage . . . . .	$V_a = \text{max. } 300$ V
Anode dissipation . . . . .	$W_a = \text{max. } 11$ W
Screen grid voltage, in cold condition . . . . .	$V_{g20} = \text{max. } 550$ V
Screen grid voltage . . . . .	$V_{g2} = \text{max. } 300$ V
Screen grid dissipation, unmodulated valve ( $V_{g1eff} = 0$ V) . . . . .	$W_{g2} = \text{max. } 1.7$ W
Screen grid dissipation at max. modulation ( $W_o = \text{max.}$ ) . . . . .	$W_{g2} = \text{max. } 3.5$ W
Cathode current . . . . .	$I_k = \text{max. } 60$ mA
Grid current commences at ( $I_{g1} = +0.3 \mu\text{A}$ ) . . . . .	$V_{g1} = \text{max. } -1.3$ V
Max. external resistance between control grid and cathode . . . . .	$R_{g1k} = \text{max. } 1$ M Ohm
Max. external resistance between heater and cathode . . . . .	$R_{fk} = \text{max. } 5000$ Ohms
Max. potential between heater and cathode . . . . .	$V_{fk} = \text{max. } 50$ V

**MAXIMUM ratings for the diode section**

Peak voltage on diode 1 . . . . .	$V_{d1} = \text{max. } 200$ V
Peak voltage on diode 2 . . . . .	$V_{d2} = \text{max. } 200$ V
Max. direct current through resistor of diode 1 . . . . .	$I_{d1} = \text{max. } 0.8$ mA
Max. direct current through resistor of diode 2 . . . . .	$I_{d2} = \text{max. } 0.8$ mA
Diode current commences ( $I_{d1} = +0.3 \mu\text{A}$ ) . . . . .	$V_{d1} = \text{max. } -1.3$ V
Diode current commences ( $I_{d2} = +0.3 \mu\text{A}$ ) . . . . .	$V_{d2} = \text{max. } -1.3$ V

APPLICATIONS

The following points should be borne in mind in the applications of this valve.

(I) Grid bias should be obtained exclusively by use of a cathode resistance. If required, so-called semi-automatic bias may be applied, but only when the cathode current of this valve exceeds 50 % of the total current flowing through the resistance used to provide the bias: the grid leak should then be correspondingly lower in value than the indicated maximum value. (II) Leads to the electrodes should be kept as short as possible. (III) To avoid parasitic oscillation, which, due to the high mutual conductance, very quickly sets in, a damping resistance of, say, 1000 Ohms may be included in the control grid lead; this resistance is to be mounted as closely as possible to the electrode concerned and must not be bypassed by a condenser.

For use of the EBL 21 with feedback, in conjunction with the ECH 21, see also p. 17, in connection with the ECH 21.

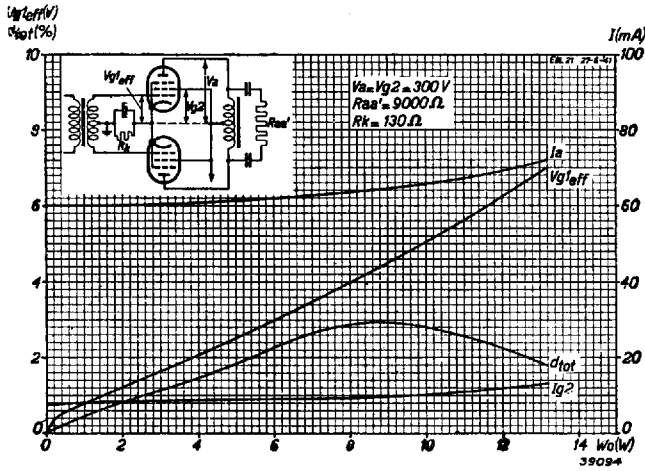


Fig. 8  
Total anode and screen current, total distortion and required alternating grid voltage (per grid) as a function of output power of two valves EBL 21 in a class AB push-pull circuit, at  $V_a = V_{g2} = 300 V$ .