

# COMPONENTS AND MATERIALS

# Part 3

# January 1969

FM tuners	A	
Coils and resonators	В	
Audio and mains transformers	С	
Loudspeakers	D	
Electronic organ assemblies		
Television tuners	F	
Components for black and white television	G	
Components for colour television	Н	
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## FOR "FERRITES FOR RADIO, AUDIO AND TELEVISION" SEE RELEVANT SECTION OF PART 4

Comprehensive contents list at the back

## DATA HANDBOOK SYSTEM

To provide you with a comprehensive source of information on electronic components, subassemblies and materials, our Data Handbook System is made up of three series of handbooks, each comprising several parts. The three series, identified by the colours noted, are:

**ELECTRON TUBES** (9 parts)

BLUE

GREEN

## SEMICONDUCTORS AND INTEGRATED CIRCUITS (5 parts) RED

### **COMPONENTS AND MATERIALS** (5 parts)

The several parts contain all pertinent data available at the time of publication, and each is revised and reissued annually; the contents of each series are summarized on the following pages.

We have made every effort to ensure that each series is as accurate, comprehensive and up-to-date as possible, and we hope you will find it to be a valuable source of reference. You will understand that we can not guarantee that all products listed in any one edition of the handbook will remain available, or that their specifications will not be changed, before the next edition is published. If you need confirmation that the published data about any of our products are the latest available, may we ask that you contact our representative. He is at your service and will be glad to answer your inquiries.

## ELECTRON TUBES (BLUE SERIES)

This series consists of the following parts, issued on the dates indicated.

## Part 1

Transmitting tubes (Tetrodes, Pentodes)

## Part 2

Tubes for microwave equipment

## Part 3

Special Quality tubes

### Part 4

Receiving tubes

## Part 5

Cathode-ray tubes Photo tubes Camera tubes

### Part 6

Photomultiplier tubes Radiation counter tubes Scintillators

## Part 7

Voltage stabilizing and reference tubes Counter, selector, and indicator tubes Trigger tubes Switching diodes

## Part 9

Transmitting tubes (Triodes) Tubes for R.F. heating (Triodes) December 1968

Associated accessories

February 1969

#### February 1968

Miscellaneous devices

## March 1968

T.V. picture tubes

April 1968

Photoconductive devices Associated accessories

## July 1968

Semiconductor radiation detectors Miscellaneous nuclear devices

## May 1968

Thyratrons Ignitrons Industrial rectifying tubes High-voltage rectifying tubes

## December 1968

Associated accessories

## SEMICONDUCTORS AND INTEGRATED CIRCUITS (RED SERIES)

This series consists of the following parts, issued on the dates indicated.

## Part 1

General section Signal diodes Variable capacitance diodes Voltage regulator diodes

## Part 2

General section Germanium transistors

## Part 3-4

General section Silicon transistors Accessories and heatsinks

## Part 5

General section Digital integrated circuits Linear integrated circuits

## September 1968

Rectifier diodes Thyristors Rectifier stacks Accessories and heatsinks

## October 1968

Photo devices Accessories and heatsinks

## November 1968

January 1969

## COMPONENTS AND MATERIALS (GREEN SERIES)

This series consists of the following parts, issued on the dates indicated.

## Part 1 Circuit Blocks, Input/Output Devices

September 1968

November 1968

Circuit blocks: 100 kHz Series 1-Series 20-Series 40-Series Norbits (60-Series) Circuit blocks for ferrite core memory drive Input/output devices Accessories for circuit blocks: Power supplies Mounting chassis Printed-wiring boards

## Part 2 Resistors, Capacitors

Fixed resistors Variable resistors Non-linear resistors Ceramic capacitors Polycarbonate, paper, mica, polystyrene capacitors Electrolytic capacitors Variable capacitors

## Part 3 Radio, Audio, Television

FM tuners Coils and resonators Audio and mains transformers Loudspeakers Electronic organ assemblies

## January 1969 Television tuners Components for black and white television

Components for colour television Deflection assemblies for camera tubes

## Part 4 Magnetic Materials, White Ceramics

March 1968

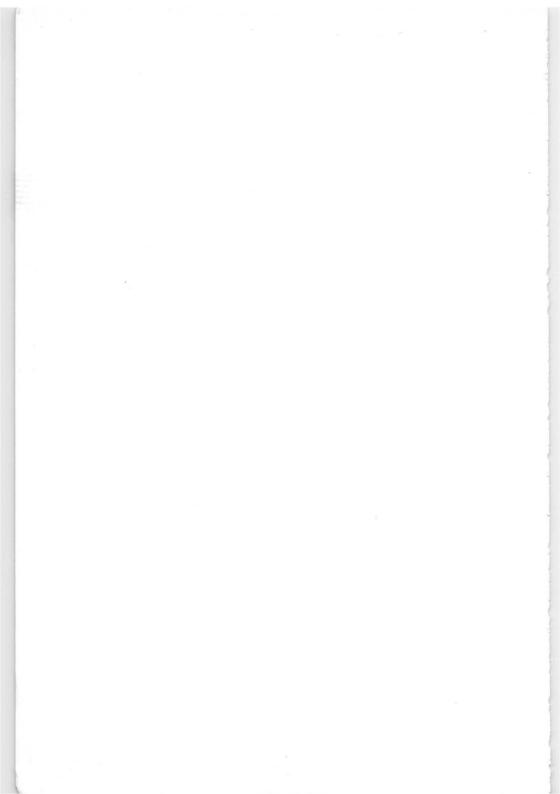
Ferrites for radio, audio and television Ferroxcube potcores Microchokes Ferroxcube transformer cores Piezoxide Insulating and dielectric materials Permanent magnet materials

## Part 5 Memory Products, Magnetic Heads, Quartz Crystals, June 1968 Microwave Devices, Variable Transformers, Electro-mechanical Components

Ferrite memory cores Matrix planes, matrix stacks Complete memories Magnetic heads Quartz crystal units, crystal filters Isolators, circulators Variable mains transformers Electro-mechanical components This Handbook does not give information on delivery or terms.

The information given in this Handbook does not imply a licence under any patent.

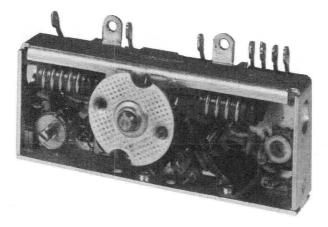
# FM tuners





AP2151/00

## F.M. TUNER



F.M. tuner for European band; with automatic frequency control Equipped with silicon transistors.

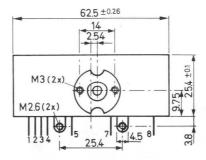
#### APPLICATION

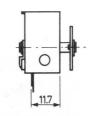
For use in radio sets for reception of F.M. signals in the European frequency band (not for portable and car radios as no supply voltage stabilisation is present).

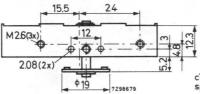
## F.M. TUNER

### MECHANICAL DATA

Dimensions in mm







clockwise rotation of the spindle increases the frequency

ELECTRICAL DATA

Supply voltage

Frequency range

Tolerance on scale calibration

Padding deviation

Total gain 1)

I.F. frequency

I.F. bandwidth  $(3 \text{ dB})^1$ )

Maximum frequency drift

Radiation measured at a distance of 3 m (I.E.C.)

fundamental wave

second harmonic

9 V<sub>dc</sub> 87-104 MHz < 350 kHz < 0.75 MHz 4.5 x 10.7 MHz The oscillator frequency is higher than the signal frequency 210 kHz 10 kHz/deg C

 $1000 \,\mu V/m$ 

 $300 \,\mu V/m$ 

1) Measured with secondary i.f. filter 3122 108 22850 (see Gain Measurement).

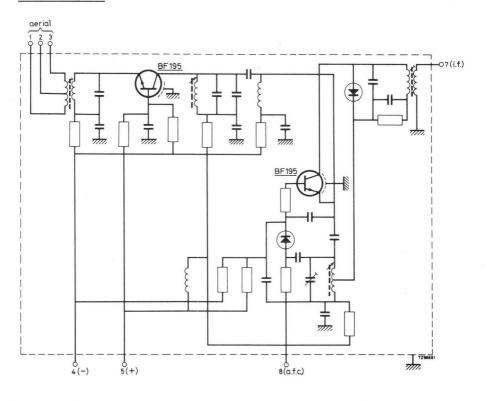
3122 108 68870

AP2151/00

Scale calibration

angle of rotation (degrees)	frequency (MHz)	angle of rotation (degrees)	frequency (MHz)
0	86.7	238	96
9.5	87.5	261.5	97
38.5	88	285	98
65.5	89	309	99
91.5	90	333.5	100
116.5	91	358.5	101
141	92	360+ 24.5	102
165.5	93	360+ 52	103
190	94	360+ 84	104
214	95	360+126.5	105

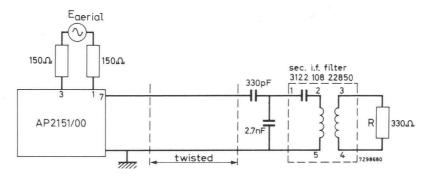
Circuit diagram



A5

## AP2151/00

GAIN MEASUREMENT

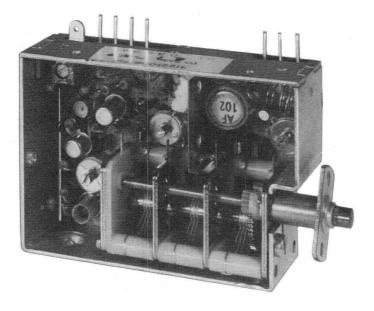


The aerial impedance of 300  $\Omega$  is connected symmetrically. The gain =  $\frac{i.f. \text{ voltage across } R (= 330 \Omega)}{\text{aerial } e.m.f.}$ 

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3122 108 69400 3122 108 81760 3122 108 68730

## F.M. TUNERS



F.M. tuner AP2152/00 AP2152/01 AP2152/02

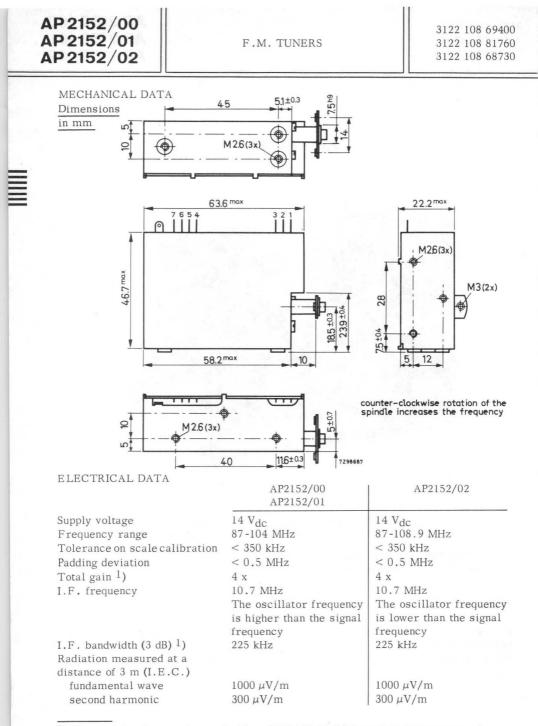
for European band; with soldering lugs for European band; with pins for printed-wiring for American band; with soldering lugs

Automatic frequency control Equipped with germanium transistors

## APPLICATION

For use in Hi-Fi radio sets (not for portable radios as no supply voltage stabilisation is present).

The advantage of this tuner is the excellent big signal handling.



1) Measured with secondary i.f. filter 3122 108 22850 (see Gain Measurement).

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August 1968

3122 108 69400 3122 108 81760 3122 108 68730

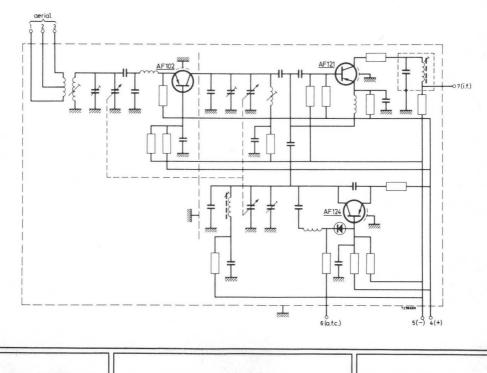
## F.M. TUNERS

## AP 2152/00 AP 2152/01 AP 2152/02

Scale calibration

angle of rotation (degrees)		frequency	angle of rotation (degrees)		frequency
AP2152/00 AP2152/01	AP2152/02	(MHz)	AP2152/00 AP2152/01	AP2152/02	(MHz)
0	0	87	311.5	279.5	98
26.5	20	87.5	341	302.5	99
41	34.5	88	360 + 11	327	100
68	61.5	89	360 + 40	350	101
94	88	90	360 + 70.5	360 + 13	102
121	112.5	91	360 + 98.5	360 + 35	103
147.5	137.5	92	360+127	360 + 57	104
174.5	161.5	93	360+159	360 + 78.5	105
202.5	185.5	94	-72	360 + 98.5	106
230	209.5	95		360 + 118	107
257	232.5	96	the second second	360+138.5	108
284	256	97	- ****	360 + 158.4	108.9

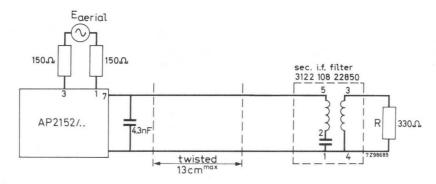
## Circuit diagram



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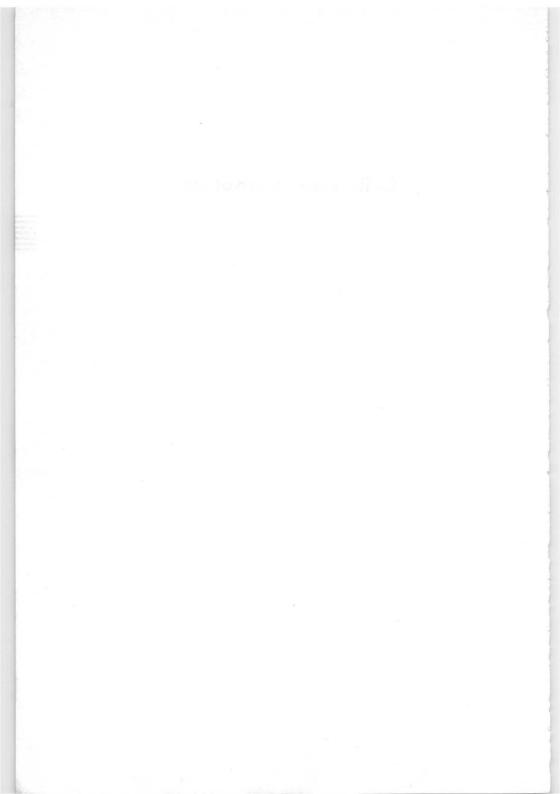


GAIN MEASUREMENT



The aerial impedance of 300  $\Omega$  is connected symmetrically. The gain =  $\frac{i.f. \text{ voltage across R (= 330 }\Omega)}{\text{aerial e.m.f.}}$ 

# **Coils and resonators**



## AP 1051

# COILS

## for transistorised radio sets





RZ 16012-1

intermediate frequency AM FM quality factor Q inductance adjustment range

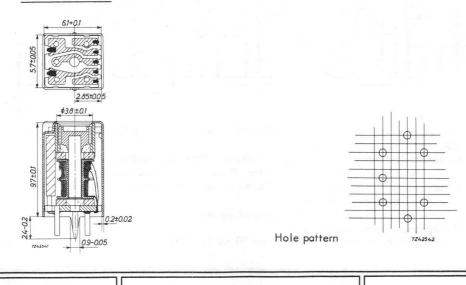
temperature coefficient

450 - 470 kHz 10.7 MHz 100 - 140 ± 10% to ± 15% 100.10<sup>-6</sup> - 400.10<sup>-6</sup>/deg C

These coils are designed for mounting in printed-wiring boards with an  $\epsilon$ -grid ( $\epsilon = \frac{e}{4} = 0.635 \text{ mm}$ ).

They can be supplied with a built-in capacitor (capacitance values 47, 82, 100 or 150  $\ensuremath{\mathsf{pF}}\xspace$ ).

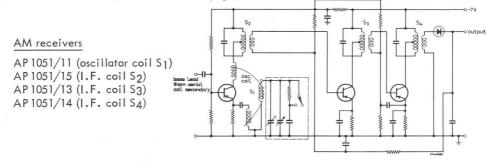
#### Dimensions in mm



AP 1051

COILS for transistorised radio sets

TYPES (for catalog numbers see last page)



The following performance can be obtained with these coils in the above-given circuit, measured at a supply voltage of -7V.

- a. Sensitivity: input 2µV ±6dB at 1 MHz for 50mV audio output. The input is modulated 30% at 400 Hz. The output is measured across a 5 kΩ load.
- b. Bandwidth: 5.1 kHz ± 500 Hz at 6 dB measured under similar conditions with a centre frequency of 470 kHz.
- c. Attenuation:  $26 dB \pm 3 dB at$  9 kHz from centre frequency.
- d. Consumption: approx. 3.3 mA

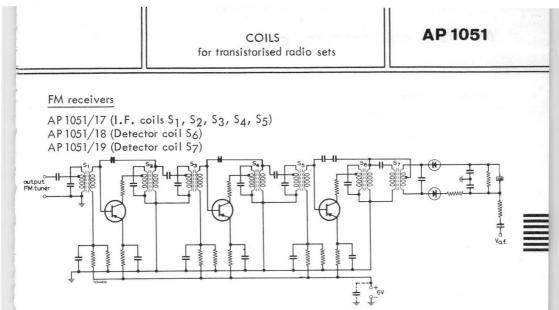
AP 1051/20 (I.F. coil S2) AP 1051/21 (I.F. coil S3 and S5) AP 1051/23 (I.F. coil S4) (S<sub>1</sub> = oscillator coil) AP 1051/23 (I.F. coil S<sub>6</sub>)  $\int_{1}^{s_1} \int_{1}^{s_2} \int_{1}^{s_3} \int_{1}^{s_4} \int_{1}^{s_5} \int_{1}^{s_5} \int_{1}^{s_6} \int_{1}^{s_6$ 

The following performance can be obtained with these coils in the above-given circuit, measured at a supply voltage of 6V.

a. Sensitivity: input 1.6 µV ±6 dB at 1 MHz for 10 mV audio output.

The input is modulated 30% at 400 Hz. The output is measured unloaded.

- b. Bandwidth: 4.8kHz ±500 Hz at 6dB. Measured under similar conditions with a centre frequency of 460 kHz.
- c. Attenuation: 77 x at 9 kHz from centre frequency.
- d. Consumption: approx. 3.3 mA
- e. Max. input: on base of first transistor 20 mV (1 MHz).



The following performance can be obtained with these coils in the above-given circuit, measured at a supply voltage of 6V.

- a. Sensitivity: input 44  $\mu V$  for 10 mV audio output. The output is measured unloaded.  $\Delta$  f = 15 kHz.
- b. Bandwidth: 160 kHz at 6 dB.
- c. Attenuation: 450 x at 300 kHz from centre frequency.
- d. Consumption: approx. 3.3 mA

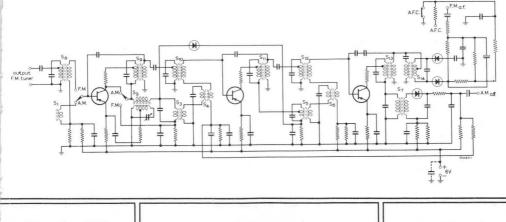
## AM/FM receivers

AP 1051/20 (I.F. coil S<sub>3</sub>) AP 1051/21 (I.F. coil S<sub>4</sub>, S<sub>6</sub>) AP 1051/22 (I.F. coil S<sub>5</sub>) AP 1051/23 (I.F. coil S<sub>7</sub>)

AP 1051/17 (I.F. coils S8, S9, S10, S11, S12) AP 1051/18 (Detector coil S13) AP 1051/19 (Detector coil S14)

 $(S_1 = aerial coil a.m.; S_2 = oscillator coil a.m.)$ 

For performance see above.



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AP 1051

COILS for transistorised radio sets

CATALOG NUMBERS (for ordering)

type	catalog number
AP1051/11	3122 107 30940
AP1051/13	3122 107 30960
AP1051/14	3122 107 30970
AP1051/15	3122 107 30980
AP1051/17	3122 108 20570
AP1051/18	3122 108 25550
AP1051/19	3122 108 25560
AP1051/20	3122 994 93890
AP1051/21	3122 994 93900
AP1051/22	3122 994 93910
AP1051/23	3122 994 93920

2422 540 00...

# PIEZOELECTRIC CERAMIC RESONATORS for a.m. radio sets



RZ 24572-1

Resonant frequency Quality factor Ambient temperature range 452, 455, 460, 468, 470 and 480 kHz > 800  $-25\ {\rm to}+85\ ^{\rm OC}$ 

## GENERAL

The piezoelectric effect of lead zirconate titanate ceramic material makes it possible to achieve frequency selective elements with electrical characteristics far better than coils and far more economical than quartz crystals.

This series of ceramic resonators is intended to be used in intermediate stages of a.m. radio receivers. Compared with coils the resonators offer several advantages:

- no installation alignment

- high selectivity

- miniature size

- no shielding (due to the absence of magnetic fields)
- low price.

#### CONSTRUCTION

A disc of extremely pure and stable piezoelectric ceramic material is provided with two gold electrodes. The disc is clamped between two gold-plated springs with lock-fitting printed-wiring terminals. This assembly is encapsulated in an insulating casing.

For each specific frequency between 452 and 480 kHz two versions are available:

- for printed-wiring boards with holes of 1.3 mm (Fig.1)

- for printed-wiring boards with holes of 0.8 mm (Fig.2).



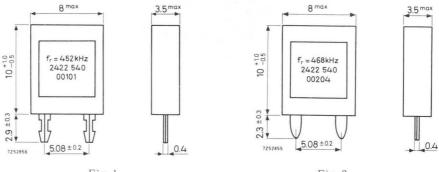


Fig.1

Fig.2

### Marking

The resonators are marked with the resonant frequency (f $_{\mbox{r}})$  and the catalogue number.

2422 540 00...

#### PHYSICAL BEHAVIOUR

The mechanical resonance of the ceramic disc causes the frequency selectivity. Due to the piezoelectricity this mechanical vibration can be described with the equivalent circuit of Fig.3.

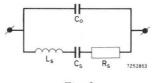


Fig.3

This circuit is valid over a very wide frequency range.

A typical impedance curve, in which impedance is plotted against frequency is shown in Fig.4.

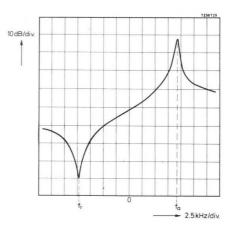


Fig.4.

 $f_r$  = resonant frequency = 452 kHz

- f<sub>0</sub> = frequency at 0-point of horizontal
   scale = 462 kHz
- $f_a$  = anti-resonant frequency = 470 kHz

The impedance curve can be measured with the circuit shown in Fig.5.

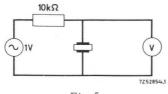


Fig.5

At resonant frequency 100  $V_{\rm TMS}$  should be considered as maximum a.c. voltage.

To calculate the elements of the equivalent circuit (Fig.3) measuring of the following parameters is sufficient:

- resonant frequency fr
- impedance at resonant frequency R<sub>s</sub>
- anti-resonant frequency fa
- capacitance at a frequency far below resonant frequency (1 kHz) C =  $C_0 + C_s$ .

The elements of the circuit can be calculated with the formulae:

$$f_{r} = \frac{1}{2\pi \sqrt{L_{s} C_{s}}}$$
$$f_{a} = \frac{1}{2\pi \sqrt{L_{s} \cdot \frac{C_{s} C_{o}}{C_{s} + C_{o}}}}$$

TECHNICAL PERFORMANCE (see also Fig.3)

Resonant frequency (fr)

452, 455, 460, 468, 470 or 480 kHz

Tolerance on resonant frequency (incl. ageing over a period of 10 years)

Quality factor (Q = 
$$\frac{2\pi f_r L_s}{R_s}$$
)

Inductance (Ls)

Capacitance ( $C = C_0 + C_s$ ), measured at 1 kHz

Maximum permissible a.c. voltage at resonant frequency

Maximum d.c. voltage

Ambient temperature range

Temperature coefficient of fr

Solderability

> 800 (typical 1000)  $8.5 \text{ mH} \pm 10\%$ 

190 pF + 10%

100 mVrms

30 V

+ 1 kHz

-25 to +85 °C

 $< 60.10^{-6}/\text{deg C}$ 

250 °C, max. soldering time 5 s

## AVAILABLE VERSIONS

	f <sub>r</sub> (kHz)	catalogue number			
		version for printed- wiring boards with holes of 1.3 mm	version for printed- wiring boards with holes of 0.8 mm		
	452	2422 540 00101	2422 540 00201		
	455	102	202		
	460	103	203		
	468	104	204		
	470	105	205		
	480	106	206		

#### APPLICATION INFORMATION

#### General

The ceramic resonators  $2422\ 540\ 00\ldots$  are characterised by a high quality factor (which results in a high selectivity and low losses) a well-defined temperature behaviour, and a high stability.

The mechanical resonance responsible for these good properties also has some drawbacks, however, mainly regarding parasitic resonance effects. Although being designed to effectively suppress the harmonics of the fundamental radial vibration, in the 3 to 6 MHz frequency range the resonators will behave as thickness vibrators with inherent resonant frequencies. Therefore measures must be taken to suppress these parasitic effects.

It should be remembered that connecting a low impedance in parallel or a high one in series with the resonator is likely to affect the low impedance at the resonant frequency, as well as the high impedance at other frequencies (also when these frequencies are in the immediate neighbourhood of the resonant frequency), which is essential for the resonator's high Q factor.

#### Filters

The application to be described here is in intermediate frequency bandpass filters for entertainment and communication a.m. radio receivers. Here the resonators are used as coupling elements in a configuration where tuned LC circuits provide sufficient suppression of parasitic signals, whilst the resonators are responsible for high selectivity and low losses in the passband. The presence of the low-loss resonators allow the whole selectivity to be concentrated in a block preceding the i.f. amplifier. This lumped selectivity, being a feature in manufacturing conventional radio receivers, is a must when integrated circuits are used in the i.f. part. In the following sections three filters are shown of increasing quality. These filters **are given as examples only**. For specific requirements on selectivity and impedance levels more application assistance can be given on request.

2422 540 00...

## Second order hybrid bandpass filter

This filter can serve as complete selectivity unit in simple radio receivers or replace double tuned LC sections in more complicated receivers. The ceramic resonator is used as coupling element between a tuned LC circuit and the first i.f. transistor. The capacitor  $\rm C_n$  is a neutralising capacitor which compensates the asymmetry of the bandpass curve caused by the parallel resonance of the resonator.

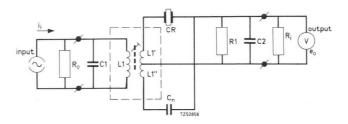


Fig.6. Circuit diagram of a second order hybrid bandpass filter

Parts list:

 $R_{\rm O}$  = output impedance of the mixer/oscillator transistor BF195 (typ. 250 k $\Omega$  at 1 mA)

- $R_i$  = input impedance of the i.f. transistor BF194 (typ. 3 k $\Omega$  at 1 mA)
- $R_1 = 470 \Omega$

 $C_1 = 3000 \text{ pF}$  $C_2 = 3300 \text{ pF}$ 

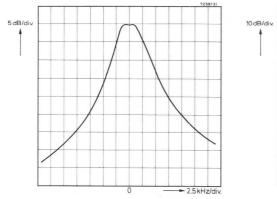
 $C_n = 180 \, pF$ 

 $\begin{array}{ll} L_1 &= 40 \; \mu H \\ V_{L1}'/V_{L1} &= V_{L1}''/V_{L1} = 0.115 \\ \text{Coupling factor } k &= 1 \; \text{approx.} \\ \text{Quality factor } Q_0 \; \text{of tuned circuit = 130; } Q_0 \; (\text{resonator}) = 1000 \; \text{approx.} \end{array}$ 

CR = ceramic resonator 2422 540 00...

Characteristics:

 $B_{3dB}$  = 4.5 kHz Selectivity (<u>+</u> 9 kHz) = 26 dB Centre frequency (f<sub>c</sub>) = 452 kHz Transfer impedance (Z<sub>T</sub>) = 700  $\Omega$  Frequency characteristics (centre frequency  $f_c = 452 \text{ kHz}$ ):



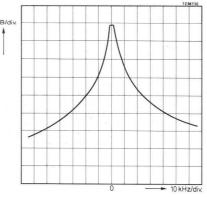


Fig.7



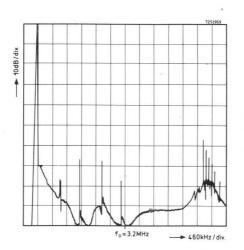


Fig.9

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## Third order hybrid bandpass filter

A triple filter has been designed for more sophisticated radio receivers. It consists of two LC circuits intercoupled with a ceramic resonator. The selectivity of this filter is about 10 dB better than that of the second order filter. Resistor R<sub>1</sub> provides the additional damping required for a symmetric bandpass curve.

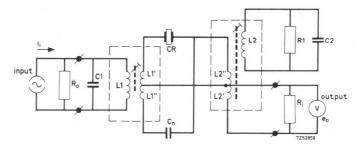


Fig.10. Circuit diagram of a third order hybrid bandpass filter

Parts list:

 $R_{0}$  = output impedance of the mixer/oscillator transistor BF195 (typ. 250 k $\Omega$  at 1 mA)

 $R_i$  = input impedance of the i.f. transistor BF194 (typ. 3 k $\Omega$  at 1 mA)

 $R_1 = 82 k\Omega$ 

 $C_1 = 3000 \text{ pF}$  $C_2 = 3000 \text{ pF}$  $C_n = 270 \text{ pF}$ 

 $\begin{array}{l} L_1 = L_2 = 40 \; \mu H \\ V_{L1} ' \! / V_{L1} = V_{L2} ' \! / V_{L2} = 0.115 \\ V_{L1} ' \! / V_{L1} = V_{L2} ' \! / V_{L2} = 0.077 \end{array}$ 

Quality factor  $Q_0$  of tuned circuits (excluding  $R_1$ )=130;  $Q_0$  (resonator)=1000 approx. CR = ceramic resonator 2422 540 00...

Characteristics:

 $B_{3dB}$  = 4.5 kHz Selectivity (<u>+</u> 9 kHz) = 36 dB Transfer impedance (Z<sub>T</sub>) = 500  $\Omega$ 

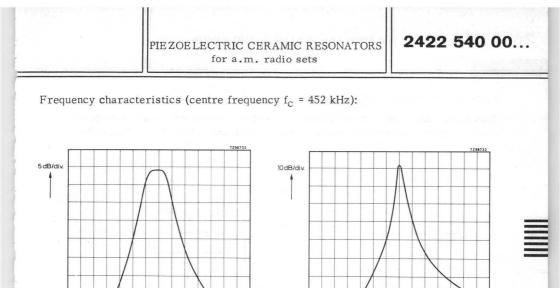
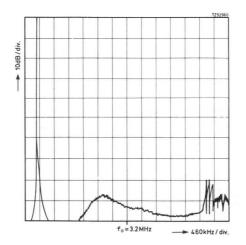




Fig.12

10kHz/div.



- 2.5 kHz/div.

Fig.13

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B15

2422 540 00...

Fifth order hybrid bandpass filter

This filter can provide the selectivity of a communication or a high-class entertainment receiver. Three resonators in series are intercoupling two LC circuits.

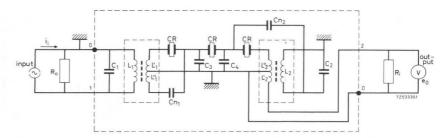


Fig.14. Circuit diagram of a fifth order hybrid bandpass filter

Parts list:

 $R_{0} = 300 \text{ k}\Omega$   $R_{i} = 1200 \Omega$   $C_{1} = C_{2} = 1000 \text{ pF}$   $C_{3} = C_{4} = 1000 \text{ pF}$   $L_{1} = L_{2} = 122 \mu\text{H}$   $\frac{V_{L1'}}{V_{L1}} = \frac{V_{L2'}}{V_{L2}} = 0.097$   $\frac{V_{L1''}}{V_{L1}} = \frac{V_{L2''}}{V_{L2}} = 0.129$   $Quality \text{ factor } \Omega_{0} \text{ of tuned}$ 

Quality factor  $\mathrm{Q}_{\mathrm{O}}$  of tuned circuits = 50 CR = ceramic resonator

Characteristics:

 $\begin{array}{l} B_{6dB} \mbox{ = 7.5 kHz} \\ \mbox{Selectivity ($\pm15 kHz$)$ <math display="inline">\geq 60 \mbox{ dB} \\ \mbox{Transfer impedance ($Z_T$) = 650 $\Omega$} \end{array}$ 

PIEZOELECTRIC CERAMIC RESONATORS for a.m. radio sets

Frequency characteristics (centre frequency  $f_c = 455 \text{ kHz}$ ):

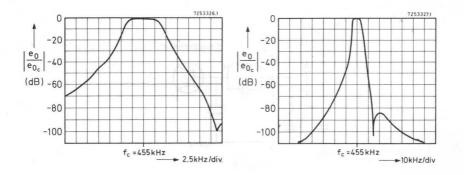


Fig.15

Fig.16

2422 540 00...

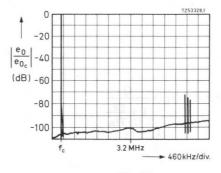
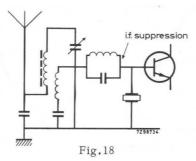


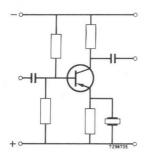
Fig.17

### Aerial filter

A ceramic resonator in the aerial circuit can suppress the i.f. frequency about 32 dB. The resonator decouples the base of the mixer-transistor at the i.f. frequency. This application is not recommended for short-wave receivers due to the thickness resonances of the resonator.



Emitter bypassing



At the resonant frequency and in the neighbourhood of this frequency the ceramic resonator diminishes the feedback effect of the emitter resistor

Fig.19 Loaded quality of the resonator =  $Q_L = \frac{Q}{1 + \frac{y_e}{y_{fe}}}$ 

$$B_{3dB} = \frac{I_0}{Q} \left( 1 + \frac{y_e}{y_{fe}} \right)$$

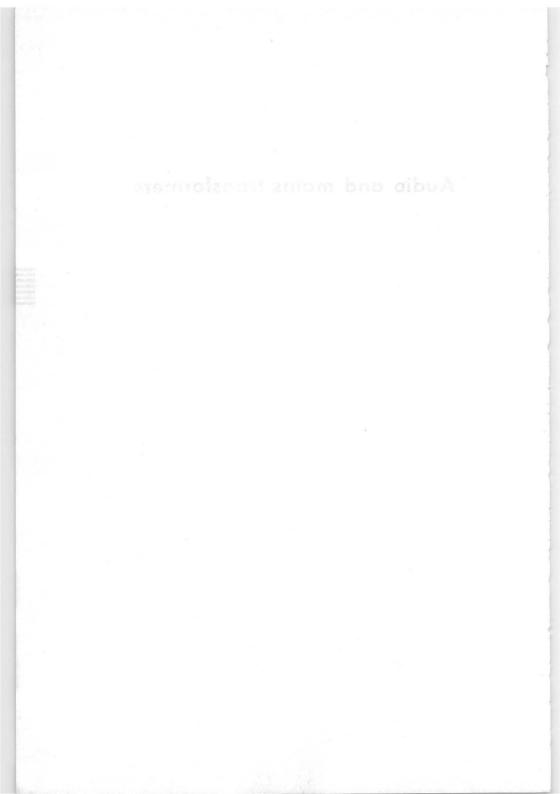
in which:

- $f_0 = resonant$  frequency of the resonator
- Q = quality factor of the resonator
- ye = admittance of the emitter circuit (resonator parallel to resistor) at resonant frequency
- $y_{fe}$  = forward transfer admittance of the transistor.

September 1968

**B18** 

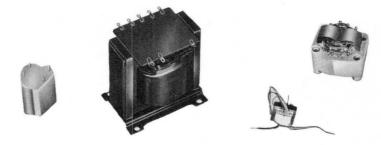




GENERAL
---------

# AUDIO TRANSFORMERS

# INTRODUCTION



C3/66

The range of audio transformers comprises a number of carefully designed items in various sizes for tube and transistor circuits. They show the following features:

- High efficiency

Thanks to a special manufacturing technique, the efficiency is high, even in the case of the smallest types.

- Sturdy construction

In order to obtain a very stable construction and a superior copper-space factor, the coils - with a few exceptions - are compressed after winding.

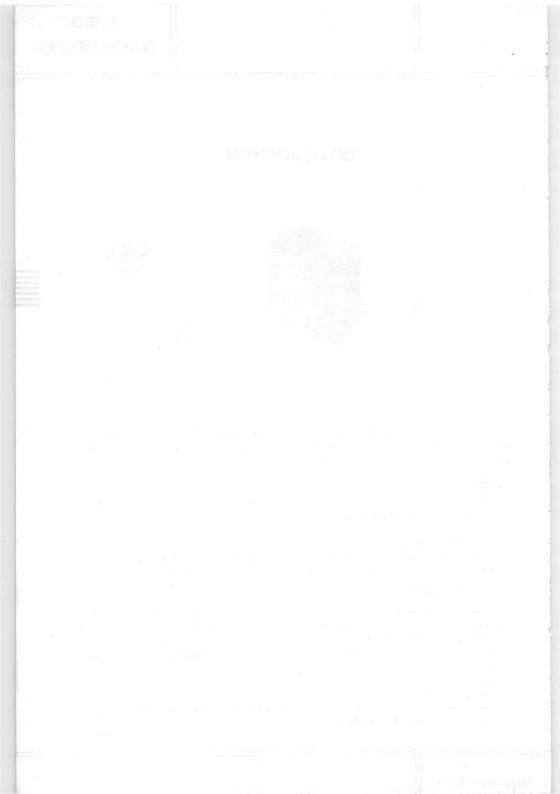
- Fully tropicalised

A moisture-repellent plastic is used as an inter-layer insulator. Moreover, the transformers are impregnated with a particular medium. Any electrolytic dissociation, which is the usual cause of burn-outs, is therefore avoided and the transformers are suitable for use under the most adverse climatic conditions.

- Superior quality

Low distortion and a flat frequency-response curve allow the transformers to be used in high-quality equipment.

September 1968



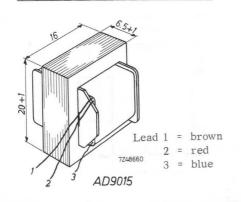
MAINTENANCE TYPE

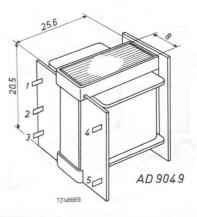
# AUDIO TRANSFORMERS FOR PUSH-PULL CIRCUITS WITH TRANSISTORS

Thanks to the application of anisotropic core material, these transformers will give excellent results in spite of their small size. They are symmetrically wound in order to obtain two absolutely identical halves as regards inductance, capacitance and d.c. resistance.

			1	AD		
type number	AD9015	AD9049	AD9051	$V_b = 7 V$	V <sub>b</sub> = 14 V	1
Primary impedance	360	52	98	7	41	Ω
Secondary impedance	3	3	3	3	-5	Ω
Power	0.2	0.3	0.75		8	W
Efficiency at 400 Hz	85	85	80		70	%
Transformation ratio	11	4.2	5.7	1.6-1.25	3.65-2.85	
Primary inductance	0.6	0.3	0.48	0	.2	H
D.C. bias magnetization	an -	-	-			mA
Primary resistance	16	2.6	9.5	2.	13	Ω
Frequency response between -3 dB points		(B)		· · · · · · · · · · · · · · · · · · ·		
(reference 1 kHz)	45-35000	50-10000	50-10000	10-	10 000	Hz
Distortion is 1 $\%$ at	160	lans.	-		90	Hz

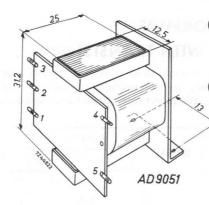
Dimensions (in mm) and connections

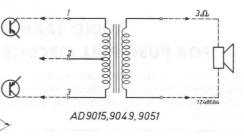




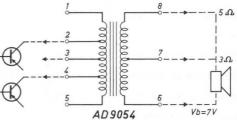
C5

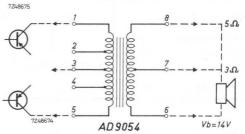
### AUDIO TRANSFORMERS FOR PUSH-PULL CIRCUITS WITH TRANSISTORS

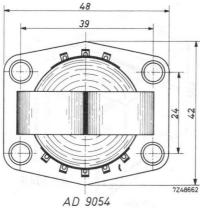


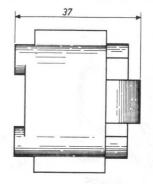


catalog r		1.5	
(for orde	ering)		
AD9015	3122	991	53900
AD9049	3122	991	54310
AD9051	3122	991	54290
AD9054	3122	991	54330









### MAINTENANCE TYPE

September 1968

C6

MAINTENANCE TYPE

AD 9008 AD 9020

# AUDIO TRANSFORMERS FOR SINGLE-ENDED CIRCUITS

_					
		AD9008	AD9020	537	
	Primary impedance	5 400	5 400	Ω	
	Secondary impedance	3-5	3-5	Ω	
	Power	3	6	W	
	Efficiency at 400 Hz	75	76	%	
	Extra windings: anti-hum (% of N <sub>prim</sub> ) feed-back (% of N <sub>sec</sub> )	10 _	_ 112	% %	
	Transformation ratio	45-34	46-33		
	Primary inductance	10	10	Н	
	D.C. bias magnetization	36	40	mA	
	Primary resistance	550	540	Ω	
	Frequency response between -3 dB points (reference 1 kHz)	50 - 10 000	40 - 20 000	Hz	
	Distortion is 1% at	60	65	Hz	

In the AD9057 the coils are wound around a C-type core of oriented laminated sheet. The stray inductance and the winding capacitance are low and, consequently, the resonance frequency is so high that heavy feedback can be applied without risking instability.

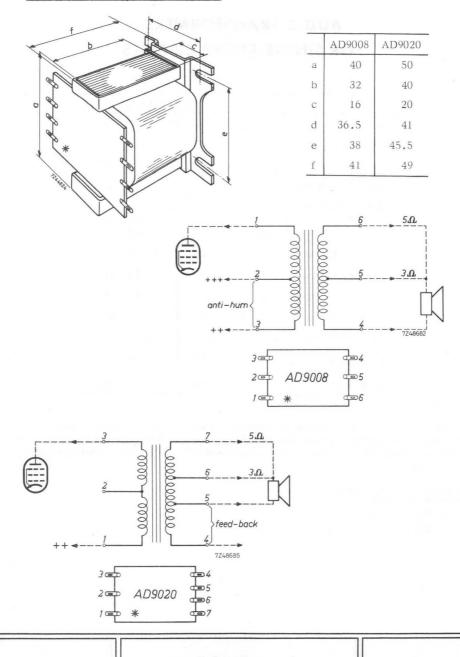
Catalogue numbers (for ordering)

type AD9008: cat. No. 3122 991 53040 AD9020: 3122 108 39990



### AUDIO TRANSFORMERS FOR SINGLE-ENDED CIRCUITS

### Dimensions (in mm) and connections



C8

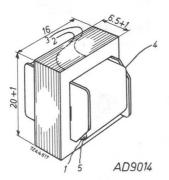
MAINTENANCE TYPE

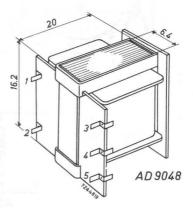
September 1968

# AUDIO TRANSFORMERS FOR DRIVER CIRCUITS WITH TRANSISTORS

type number <sup>1</sup> )	AD9014	AD9048	AD9050	AD9053	
Efficiency at 400 Hz	70	70	75	95	%
Transformation ratio	1	0.65	1.15	1.24	
Primary inductance	10	1,1	3.4	0.44	Н
D.C. bias magnetization	1	4.5	4	75	mA
Primary resistance	400	106	123	4	Ω
Frequency response between -3 dB points (reference 1 kHz)	20-40 000	50-10000	50-10000	10-60 000	Hz
Distortion is 1% at	70	1 - X ( )	-	- 12	Hz

Dimensions (in mm) and connections



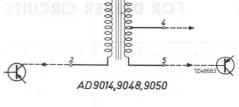


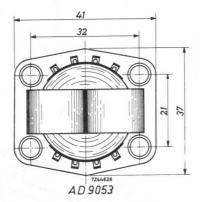
Lead 1 = red

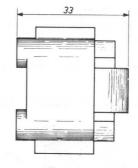
- 2 = blue
- 3 = yellow
- 4 = black
- 5 = green

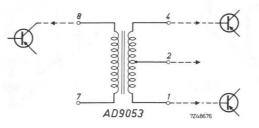
1) For ordering see last page.

AUDIO TRANSFORMERS FOR DRIVER CIRCUITS WITH TRANSISTORS









Catalog numbers (for ordering)

type	catalog number
AD9014	3122 991 62030
AD9048	3122 991 62260
AD9050	3122 991 62240
AD9053	3122 991 62270

C10

MAINTENANCE TYPE

September 1968

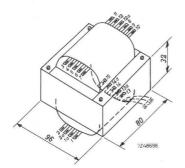
3122 108 39790 3122 108 39800 AD 9026 AD 9027

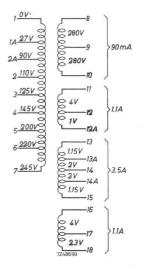
### FIXED MAINS TRANSFORMERS



RZ 17539-4

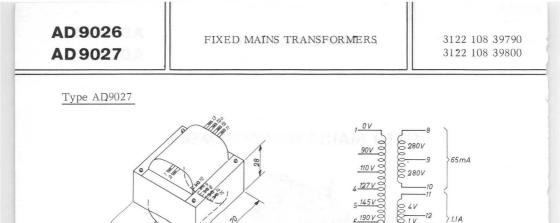
Type AD9026





Catal. No. : 3122 108 39790 No-load current: max. 130 mA No-load losses : max. 7.5 W Weight : 1.93 kg

The secondary voltages indicated in the diagram apply to the loaded condition.



The secondary voltages indicated in the diagrams apply to the loaded condition.

MAINTENANCE TYPE

September 1968

12A

6 21

2A

- 220V

C12

7748700

No-load current: max. 90 mA No-load losses : max. 6 W

: 3122 108 39800

: 1.27 kg

Catal. No.

Weight

# Loudspeakers

# CONTENTS

		page
SURVEY OF LOUDSPEAKER TYPES		D3
GENERAL		D5
Introduction		D8
New commercial coding system		D6
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Frequency response curves		D7
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# SURVEY OF LOUDSPEAKER TYPES

STANDARD RANGE

nominal size (inches)	size shape of basic part of type No. 1)		versions 2)	max. power (W)	old type number (basic part)	page	
$2\frac{1}{2}$	round	AD2070	Z4, Z8, Z15, Z25	0.5	AD3207	D31	
3 3	round square				-	D33 4)	
3 x 5	oval	AD3590	X4, X8, X15, X50, X400	2	AD3359	D37	
4 4 4	round round round	AD4070 AD4080 AD4090	Y4, Y8, Y15, Y25 X4, X8, X15, X25 X8, X15 X400	1 3 2 0.6	- AD3419	D43 D45 D47	
3 x 8 3 x 8			(X4) (X15) X4, X8	2 2 2	AD3386RX AD3386PX -	D35 4)	
4 x 6 4 x 6	oval oval	AD4680 AD4690	Z4, Z8, Z15, Z25 M4, M8, M15, M25 X4, X8, X15, X25 M4, M50, M400, M800	3 4 6 4 4	- AD3469	D51 4)	
5	octag.	AD5080	Z4, Z8, Z15, Z25 M4, M8, M15, M25 X4, X8, X15, X25	3 4 6		D57	
5 x 7	x 7 oval AD5780		X4, X8, X15, X25 M4, M8, M15, M25	4 4	-	D59	
$6\frac{1}{2}$ $6\frac{1}{2}$	octag. octag.	AD7080 AD7091 3)	M4, M8 X4, X8 X4, X8 M4, M800	4 6 3 3	- AD3729	D65 D67	

 A complete type No. is composed of a basic part, a stroke and a version code, e.g. AD2070/Z4, AD7091/M800.

<sup>2</sup>) Letter for type of response characteristic (see General section), followed by the nominal impedance in  $\Omega$ .

3) Inverted magnet system.

4) Data sheets will be issued separately.

### SURVEY OF LOUDSPEAKER TYPES

nominal size (inches)	shape of flange	basic part of type No. 1)	versions 2)	max. power (W)	old type number (basic part)	page
6 x 9	oval	-	(X4)	6	AD3696RX	D39
			(M4)	6	AD3696RM	
	March 11	2011 C	(M8)	6	AD3696SM	
6 x 9	oval	AD6980	X4, X8, M4, M8	6	-	4)
8	octag.		(X4)		AD3806RX	D41
			(X8)		AD3806SX	
			(M4)		AD3806RM	
			(M8)		AD3806SM	
8	octag.	AD8080	X4, X8, M4, M8	6	-	4)

### SPECIAL AND HIGH QUALITY LOUDSPEAKERS

Tweeters

$2\frac{1}{4}$	round	AD2070 AD4490	T4, T8 T4, T8	10 <sup>5</sup> )	- AD3408	D29 D49
4	square	AD4490	14, 10	10	AD3400	D49
Woofers						
5	octag.	AD5060	W4, W8	106)	AD3503	D55
$6\frac{1}{2}$	octag.	AD7065	W8	206)	AD3703	D63
8	octag.	AD8065	W8	206)	AD3803	D71
10	round	AD1055	W8	406)	-	D11
12	round	AD1255	W8	20	AD5201	D17
Wide fre	equency rang	ge				
5	octag.	AD5060	M4, M8	6	AD3501	D53
$6\frac{1}{2}$	octag.	AD7060	M5	10	AD3701	D61
8	octag.	AD8050	M5	6	AD4800	D69
$8\frac{1}{2}$	round	-	M7	10	9710M/01	D73
			M800	10	9710AM/01	
10	round	AD1050	M7, M800	10	AD4000	D9
12	round	AD1250	M7, M800	20	AD4200	D11
12	round	AD1255	M7, M800	20	AD5200	D15
12	round	AD1260	M5	10	AD4201	D27

 $\overline{4}$ ) Data sheets will be issued seperately.

5).With  $5 \,\mu F$  in series.

6) In a closed acoustic box of specified volume.

### GENERAL

#### INTRODUCTION

A correctly chosen loudspeaker is essential to obtain adequate acoustic results from electro-acoustic equipment. The following factors should be considered.

- Shape, size and attachment with reference to the available space.
- Quality and sensitivity, a compromise between fidelity of reproduction and price.
- The frequency-response characteristic in relation to the kind of application.
- Impedance and power-handling capacity, which should be adapted to the output stage of the equipment.
- Appearance and finish.

With a view to these factors our loudspeakers are divided into three groups:

#### Standard speakers

The standard speakers form an extensive group offering a diversity in characteristics, size and price for all kinds of radio and television sets, gramophones, tape recorders, sound columns, etc.

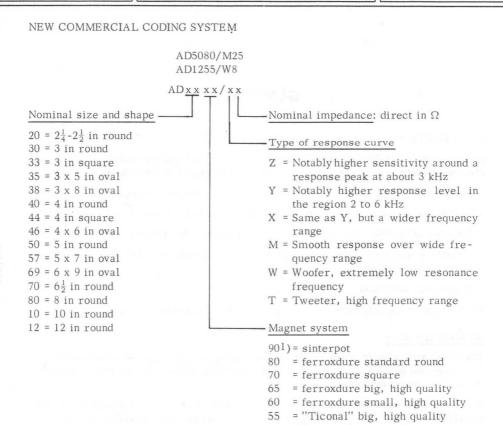
Most standard speakers have a flat magnet system of powerful Ferroxdure. For television sets and other applications where the leakage field should be as small as possible, there are loudspeakers having a Ticonal magnet in a pot system. Due to the use of Ticonal 750 these pot systems are very small.

Special speakers

The special speakers have specific applications.

### High-quality speakers

The high-quality speakers have been specially designed for use in Hi-Fi equipment, where a high power-handling capacity, a very wide frequency-range and a negligible distortion level are required. Examples of application: acoustic boxes, bass-reflex boxes, juke boxes, Hi-Fi enclosures with or without cross-over network and stereo columns.



50 = "Ticonal" small, high quality

#### IMPEDANCES

The nominal impedance is the lowest impedance on the impedance/frequency curve measured at the high-frequency side of the resonance peak.

Loudspeakers with impedances not given in the data sheets are available to special order. Details on request.

 Mechanical or acoustical variations are indicated by replacing 0 or 5 by some other figure (91 = Sinterpot Wafer).

#### FREQUENCY RESPONSE CURVES

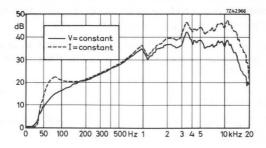
### Measuring conditions

The frequency-response curves are measured under the following conditions:

- 1. recorded in anechoic room;
- 2. without baffle;
- 3. microphone in axis of loudspeaker at a distance of 50 cm;
- 4. input 50 mW (12" high-quality types 25 mW);
- 5. constant voltage;
- 6. 0 dB of the curves corresponds with 52 dB above  $2x10^{-4} \mu bar$ .

Comparing a constant-current characteristic of any loudspeaker with a constantvoltage one, we find the latter flatter in the region of the resonance frequency, whereas it drops more abruptly at the higher frequencies. This is explained as follows:

The power which moves the coil and the cone is proportional to the current through the coil. In the case of constant voltage the current will decline, as a consequence of rising coil impedance, in the neighbourhood of the resonance frequency and at higher frequencies. The result is a dropping sound pressure in these frequency regions. This should be borne in mind when comparing our response curves with those of other documentations.



### The use of response curves

First of all we wish to emphasise that these curves should be used exclusively for comparison.

Never compare curves which are not based on one and the same measuring method (identical measuring equipment, measuring room, distance, power input and, even, identically mounted speakers). Only experienced experts are able to compare response curves not based on exactly identical conditions. Also the condition of the anechoic chamber may greatly affect the results.

Contrary to many other manufacturers' methods, frequency characteristics of our loudspeakers were determined without a baffle.

#### The response curves for making comparisons

The response curve does help us to disclose differences in reproduction quality. The comparison of curves determined under identical conditions may give a picture of a few acoustical aspects. A difference in level means a difference in sensitivity (efficiency) in various frequency regions. A difference in width means a difference in frequency range.

One should never forget, however, that the curves represent the sound pressure only in the centre of a circular plane. Since the distribution of the sound pressure is not uniform over the plane and different in various cases, the sound impression may differ more than the response curves suggest.

It will be evident that a high degree of expertness is required to interpret the differences in response curves. For the greater part, this expertness is gained through experience.

#### Response curves an aid for the manufacturer

Response curves play a great part in the development of loudspeakers, pinpointing their acoustic characteristics, manufacture and production checks.

It is but a small problem for the development engineer to establish response curves required for a particular application. And then, as the acoustic characteristics of a speaker are largely associated with its moving parts (coil, centring ring and cone), it is a fairly simple matter for him to base modifications on the frequency curve and with its aid examine the effect.

For loudspeakers in production the frequency characteristic is excellently useful to check the production quality and, at the same time, the sensitivity of the magnet system.

### POWER HANDLING CAPACITY

The rated power handling capacity is the maximum power which the loudspeaker can withstand, when subjected to the following tests:

1. Operational test.

A test voltage of audio frequency is applied to the loudspeaker. The loudspeaker is then checked for buzz, chips, rattle, or cone break-up. The test voltage V = 0.7 x  $\sqrt{Z \times P_{max}}$ , where Z = nominal impedance in ohms and  $P_{max}$  = power handling capacity in watts.

2. Continuous load test.

100 hours life-test conforming to DIN 45573 - sheet 2 with a test-power of  $\rm P_{max}$  and a white noise generator.

#### FINISH

The loudspeakers are tropic-proof, and cadmium-plated to prevent corrosion.

(AD4000M) (AD4000AM)

## AD 1050/M7 AD 1050/M800

### **10" HIGH-QUALITY LOUDSPEAKERS**

#### Primary application

Hi-Fi and stereo equipment (see "Enclosures").

### Details

Very high sensitivity, Ticonal magnet.

Particularly large airgap, resulting in the voice coil being completely enclosed by a uniform magnetic field even at the largest amplitudes. No distortion will thus be experienced as the coil amplitude is disproportional to the current. Constant voice-coil impedance throughout the entire frequency range, so that the output stage always has a perfectly matched load.

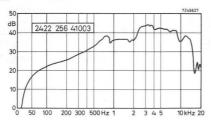
Very smooth response curves.

Clear bass response without boom effects, because of mechanical damping at low frequencies.



RZ 14210-5

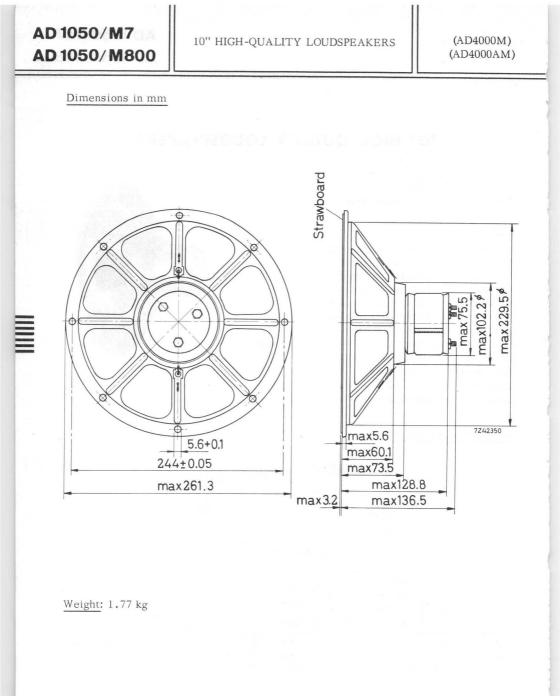
### Technical performance



version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number
M7	M	7	10	50	98 000	8000	2422 256 41003
M800	M	800	10	50	98 000	8000	2422 156 41002

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



### AD1055/W8

### **10 in HIGH-QUALITY WOOFER LOUDSPEAKER**

#### Application

In acoustic enclosures for Hi-Fi reproduction; suitable for frequencies of 18 to 1000 Hz. See data sheet on the 40 W combination with AD5060/M8 and AD3506SM or AD5080/M8 in an acoustic box of 35 litres.

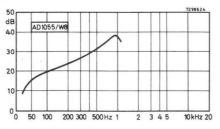


Ticonal magnet. Weight of magnet 880 g. Constant flux through moving voice coil resulting in a low distortion. Rigid paper cone with highly flexible butyl-rubber suspension.



RZ 25052-31

### Technical performance



version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number 2)
W8	W	8	40 <sup>1</sup> )	24	130 000	> 9000	4304 078 70261

1) In an acoustic enclosure of max. 35 litres, and conforming to DIN45573.

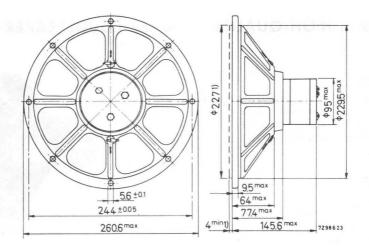
<sup>2</sup>) For bulk packing the catal. No. is 4304 079 01001; for single-unit packing the catal. No. is 4304 079 01021.

October 1968

# AD1055/W8

### 10 in HIGH-QUALITY WOOFER LOUDSPEAKER

### Dimensions in mm



<sup>1</sup>)Baffle hole and clearance depth required for cone movement at 40 W input.

 ${\rm A}\xspace$  red mark near one of the tags serves for in-phase connection with other loudspeakers of our range.

Weight: 3 kg

(AD4200M) (AD4200AM)

## AD 1250/M7 AD 1250/M800

### 12" HIGH-QUALITY LOUDSPEAKERS

### Primary application

Hi-Fi installations.

### Details

Very high sensitivity, Ticonal magnet.

Particularly large air gap, resulting in the voice coil being completely enclosed by a uniform magnetic field even at the largest amplitudes. No distortion will thus be experienced as the coil amplitude is disproportional to the current. Constant voice-coil impedance throughout the entire frequency range, so that the output stage always has a perfectly matched load.

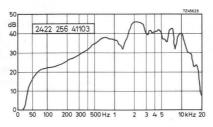
Very smooth response curve.

Clear bass response without boom effects, because of mechanical damping at low frequencies.



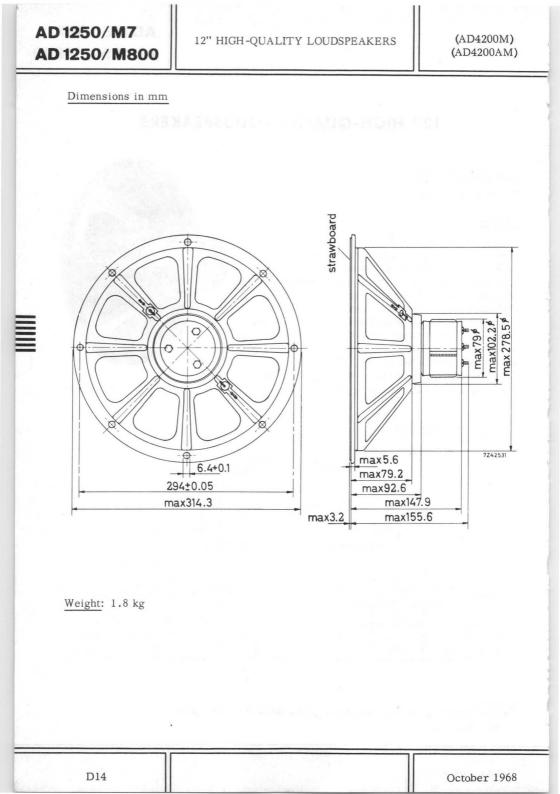
RZ 19741-15

### Technical performance



version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number
M7	M	7	20	50	98 000	8000	2422 256 41103
M800	M	800	20	50	98 000	8000	2422 256 41102

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.



(AD5200M) (AD5200AM)

### AD 1255/M7 AD 1255/M800

### 12" HIGH-QUALITY LOUDSPEAKERS

### Primary application

Hi-Fi installations.

### Details

Extremely high sensitivity thanks to the use of a very powerful Ticonal magnet.

Particularly large air gap, resulting in the voice coil being completely enclosed by a uniform magnetic field even at the largest amplitudes. No distortion will thus be experienced as the coil amplitude is disproportional to the current. Constant voice-coil impedance throughout the entire frequency range, so that the output stage always has a perfectly matched load.

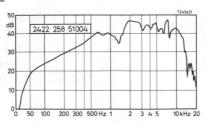
Very smooth response curves.

Clear bass response without boom effects, because of mechanical damping at low frequencies.



C 65219

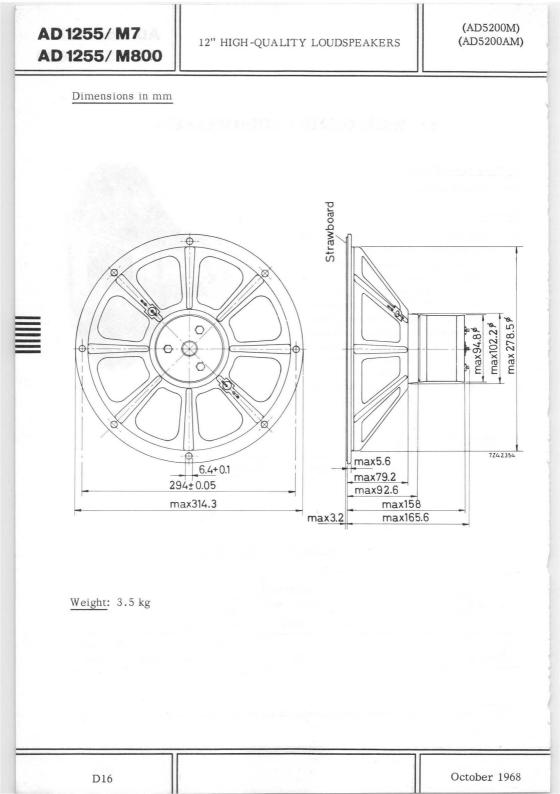
#### Technical performance



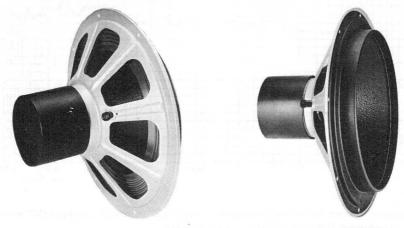
version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number 1)
M7	M	7	20	50	$\frac{134000}{134000}$	11 000	2422 258 51004
M800	M	800	20	50		11 000	2422 258 51003

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



12" HIGH-QUALITY WOOFER LOUDSPEAKER



RZ 19218-1

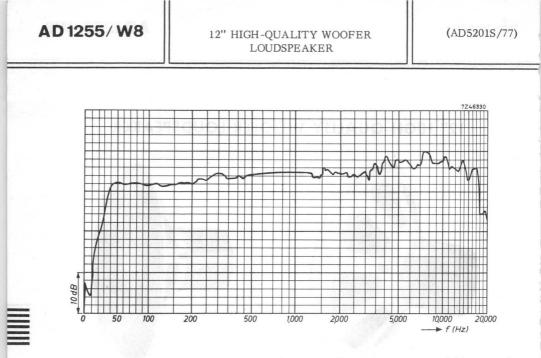


Though the design of this woofer is based on the normal electrodynamical principle, a number of striking features make it unique in its kind. The use of new materials and techniques allowed the development of a Hi-Fi low-note speaker which, in conjunction with high and medium-note speakers and housed in an acoustically adequate enclosure, will be found a major contribution towards natural sound reproduction. Because of its specific design and characteristics, this speaker is a solitary in our programme.

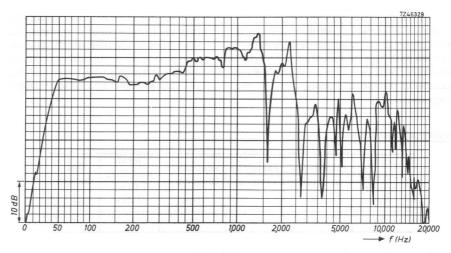
Technical performance

power handling capacity (W)	impedance at 1 kHz (Ω)	response curve	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)
20	8	W	29	134 000	9300

Catalog number, bulk packing : 2422 258 41121 single-unit packing : 2422 258 41161 on loudspeaker itself: 2422 258 41101



Response of the woofer in conjunction with two 5 x 7" standard speakers (M4 version) and a cross-over filter in a 45-litre acoustic box.



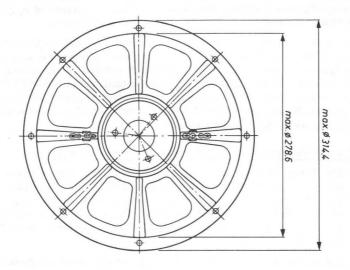
Response of the woofer (alone) in a 45-litre acoustic box.

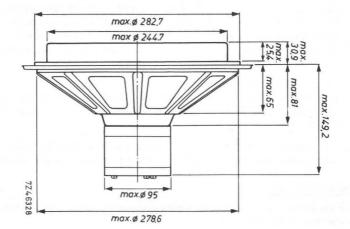
Note: See also "Recommended enclosures".

### 12" HIGH-QUALITY WOOFER LOUDSPEAKER

AD 1255/W8

### Dimensions in mm





Weight: 3.5 kg

October 1968

### AD 1255/W8

#### REMARKS ON LOW-NOTE REPRODUCTION

#### Introduction

Low notes are a perpetual obstacle on the way to Hi-Fi reproduction. Prior to discussing this problem, let us consider the importance of an effective reproduction of the low notes, particularly in the case of music.

One musical instrument differs from another not only in the range of notes but also in the tone colour or timbre. This latter phenomenon is a consequence of the fact that a musical instrument produces complex sounds which are composed of a fundamental tone and overtones. If the fundamental tone and the lower overtones are not reproduced, we hear the fundamental pitch - but the timbre will be degraded. Hence, the lower the notes reproduced by a loudspeaker, the more instruments we hear true-to-nature.

#### What are the requirements for a good low-note reproduction

- The lower limit of the loudspeaker's frequency range should be as low as possible. A minimum frequency of 40-50 Hz is quite favourable. Some instruments such as organs have a fundamental frequency of 16 Hz, which is about the limit of audibility. The wavelength of a tone of 25 Hz, for instance, is approx. 13 metres, and this is too large to sound well in the majority of rooms.
- 2. A sufficiently large acoustic power also in the lowest frequencies.
- 3. Generally, an acoustic power of 4 mW per cub.metre of room volume is ample. That means about 0.5 W for a living room of fair dimensions. Particularly in the case of organ music but also of orchestral music, for short periods this energy may be entirely concentrated in the lowest octaves. Therefore, a bass energy between 0.5 and 1 W in the lowest octaves is a must for a good Hi-Fi speaker.
- 4. The low notes should be reproduced without distortion. This difficult requirement can be complied with only in the case of speakers specifically designed for low-note reproduction and housed in an adequate acoustic box.
- 5. The acoustic enclosure carries with it the difficulty of its size, and this leads to the additional requirement of small dimensions for the speaker system.

#### The acoustic box

The enclosure is a closed box which completely separates a given volume of air at the rear of the speaker.

### Advantages

1. Between the so-called relaxation frequency (800-1000 Hz) and the frequency resonance, the low-note reproduction is improved by about 6 dB per octave with regard to a speaker without baffle.

The acoustic box acts, as it were, as a baffle of infinite size.

- 2. The separated air volume accomplishes an effective damping and, hence, an increased loadability.
- 3. The separated air volume increases the stiffness of the cone suspension and so prevents distortion due to non-linearity of the cone movement.

#### Drawbacks

- 1. The separated air raises the resonance frequency of the system.
- The large box occupies much space.
   With this woofer, these drawbacks are limited to the strict minimum.

#### The loudspeaker

The following equation applies to the acoustic power produced by a loudspeaker:

- $W = k x f^4 x s^2 x A^2$ , where
- W = the acoustic energy in watts,
- f = the frequency,
- s = the stroke of the moving coil,
- A = the area of the cone.

This implies that the product sA should be large enough to render, also in the lowest octaves, the required quantity of acoustic power (s is two times the amplitude of the coil movement in the air gap).

For a satisfactory low-note reproduction, the self-resonance of the speaker should be as low as possible, and also the resonance increase resulting from the insertion in a box. This increase will be greater when the box volume is smaller and the cone diameter larger. Hence, to obtain the final resonance-frequency of the system as low as possible at a box volume as small as possible, the cone diameter should not be chosen too large.

In order nevertheless to have a large product sxA, a large stroke is therefore a requirement of pre-eminent importance.

For the avoidance of distortion, notwithstanding the long stroke of the coil, the following requirements should be met.

Even in its ultimate positions, the coil should remain within the homogeneous magnetic field.

The reaction of cone and centring ring should always be in accordance with the coil movements.

This means that the cone suspension should be flexible, that the cone itself should be stiff, and that the non-harmonic movements of cone and centring ring should be adequately damped. Furthermore, an efficiency as high as possible is of importance to acquire the maximum acoustic output with the minimum electric input. This requires, among other things, a powerful magnetic field, a light cone and a light centring ring. Requirements to obtain a low resonance frequency are, inter alia, a flexible cone suspension and a not too small cone mass, which involves a fairly large cone diameter.

To complete the situation, we observe that an adequate loadability requires an effective damping and, therefore, a not too large volume of separated air, a sufficiently strong cone and a sturdy suspension.

From the above, the following will be clear.

The loudspeaker should have a cone of great stiffness, a powerful magnetic field, a large coil stroke in a homogeneous field, and a low resonance frequency.

The optimum compromise should be found for the stiffness of the cone suspension, the cone diameter, the cone weight and the box volume.

After a great numbre of experiments, we obtained the following as the optimum result.

### DESIGN OF THE WOOFER

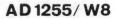
#### The cone

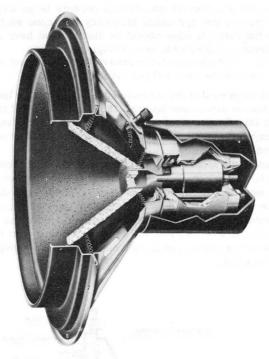
Foam plastic as the cone material guarantees a combination of great stiffness and a low mass.

Of course, though not ideal, paper is not a bad cone material; until recently, there was no second of equal strength, lightness and acoustic effect. The specific weight of cone paper is 0.2. However, the lacquer required to obtain resistance to moisture, raises the specific weight to 0.5.

The specific weight of the plastic foam used for the woofer is 0.02. That means, the thickness may be 25 times as large before the weight of a corresponding cone in paper is reached. Thus, diaphragms having a thickness of 1 cm and more can be used that are perfectly rigid. These diaphragms, included the voice coil, do not weigh more than about 12 g.

In this case, it is not necessary to stiffen the cone artificially through the box to reduce the distortion, and the dimensions of the box can be chosen purely in view of the low-note reproduction. Distortions as a result of deformations of the diaphragms are likewise out of the question.





### Frequency characteristic

The almost complete stiffness of the cone engenders a drawback. Paper diaphragms vibrate as a whole as long as the wavelength of the tone produced exceeds the cone diameter. Hence, at rising frequency, the effective area of the paper cone and, correspondingly, the moving mass, decrease steadily. As a result of this phenomenon, paper cones reproduce notes beyond 1 kHz with an adequate efficiency.

In the case of a relatively small cone such as that of the woofer, however, rise in frequency causes no drop in moving mass and, consequently, beyond the frequency at which the cone ceases to act as a piston, no effective output is to be expected. Therefore, the woofer should be used exclusively in conjunction with other speakers for reproduction of the high and the medium notes.

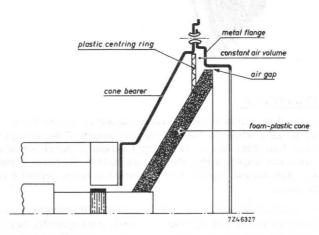
### Cone suspension

It will be clear that the special cone design permits large amplitudes. Therefore, and to obtain a low resonance frequency, the cone suspension should be flexible. Also the centring edge should be flexible and have a large area; the ridges in the centring edge should have a hinging function.

The hinging edge might disturb the linearity of the movement and so cause distortion. In the case of the woofer this is avoided as follows.

The cone is not suspended at the ultimate edge but somewhat lower, and a metal flange is attached on to the cone bearer. The ultimate edge of the cone moves to and fro within this flange. Cone edge, centring ring and flange form a ring-shaped chamber which is only connected to the external air by means of a narrow gap between cone and flange.

The dimensions of the separate air chamber are such that theoretically, during the entire stroke of the cone edge, the volume of the chamber remains almost constant if we assume a linear movement of the centring ring. According as nonlinearity in the cone suspension tends to deform the centring ring, any change in volume pumps the air through the narrow gap. Hence the surname of this original speaker: the low-note pump. The gap acts as a flow resistance whose energy absorption causes damping. Any distortion of the moving system is, as it were, pumped away.



### The permissible stroke of the cone

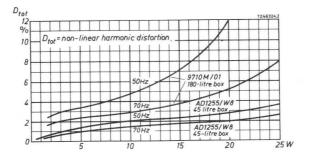
All causes of distortion resulting from diaphragm deformations now being eliminated, or at least substantially reduced, it is all the more important to avoid any distortion resulting from non-linearity in the diaphragm drive as well. The force exerted on the voice coil is  $0.1 \times B \times I \times L$ , where B, is the induction, I the current through the coil and L the length of wire. At any moment and independent of the position of the coil, this force should be proportional to I and, therefore, the coil should be always in a field of constant intensity.

In principle, there are two manners to meet this condition. The first one is making the coil considerably longer than the thickness of the pole plate or, in other words, the height of the field in the air gap. An advantage of this method is a high field-intensity without a heavy magnet, which tends to keep the price low.

A disadvantage is a significant increase in mass and resistance of the coil, resulting in a drop in efficiency. Therefore, a more powerful amplifier will be required and the price of the total equipment will rise. Of even greater consequence may be the fact that the inactive part of the coil increases the internal resistance of the amplifier and so adversely affects the damping factor.

An alternative is heightening the air gap so as to keep the coil movement within the homogeneous field. In this case, the mass and the resistance of the coil can be kept as small as possible - but a drawback is, of course, the necessity of a much larger magnet. Freedom of distortion cannot be obtained on the cheap.

It is the second method that was applied to the woofer. The thickness of the pole plate is two times the length of the coil which can, thus, make a stroke of 8 mm within the homogeneous part of the filed. This stroke is an enormous feature of this speaker, the more so as - even at the stroke of this length - no distortion whatever of the signal occurs.



Non-linear distortion as a function of the input power compared with that of an  $8\frac{1}{2}$ , 10 W high-quality loudspeaker.

#### The acoustic box

Building the speaker into an enclosure of about 40 litres nett, makes the resonance frequency of 29 Hz rise to about 50 Hz.

Measurements in a box of this volume demonstrated that even a 50-W load did not cause any audible distortion; in larger boxes, an energy of at least 20 W is permissible (these figures apply to normal orchestral music). In the case of musical passages such as low organ notes, where almost the entire reproduction occurs in the lowest frequencies, a smaller electric energy suffices for an adequate sound intensity.

To obtain the optimum reproduction quality, we advice to build the speaker in an enclosure of 40-50 litres nett, which results in an almost flat response curve between 40 and 1000 Hz. At a load of 30 W, the distortion is max. 3 % at half an octave beyond the resonance frequency.

#### Reproduction of the high and medium notes

If the speakers for these notes are housed in the same enclosure - of course in a separate room - it is not necessary to choose the cross-over frequency extra low: this would cause difficulties as regards the filter dimensions. A cross-over frequency of 800 Hz and a cut-off rate of 12 dB per octave are recommended.

(AD4201M)

### AD 1260/M5

# 12" SPECIAL LOUDSPEAKERS

### Primary application

Juke boxes; acoustic boxes for musical installations. See "Recommended enclosures".

### Details

Inexpensive speaker with a reasonably good efficiency, well suitable for those installations where both costs and quality are factors of importance.

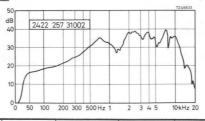
Suited for stereo reproduction because of its wide frequency range,

Ferroxdure magnet.



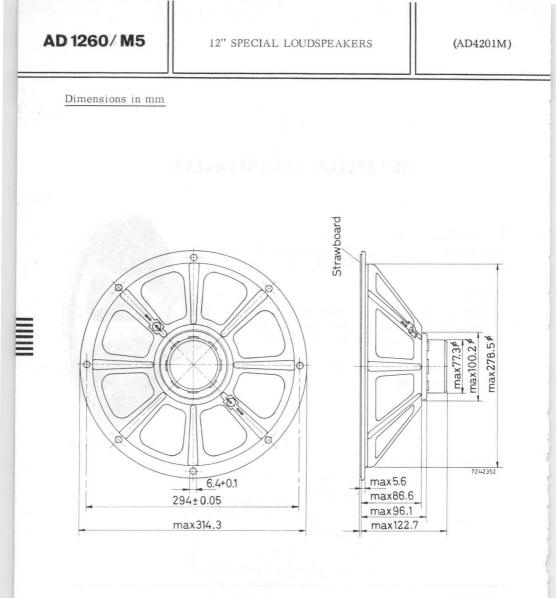
RZ 14211-10

#### Technical performance



power handling capacity (W)	impedance at 1 kHz (Ω)		resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number (bulk packing) <sup>1</sup> )
10	5	М	50	42 600	9 5 0 0	2422 257 31002

 When ordering, the last but one digit should be 2 for bulk packing and 6 for single-unit packing.



Weight: 850 g

### 2 1/4 in TWEETER LOUDSPEAKERS

### Application

In acoustic enclosures; suitable for frequencies of 800 Hz to 19 kHz. These tweeters can be combined with the 5 in woofer AD5060/W without extra loud-speaker being necessary for the medium frequency range.

#### Construction

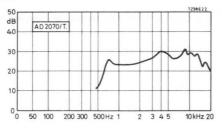
Flat square magnet of Ferroxdure 300 R. Weight of magnet 20 g.



AD2070/T4 AD2070/T8

RZ 25052-32B

#### Technical performance



version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number 2)
T4	T	4	10 <sup>1</sup> )	800	6900	> 6900	2422 257 22001
T8	T	8	10 <sup>1</sup> )	800	6900	> 6900	2422 257 22002

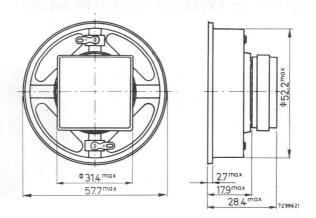
1) With a capacitor of  $5 \,\mu\text{F}$  in series and a signal in conformity with DIN45573.

2) When ordering bulk packing add 20 to the last two digits; when ordering singleunit packing add 60 to the last two digits.

April 1968



Dimensions in mm



Baffle hole diameter 52 mm

A red mark near one of the tags serves for in-phase connection with other loud-speakers of our range.

Weight: 70 g

# AD 2070/Z4 -AD 2070/Z25

# $2^{1\!\!/_2}$ in STANDARD LOUDSPEAKERS

### Application

Small transistorized radios.

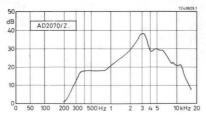
### Construction

Flat square magnet of Ferroxdure 300R.



RZ 20704-2

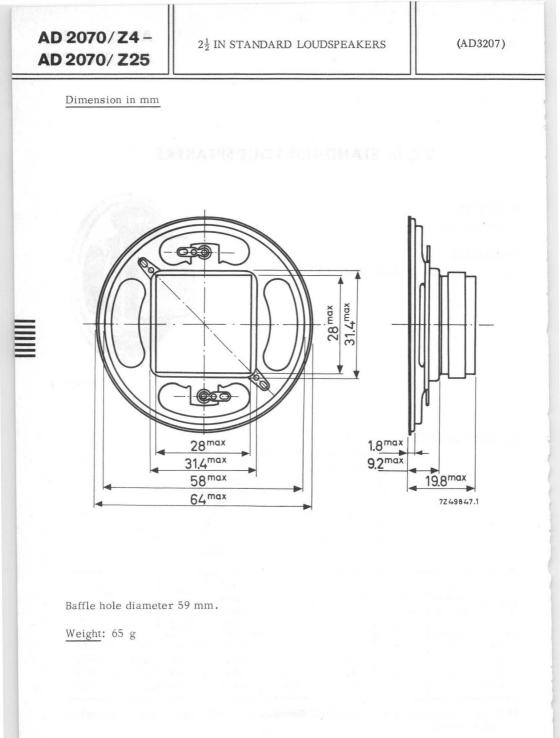
### Technical performance



version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalogue number 1)
Z4 Z8 Z15 Z25	Z Z Z Z	4 8 15 25	0.5 0.5 0.5 0.5	360 360 360 330	6300 6300 6300 6300	> 7400 > 7400 > 7400 > 7400 > 7400	2422 257 23801 2422 257 23802 2422 257 23803 2422 257 23803

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



AD 3070/Y.

# **3 in STANDARD LOUDSPEAKERS**

### Application

Portable receivers.

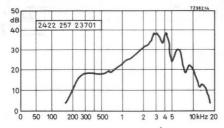
### Construction

Flat square magnet system of Ferroxdure 300R.



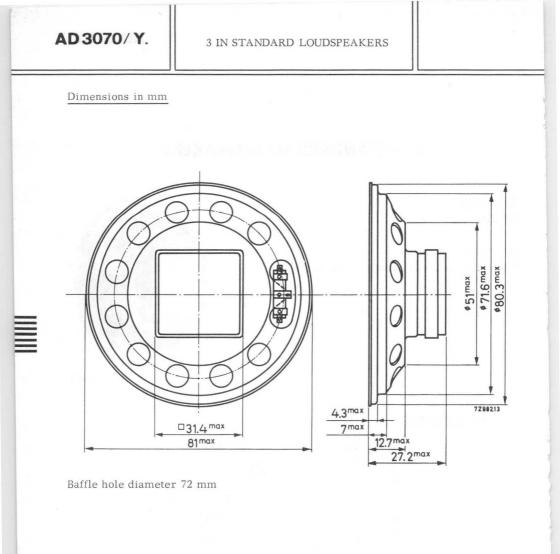
RZ 24408-4

### Technical performance



version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number
Y4	Y	4	1	250	6300	7500	2422 257 23701
Y8	Y	8	1	250	6300	7500	2422 257 23702
Y15	Y	15	1	250	6300	7500	2422 257 23703
Y25	Y	25	1	250	6300	7500	2422 257 23704

1) When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.



Weight: 75 g

# 3"×8" STANDARD LOUDSPEAKERS

Primary application

Radio and TV receivers.

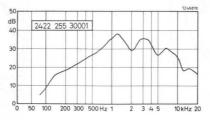
Details

Magnet of Ticonal 750 and a pressed voice coil.



RZ 21906-9

Technical performance

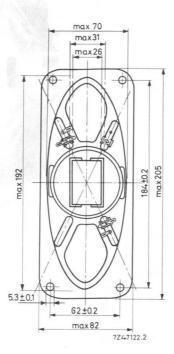


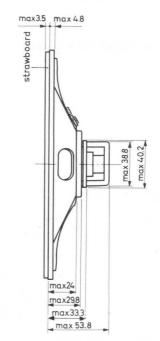
version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number
RX	X	4	2	130	15 800	8800	2422 255 30001
PX	X	15	2	130	15 800	8800	2422 255 30002

1) When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing. AD 3386.X

3" x 8" STANDARD LOUDSPEAKERS

Dimensions in mm





Weight: 210 g

October 1968

(AD3359.X)

### AD 3590/X.

### **3 X 5 in STANDARD LOUDSPEAKERS**

### Application

TV sets, portable radios, tape recorders

#### Construction

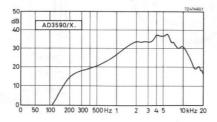
Equipped with a powerful magnet of Ticonal 750 and a pot of sintered iron.

Negligible stray field (at 1 mm distance from the magnet system, the stray field is hardly measurable).



RZ 20704-3

### Technical performance

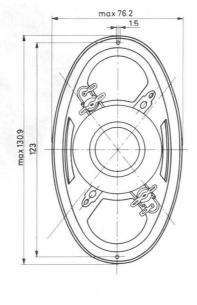


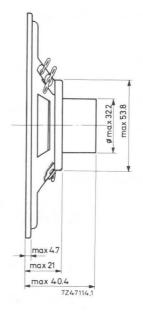
version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catal. number
X4	X	4	2	200	11800	10 000	2422 256 30301
X8	X	8	2	200	11800	10 000	2422 256 30304
X15	X	15	2	200	11 800	10 000	2422 256 30305
X50	Х	50	2	200	11 800	10 000	2422 256 30302
X400	Х	400	2	200	11 800	10 000	2422 256 30303

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968

AD 3590/X. 3 x 5 in STANDARD LOUDSPEAKERS (AD3359.X)
Dimensions in mm





Weight: 135 g

# AD 3696 RX -AD 3696 SM

### 6"×9" STANDARD LOUDSPEAKERS

### Primary application

AM/FM receivers, TV receivers, radiograms.

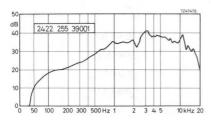
#### Details

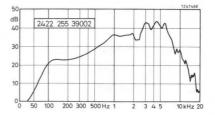
Equipped with a powerful magnet of Ticonal 750 and a pressed voice coil.



#### RZ 21096-6

#### Technical performance

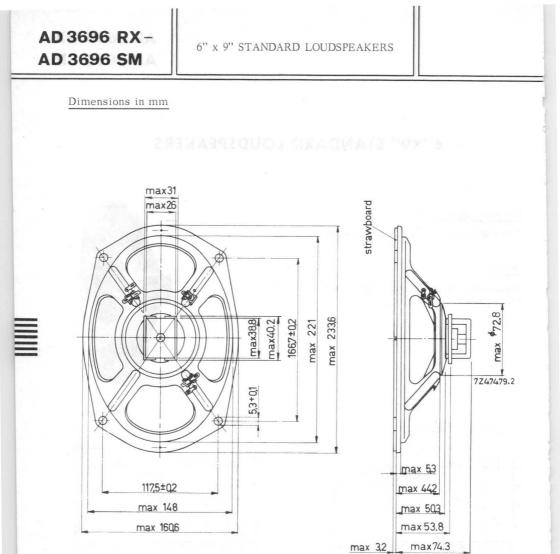




version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number l)
RM	М	4	6	77	14500	8100	2422 255 39001
SM	М	8	6	77	14 500	8100	2422 255 39004
RX	Х	4	6	85	15 800	8800	2422 255 39002

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



Weight: 310 g

# AD 3806 RM-AD 3806 SX

# 8" STANDARD LOUDSPEAKERS

### Primary application

Radio and TV receivers.

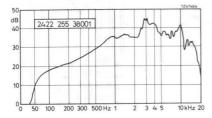
### Details

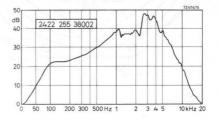
Equipped with a powerful magnet of Ticonal 750 and a pressed voice coil.



RZ 20890-12

### Technical performance

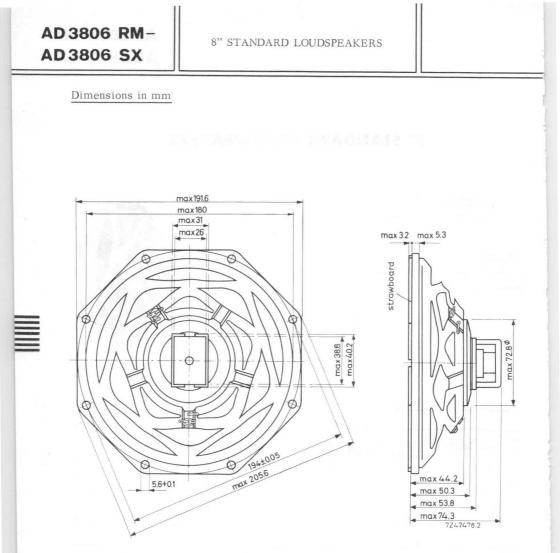




version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number 1)
RM	М	4	6	75	14 500	8100	2422 255 38001
SM	M	8	6	75	14 500	8100	2422 255 38004
RX	Х	4	6	95	15 800	8800	2422 255 38002
SX	Х	8	6	95	15800	8800	2422 255 38003

1) When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



Weight: 280 g

AD 4070/Y.

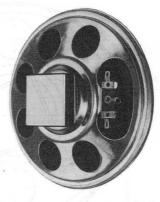
### 4 in STANDARD LOUDSPEAKERS

### Application

Portable receivers, small tape recorders, in-tercoms.

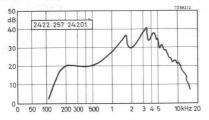
#### Construction

Flat square magnet system of Ferroxdure 300R.



RZ 22408-3

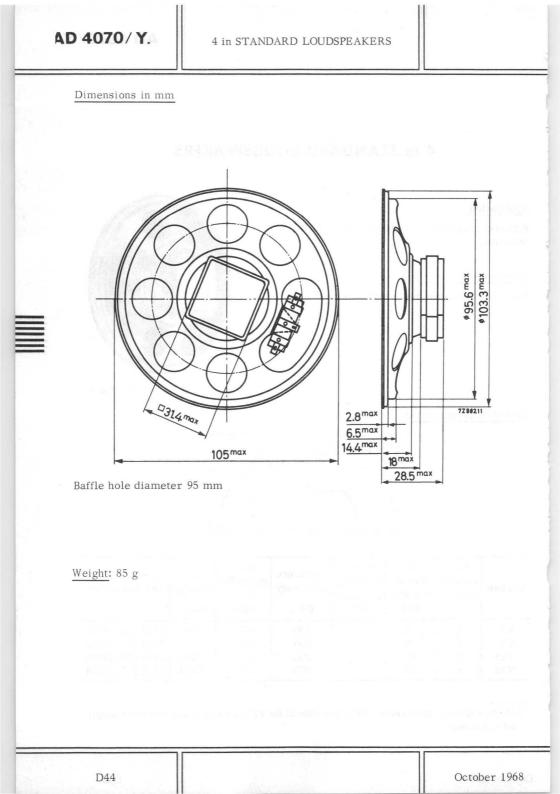
### Technical performance



version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catal. number 1)
Y4	Y	4	1	200	6300	7400	2422 257 24201
Y8	Y	8	1	200	6300	7400	2422 257 24202
Y15	Y	15	1	200	6300	7400	2422 257 24203
Y25	Y	25	1	200	6300	7400	2422 257 24204

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



# 4 in STANDARD LOUDSPEAKERS

### Application

Portable receivers, small tape recorders, in-tercoms.

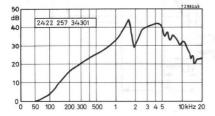
### Construction

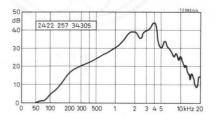
Highly sensitive magnet system of Ferroxdure  $300 \ensuremath{\mathsf{R}}\xspace$  .



RZ 24635-1

### Technical performance

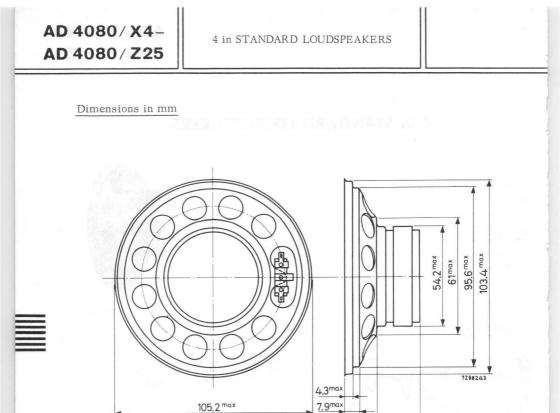




version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catal. number 1)
X4	Х	4	3	165	17500	9800	2422 257 34301
X 8	X	8	3	165	17500	9800	2422 257 34302
X15	Х	15	3	165	17500	9800	2422 257 34303
X25	Х	25	3	165	17500	9800	2422 257 34304
Z4	Z	4	3	185	17500	9800	2422 257 34305
Z 8	Z	8	3	185	17500	9800	2422 257 34306
Z15	Z	15	3	185	17500	9800	2422 257 34307
Z25	Z	25	3	185	17500	9800	2422 257 34308

<sup>1</sup>) When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



17.2 max

39<sup>max</sup>

Baffle hole diameter 96 mm

Weight: 250 g

(AD3419.X)

AD 4090/X.

# 4 in STANDARD LOUDSPEAKERS

#### Primary application

Portable receivers (in particular for AM/FM)

### Details

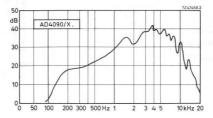
High sensitivity

Magnet of Ticonal 750 and a pot of sintered iron. Negligible stray field (at 1 mm distance from the magnet system, the stray field is hardly measurable).



RZ 20704-5

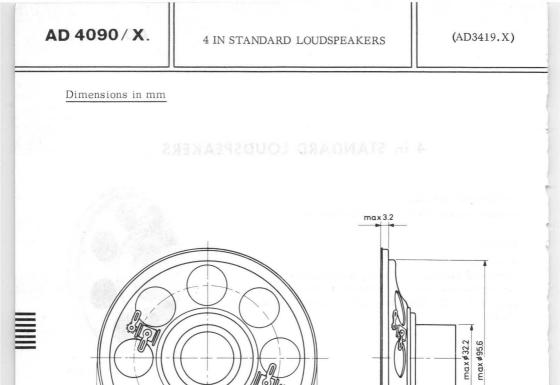
#### Technical performance



version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catal. number 1)
X8	X	8	2	180	11 800	10 000	2422 256 34301
X15	X	15	2	175	11 800	10 000	2422 256 34302
X400	X	400	0.6	190	11 800	10 000	2422 256 34303

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



### Weight: 125 g

max 105

İ

max 14.9 max 16.7

max 36.2

# 4" HIGH-QUALITY TWEETER LOUDSPEAKERS

### Primary applications

Hi-Fi high-note reproduction. Particularly suitable for use in combination with high-quality loudspeakers for low- and medium-note reproduction.

#### Details

Equipped with a relatively small, but nevertheless powerful magnet of Ticonal 750, which ensures a high efficiency.

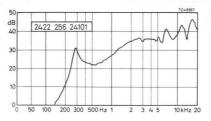
Rigid cone suspension.

Reproduction of high frequencies up to over 20 kHz.



RZ 21906-5

### Technical performance



version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number <sup>1</sup> )
T4	T	4	10	300	18 800	> 7000	2422 256 24102
T8	T	8	10	300	18 800	> 7000	2422 256 24101

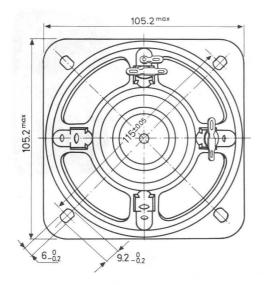
 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

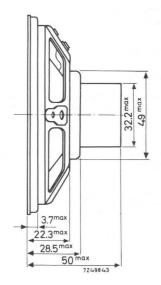
October 1968

AD 4490/T.

(AD3408.M)

Dimensions in mm





Baffle hole diameter 96 mm.

A red mark near one of the tags serves for in-phase connection with other loudspeakers of our range.

Weight: 140 g

# 4 x 6 in STANDARD LOUDSPEAKERS

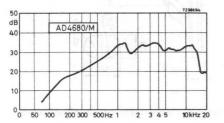
#### Application

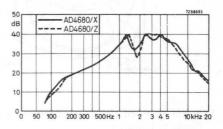
Radios (car and domestic), tape recorders and TV receivers.

#### Construction

Round magnet of Ferroxdure 300R. Weight of magnet 100 g. Pressed voice coil.

Technical performance





version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number 2)
M4	М	4	4 l)	125	18 000	> 10 000	2422 257 30209
M8	М	8					2422 257 30211
M15	М	15					2422 257 30212
M25	М	25					2422 257 30213
X4	Х	4	61)	140	18 000	> 10 000	2422 257 30205
X8	Х	8			-		2422 257 30206
X15	Х	15					2422 257 30207
X25	Х	25					2422 257 30208
Z4	Z	4	31)	155	18 000	> 10 000	2422 257 30201
Z8	Z	8				*	2422 257 30202
Z15	Z	15					2422 257 30203
Z25	Z	25					2422 257 30204

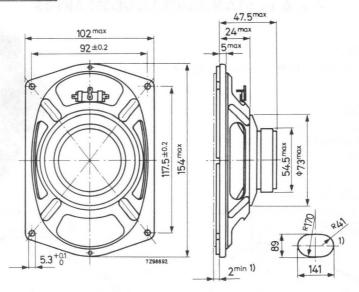
1) With an input signal in conformity with DIN 45573.

2) When ordering bulk packing add 20 to the last two digits; when ordering singleunit packing add 60 to the last two digits.





Dimensions in mm



1) Baffle hole and clearance depth required for cone movement at specified power handling capacity.

 ${\rm A}$  red mark near one of the tags serves for in-phase connection with other loud-speakers.

Weight: 0.26 kg.

(AD3501.M)

### AD 5060/M.

# 5 in HIGH-QUALITY LOUDSPEAKERS

#### Primary application

5-8 litres acoustic enclosures.

#### Details

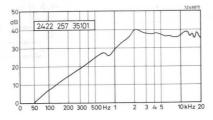
Equipped with a very sensitive Ferroxdure magnet system.

Special textile cone rim allows large amplitudes of the cone movements at low frequencies. This results in an optimum bass reproduction in the smallest enclosures. Low resonance frequency and wide frequency range.



RZ 21906-13

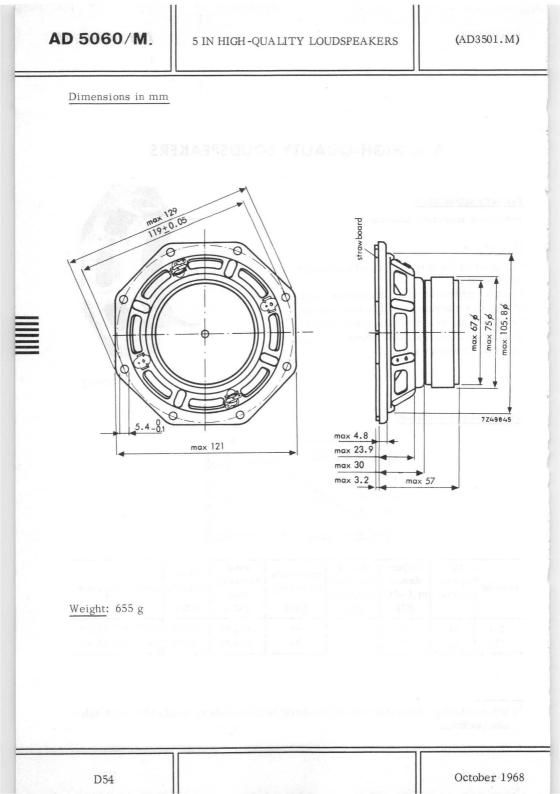
### Technical performance



version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number
M4	M	4	6	85	29 400	9800	2422 257 35101
M8	M	8	6	85	29 400	9800	2422 257 35102

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



(AD3503R) (AD3503S)

# AD 5060/ W4 AD 5060/ W8

### 5 in WOOFER LOUDSPEAKERS

#### Application

In very small acoustic enclosures; suitable for frequencies of 38 to 2000 Hz. See data sheet on the 10 W combination with tweeter AD2070/T in an acoustic box of 3 litres.

### Construction

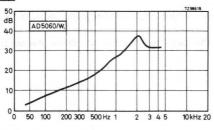
Round magnet of Ferroxdure 300R. Weight of magnet 260 g.

Constant flux through moving voice coil. Rigid paper cone with a highly flexible butyl-rubber suspension.



RZ 25052-32A

### Technical performance

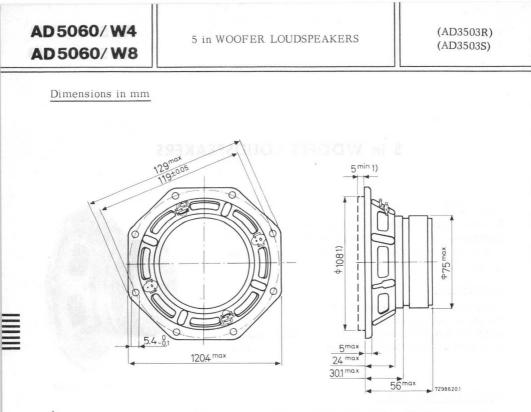


version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number 2)
W4	W	4	10 <sup>1</sup> )	50	39 000	> 9300	2422 257 35301
W8	W	8	10 <sup>1</sup> )	50	39 000	> 9300	2422 257 35302

1) In an acoustic enclosure of max. 3 litres, and conforming to DIN45573.

2) When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



<sup>1</sup>)Baffle hole and clearance depth required for cone movement at 10 W input.

A red mark near one of the tags serves for in-phase connection with other loud-speakers of our range.

Weight: 700 g

# 5 in STANDARD LOUDSPEAKERS

### Application

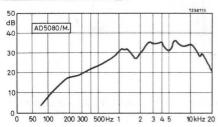
Radios (car and domestic), television sets, tape recorders, portable gramophones, intercoms.

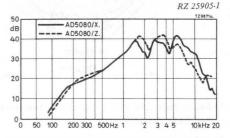
### Construction

Round magnet of Ferroxdure 300R. Magnet mass 100 g.



Technical performance



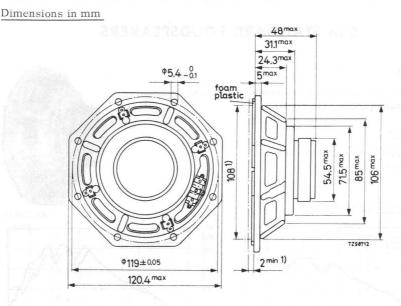


version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catal. number 2)
M4 M8 M15 M25	М	4 8 15 25	4 <sup>1</sup> )	130	18000	> 10 000	242225735209 11 12 13
X4 X8 X15 X25	X	4 8 15 25	6 <sup>1</sup> )	140	18000	> 10 000	2422 257 35205 06 07 08
Z4 Z8 Z15 Z25	Z	4 8 15 25	31)	155	18000	> 10 000	242225735201 02 03 04

<sup>1</sup>) Signal in conformity with DIN45573.

<sup>2</sup>) When ordering bulk packing add 20 to the last two digits; when ordering singleunit packing add 60 to the last two digits.

# AD 5080/M4 -AD 5080/Z25



 Baffle hole and clearance depth required for cone movement at the specified power handling capacity.

A red mark near one of the tags serves for in-phase connection with other loud-speakers of our range.

Weight: 260 g

# **5x7 in STANDARD LOUDSPEAKERS**

#### Application

Radios (car and domestic), television sets, portable gramophones, acoustic enclosures.

### Construction

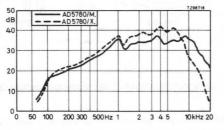
Round magnet of Ferroxdure 300R. Magnet mass 100 g.



AD5780/M4-AD5780/X25

RZ 25809-4

### Technical performance



version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catal. number 2)
M4	М	4	4 <sup>1</sup> )	100	17 500	> 9800	2722 257 36105
M8		8					06
M15		15					07
M25		25					08
X4	X	4	31)	115	17 500	> 9800	2722 257 36101
X8		8					02
X15		15					03
X25		25					04

<sup>1</sup>) Signal in conformity with DIN 45573.

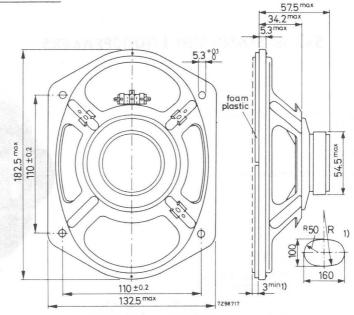
2) When ordering bulk packing add 20 to the last two digits; when ordering singleunit packing add 60 to the last two digits.

### 5x7 in STANDARD LOUDSPEAKERS

Dimensions in mm

AD5780/M4-

AD5780/ X25



 Baffle hole and clearance depth required for cone movement at the specified power handling capacity.

A red mark near one of the tags serves for in-phase connection with other loud-speakers of our range.

Weight: 320 g.

## AD 7060/M5

## **6½ in HIGH QUALITY LOUDSPEAKERS**

## Primary application

Technical performance

Small closed cabinets for monophonic and stereophonic reproduction. See "Recommended enclosures".

## Details

Hi-Fi reproduction over a very wide frequency range owing to the special double cone which has a very low resonance frequency and reproduces even the highest tones so as to ensure a true timbre.

Great power-handling capacity when placed in a closed cabinet having a volume of maximum 25 litres.

Very high sensitivity owing to the large annular Ferroxdure magnet.



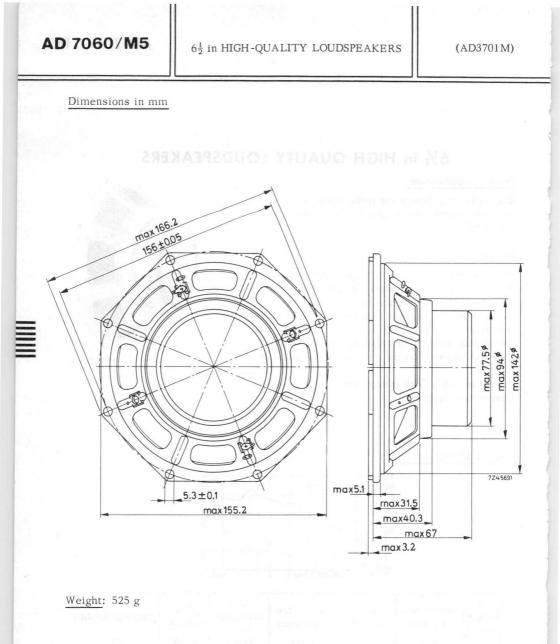
RZ 14210-9

## 50 dB 40 30 20 0 0 0 50 100 200 300 500 Hz 1 2 3 4 5 10 kHz 20

power handling capacity	impedance at 1 kHz	response curve	resonance frequency	total magnetic flux	flux density	catalog number
(W)	<b>(</b> Ω)		(Hz)	(Mx)	(Gs)	1)
10	5	М	55	42 600	9500	2422 257 37102

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968



(AD3703S)

# 6<sup>1</sup>/<sub>2</sub>" HIGH-QUALITY WOOFER LOUDSPEAKER

## Primary application

Small acoustic enclosures for low-note reproduction.

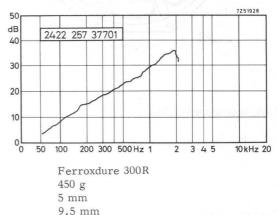
## Details

Very low resonance frequency, thanks to the rigid paper cone together with butyl-rubber cone rim. High flexible suspension of the cone, resulting in a sound reproduction with extremely low distortion, even at high powers.

Housed in a well damped acoustic box, even in a small volume of 9 litres, and in combination with the right loudspeaker for the medium and high-note reproduction <sup>1</sup>), this  $6\frac{1}{2}$  woofer loudspeaker meets the requirements of DIN 45500 (Hi-Fi) specifications.



RZ 23783-1



Material of magnet system Weight of magnet system Height of air gap Length of voice coil

Technical performance

power handling capacity (W)	nominal impedance (Ω)	response curve	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number <sup>3</sup> )
20 2)	8	W	28	45 000	9600	2422 257 37701

1) See data sheet "9 1 acoustic box for AD7065/W8 and AD5080/M4".

2) In an acoustic box of 30 litres or smaller conforming to the recommendations of DIN 45573, page 2.

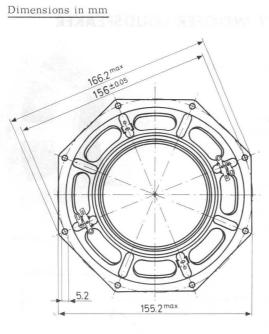
<sup>3</sup>) For bulk packing the catalog number is 2422 257 37721, for single-unit packing the catalog number is 2422 257 37761.

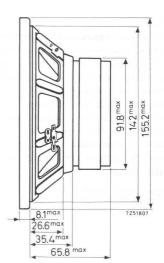
October 1968

# AD 7065/W8

## $6\frac{1}{2}$ " HIGH-QUALITY WOOFER LOUDSPEAKER

(AD3703S)





Baffle hole diameter 95 mm.

Weight: 1.2 kg

October 1968

# AD7080/M4-AD7080/X8

RZ 25905-5

# 6<sup>1</sup>/<sub>2</sub> in STANDARD LOUDSPEAKERS

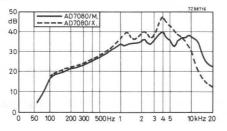
## Application

Radios (car and domestic), television sets, acoustic enclosures.

## Construction

Round magnet of Ferroxdure 300R. Magnet mass 100 g.

## Technical performance



version	re- sponse curve	nom. impe- dance (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catal. number 2)
M4 M8	М	4 8	4 <sup>1</sup> )	95	17 500	> 9800	2422 257 37803 04
X4 X8	X	4 8	6	110	17 500	> 9800	2422 257 37801 02

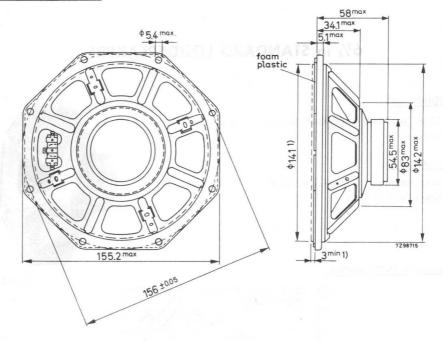
 $^1$ ) Signal in conformity with DIN45573.

<sup>2</sup>) When ordering bulk packing add 20 to the last two digits; when ordering singleunit packing add 60 to the last two digits.

September 1968



Dimensions in mm



1) Baffle hole and clearance depth required for cone movement at the specified power handling capacity.

A red mark near one of the tags serves for in-phase connection with other loudspeakers of our range.

Weight: 300 g

(AD3729..)

AD 7091/M4 -AD 7091/X800

## 6<sup>1</sup>/<sub>2</sub> in STANDARD LOUDSPEAKERS

#### Application

TV receivers.

## Construction

Small mounting depth as a result of the inverted construction.

High sensitivity owing to the use of a Ticonal 650 magnet.

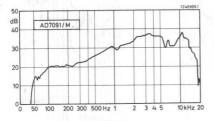
Absence of a stray field.

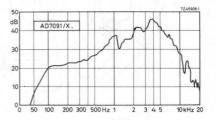
When the speakers, which are supplied in a plastic envelope, are built in, the front must be covered with a piece of muslin so as to prevent dust from entering the air gap.



RZ 19741-14

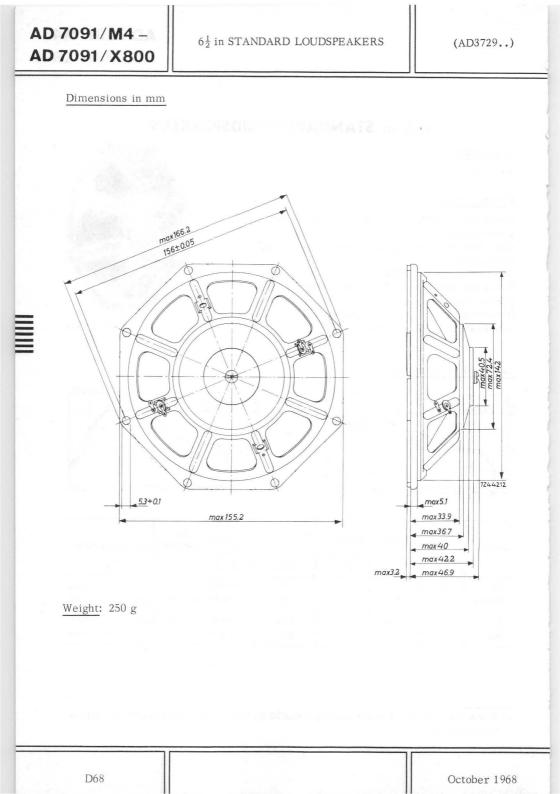
## Technical performance





version	re- sponse curve	impe- dance at 1 kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number l)
M4	M	4	3	95	18 900	7000	2422 256 37004
M800	M	800	3	95	18 900	7000	2422 256 37001
X4 X800	X X	4 800	3 3	100 100	18 900 18 900	7000 7000	2422 256 37005 2422 256 37002

## 1) When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.



(AD4800M)

## AD 8050/M5

# 8" HIGH-QUALITY LOUDSPEAKERS

## Primary application

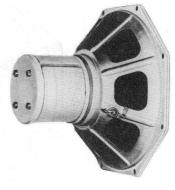
Hi-Fi and stereo equipment. See "Recommended enclosures"

## Details

High sensitivity, Ticonal magnet.

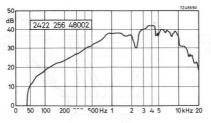
When these speakers are placed in an acoustic box or any other suitable enclosure, their sensitivity and response qualities result in an almost constant sound pressure over the entire audible frequency range.

Practically undistorted sound reproduction.



A 46102

## Technical performance



power handling capacity (W)	impedance at 1 kHz (Ω)	response curve	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number
6	5	М	60	58 300	13 000	2422 256 48002

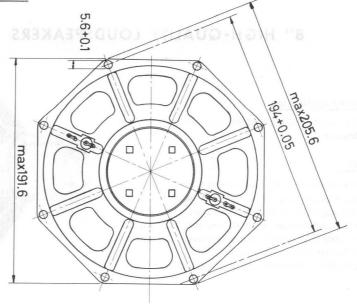
 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

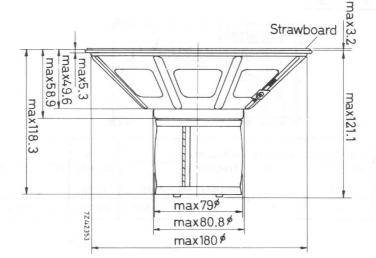
October 1968

AD 8050/M5

(AD4800M)

## Dimensions in mm







October 1968

## AD8065/W8

# 8 in HIGH-QUALITY WOOFER LOUDSPEAKER

## Application

In small acoustic enclosures for Hi-Fi reproduction; suitable for frequencies of 22 to 1800 Hz. See data sheet on the 20 W combination with AD5780/M4 in an acoustic box of 15 litres.

### Construction

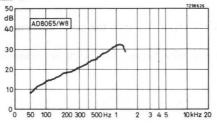
Round magnet of Ferroxdure 300 R. Weight of magnet 450 g. Constant flux through moving voice coil, resulting in a low distortion.

Rigid paper cone with highly flexible butyl-rubber suspension.



RZ 24709-5

## Technical performance



version	re- sponse	nom. impe- dance	power handling capacity	resonance frequency	total magnetic flux	flux density	catalog number
	curve	<b>(</b> Ω <b>)</b>	(W)	(Hz)	(Mx)	(Gs)	2)
W8	W	8	20 <sup>1</sup> )	28	45000	> 9000	2422 257 38101

 $^{\rm l}$  ) In an acoustic enclosure of max. 15 litres, and conforming to DIN45573.

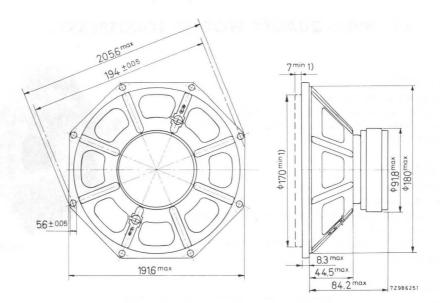
<sup>2</sup>) For bulk packing the catalog number is 2422 257 38121, for single-unit packing 2422 257 38161.

October 1968



(AD3803S)

Dimensions in mm



<sup>1</sup>) Baffle hole and clearance depth required for cone movement at 20 W input.

A red mark near one of the tags serves for in-phase connection with other loud-speakers of our range.

Weight: 1.35 kg

# 9710 M/01 9710 AM/01

## 8<sup>1</sup>/<sub>2</sub>" HIGH-QUALITY LOUDSPEAKERS

#### Primary application

Hi-Fi equipment. See "Recommended enclosures".

## Details

High sensitivity, Ticonal magnet.

Particularly large air gap, resulting in the voice coil being completely enclosed by a uniform magnetic field even at the largest amplitudes. No distortion will thus be experienced as the coil amplitude is disproportional to the current. Constant voice-coil impedance throughout the entire frequency range, so that the output stage always has a perfectly matched load.

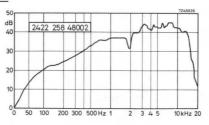
Very smooth response curve.

Clear bass response without boom effects, because of mechanical damping at low frequencies.



C 65233

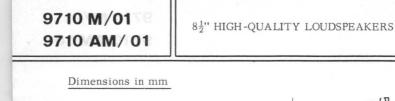
### Technical performance

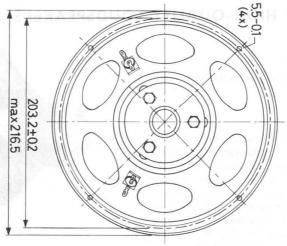


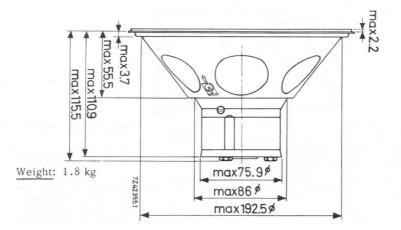
version	re- sponse curve	impe- dance at l kHz (Ω)	power handling capacity (W)	resonance frequency (Hz)	total magnetic flux (Mx)	flux density (Gs)	catalog number l)
M/01	M	7	10	50	98 000	8000	2422 258 48002
AM/01	M	800	10	50	98 000	8000	2422 258 48004

 When ordering, the last but one digit should be 2 for bulk packing and 6 for singleunit packing.

October 1968







## GENERAL

#### INTRODUCTION

On the following pages drawings are shown of enclosures which will give good results when used in combination with the indicated loudspeaker types. We distinguish standard class and high-fidelity class combinations.

#### Standard class

In some of the combinations of standard quality, less expensive standard loudspeakers are employed, and the acoustic boxes can in general be made cheaply by the user himself. Yet, used in conjunction with a good radio, tape recorder or record player with amplifier, the enclosures will give the builder much pleasure because of their good quality of reproduction.

## High-fidelity class

Combinations of this class have an exceptional performance thanks to the use of high-quality loudspeakers. Users are recommended to employ hi-fi equipment for best results.

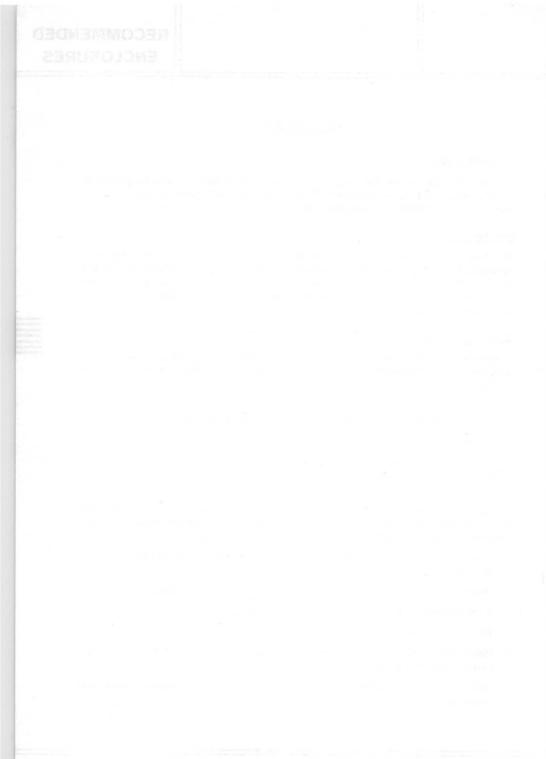
### POINTS TO OBSERVE WHEN ASSEMBLING ACOUSTIC BOXES

All boxes are built up of three mains parts:

- a front panel (1)
- four side panels, fastened together (2)
- a rear panel (3).

These components can be screwed together. Of course, the handy man may well decide to join the front panel and the four side panels together in his own way. He should, however, remember the following pieces of advice:

- 1. Use strong and rigid material for the sides, preferably multi-layer plywood or chipboard.
- 2. Minimum wall thickness is indicated on the Installation drawings.
- 3. A suitable damping lining must be provided, e.g. cotton wool 2 cm thick.
- 4. The enclosure must be acoustically sealed.
- 5. Make sure that the loudspeaker is properly fastened and that there are no loose component parts.
- 6. Make sure to use suitable loudspeaker cloth because otherwise the sound might be muffled.

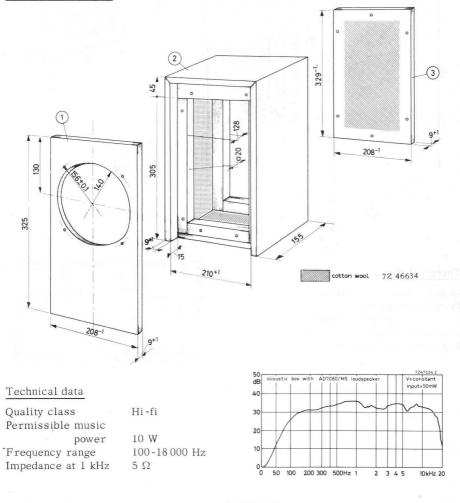




# ACOUSTIC BOX FOR 61/2" LOUDSPEAKER

This enclosure can be built for loudspeaker AD7060/M5 (AD3701M).

Installation drawing (dimensions in mm)

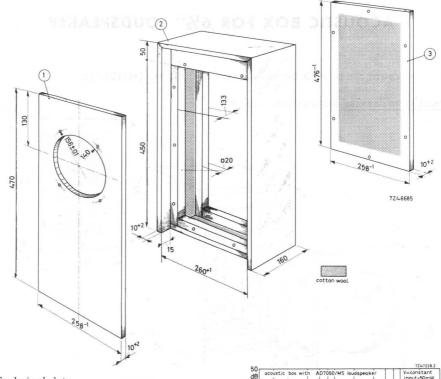


October 1968

ACOUSTIC BOX FOR  $6\frac{1}{2}$ " LOUDSPEAKER

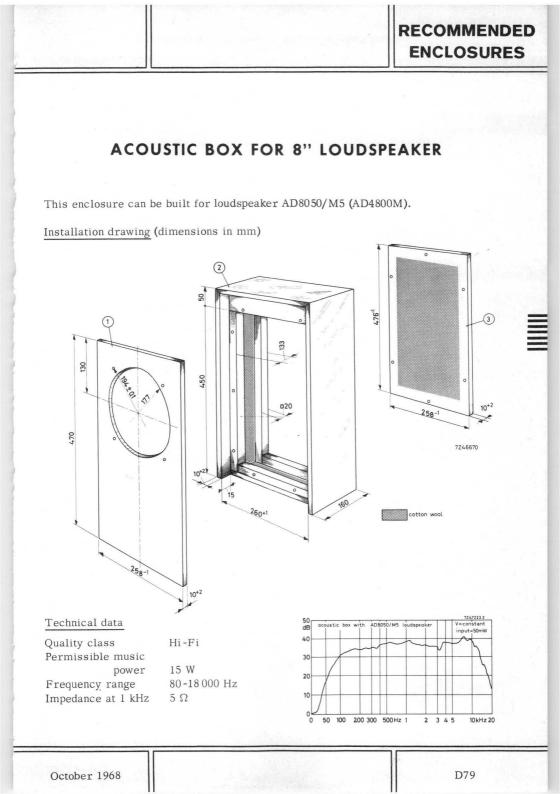
This enclosure can be built for loudspeaker AD7060/M5 (AD3701M).

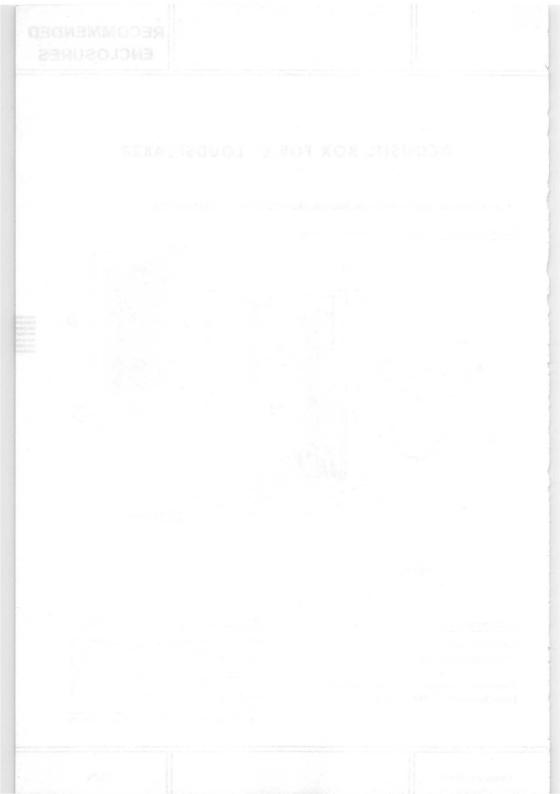
Installation drawing (dimentions in mm)



## Technical data

Quality class	Hi-fi
Permissible music	
power	10 W
Frequency range	70-18000 Hz
Impedance at 1 kHz	5 Ω





# 3 | ACOUSTIC BOX FOR AD5060/W. AND AD2070/T.

This box can be built for the 5 in woofer AD5060/W4 or /W8 and the  $2\frac{1}{4}$  in tweeter AD2070/T4 or T8. Main properties: max. 10 W; 90-20000 Hz; simple filter.

Nett volume	3 litres
Wall thickness	min. 7 mm
Damping	5 cm damping material against the back panel
Eastoning of the papels	with glue baffle with screws

Fastening of the panels

Constructional data

with glue, baffle with screws

Both loudspeakers to be mounted behind the baffle, the tweeter acoustically sealed off from the woofer.

The clearance depth for the woofer's cone movement falls within baffle thickness.

Baffle holes

diameters 108 mm and 52 mm, centre to centre distance min. 98 mm

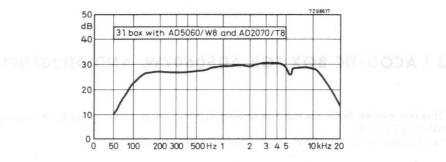
## Electrical and acoustical data

Power handling capacity (DIN 45573)	10 W
Frequency range (DIN 45500, Blatt 7)	90-20000 Hz
Cross-over filter	1 mH in series with the woofer 5 $\mu F$ in series with the tweeter
Cross-over frequency	2000 Hz
Resonance frequency	110 Hz
Nominal impedance	$4~\Omega$ or $8~\Omega$
Sensitivity: input power for an average sound level of 86 dB (4 $\mu$ bar) over 50-12500 Hz at 3 m distance from the	

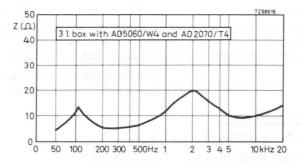
8 W

box

# 3 1 ACOUSTIC BOX FOR AD5060/W AND AD2070/T

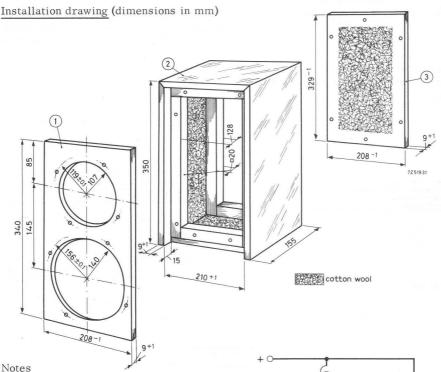


0 dB corresponds with 52 dB above  $2x10^{-4} \mu bar$  V = constant; input = 50 mW at 400 Hz; microphone at 50 cm



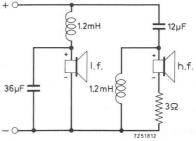
## 9 | ACOUSTIC BOX FOR AD7065/W8 AND AD5080/M4

This box can be built for the  $6\frac{1}{2}$  in woofer AD7065/W8 and the 5 in loudspeaker AD5080/M4. (Instead of the 5 in loudspeaker, the 4 in tweeter AD4490/T4 can be used) Main properties: max. 20 W; 50-18000 Hz; filter available.



The 5" loudspeaker must be acoustically sealed off from the remainder of the enclosure.

The use of the cross-over filter, given in the adjacent figure, is recommended. This filter has its cross-over frequency at 850 Hz; it can be ordered under the catalog number 4304 078 71330.



RECOMMENDED **ENCLOSURES** 

## 9 1 ACOUSTIC BOX FOR AD7065/W8 AND AD5080/M4

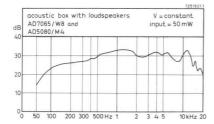
## TECHNICAL DATA

Quality class Nett volume Permissible music power Frequency range

Resonance frequency Impedance Sensitivity, measured at a distance of 3 m from the acoustic box

Distortion, measured at an average sound level of 86 dB, in the frequency range

250 - 1000 Hz 1000 - 2000 Hz 2000 - 18000 Hz



Hi-fi; in conformity with DIN 45500 (page 7) 9 litres

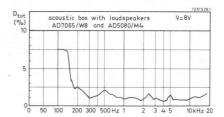
20 W; in conformity with DIN 45573 (page 2) 50-18 000 Hz; in conformity with DIN 45500 (page 7)

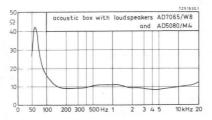
60 Hz

8Ω

at an input of 8 W the average sound level over the frequency range  $50-12\,500$  Hz is 86 dB (4  $\mu$ bar); in conformity with DIN 45500 (page 7)

< 3% from 3 to 1% decreasing continually < 1%





. Note: The sensitivity at frequencies from  $1.5\,\rm kHz$  upwards will be about 3 dB higher, if the M8 version of the 5" loudspeaker is used, and the 3  $\Omega$  resistor in the cross-over filter is short-circuited.

# 15 I ACOUSTIC BOX FOR AD8065/W8 AND AD3576RM

This box can be built for the 8 in woofer AD8065/W8 and the 5x7 in loudspeaker AD3576RM (or AD5780/M4).

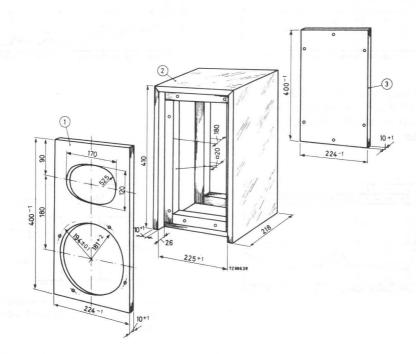
Main properties: max. 20 W; 50-16000 Hz; filter available.

## Constructional data

Nett volume Inside height x width x depth Wall thickness Damping 15 litres
400x225x180 mm
10 mm (minimum)
5 cm damping material against the back
panel

RECOMMENDED ENCLOSURES

Both loudspeakers to be mounted against front of baffle, the AD3576RM acoustically sealed off from the remainder of the compartment.



Installation drawing (dimensions in mm)

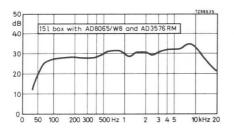
## Electrical and acoustical data

Power handling capacity (DIN 45573) Frequency range (DIN 45500, Blatt 7) Cross-over filter Cross-over frequency Resonance frequency Nominal impedance Sensitivity: input power for an average sound level of 86 dB (4  $\mu$ b) over 50-12 500 Hz at 3 m from the box Distortion, measured at an average sound level of 86 dB

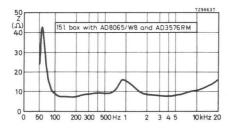
20 W 50-16 000 Hz catalog number 4304 078 71330 850 Hz 55 Hz 8 Ω

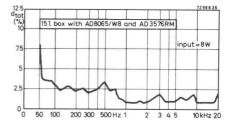
### 8 W

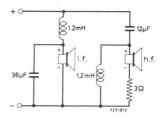
conforms to DIN 45500, Blatt 7; see curve.



0 dB corresponds with 52 dB above 2 x  $10^{-4} \mu b$  V = constant; input = 50 mW at 400 Hz; microphone at 50 cm







Circuit diagram of cross-over filter 4304 078 71330 and loudspeakers

# 35 I ACOUSTIC BOX FOR AD1055/W8, AD5060/M8 AND AD3506SM

This box can be built for the 10 in woofer AD1055/W8, the 5 in loudspeaker AD5060/M8 (AD3501SM) for the medium notes and the 5 in loudspeaker AD3506SM or AD5080/M8 for the high notes. Main properties: max. 40 W; 40-20000 Hz

Constructional data

Nett volume

351

Wall thickness

Damping

box entirely filled with damping material

min. 13 mm

Mounting of the loudspeakers

behind baffle, each fixed by 8 screws. The AD5060/M8 and the AD3506SM should be acoustically sealed off from the woofer.

Baffle hole diameters

227 mm, 105 mm and 105 mm

The clearance depth for the woofer's cone movement falls within the baffle thickness.

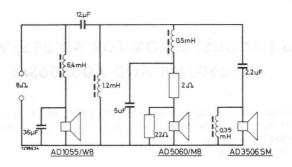
Electrical and acoustical data

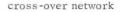
Power handling capacity (DIN 45573)	40 W
Frequency range (DIN 45500, Blatt 7)	40-20000 Hz
Cross-over network	see below
Cross-over frequencies	500 Hz and 4000 Hz
Resonance frequency	48 Hz
Nominal impedance	8 Ω
Sensitivity; input power for an average sound level of 86 dB (4 $\mu b$ )	
over 50-12 500 Hz at 3 m from the box	8 W

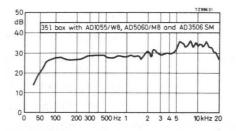
Distortion, measured at an average sound level of 86 dB

conforms to DIN 45500, Blatt 7; see curve

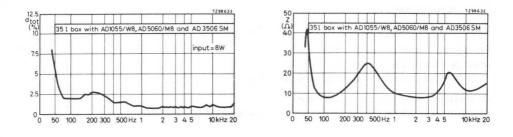
## 35 1 ACOUSTIC BOX FOR AD1055/W8, AD5060/M8 AND AD3506SM







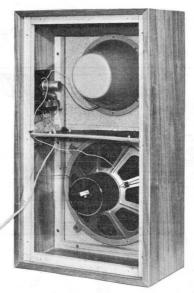
0 dB corresponds with 52 dB above 2 x  $10^{-4} \mu$ bar. V = constant; input = 50 mW at 400 Hz; microphone at 50 cm



April 1968

# 45 | ACOUSTIC BOX FOR AD1255/W8 AND 9710/01

This enclosure can be built for the high-quality loudspeakers 9710M/01 and the AD1255/W8 (AD5201S/77). This is a combination of one of the best middle and high-note loudspeakers and that remarkable woofer (also called "Bombardon") which has a resonance frequency of 29 Hz.

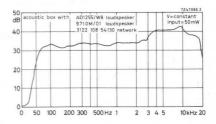


RZ 20890-9

Rear view, box opened; top loudspeaker enclosed in plastic pot.

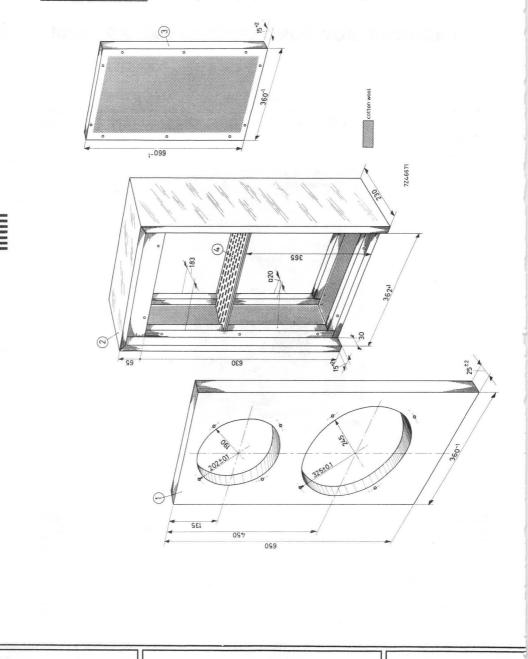
#### Technical data

Quality classHi-fiPermissible musicpowerpower40 WFrequency range40-18 000 HzImpedance at 1 kHz7 Ω



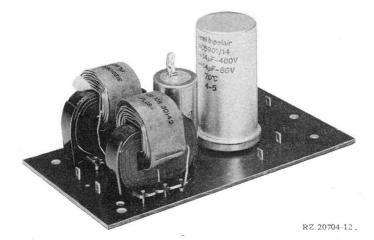
October 1968

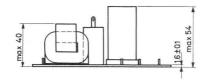
Installation drawing (without plastic pot, dimensions in mm)

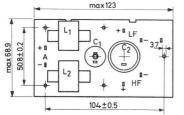


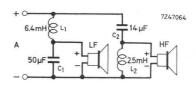
## Notes

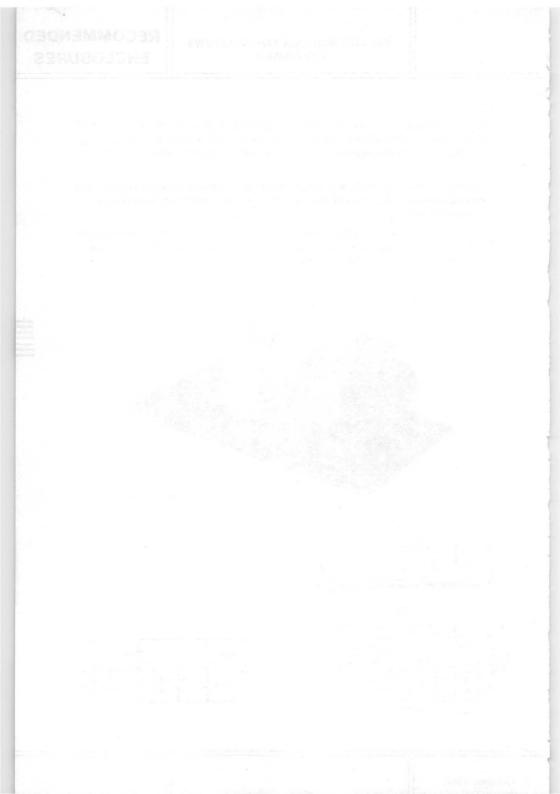
- 1. The top loudspeaker must be acoustically sealed off from the remainder of the enclosure, otherwise it will affect the reproduction quality of the low-tone loudspeaker. The polystyrene pot is not available, a cubic wooden enclosure is a good alternative.
- 2. For proper damping of the low tones, a partition must be placed between the two loudspeakers; this should be made from a perforated plate covered by two layers of flannel.
- 3. The use of a cross-over filter is recommended. The one shown below has its cross-over frequency at 450 Hz and a rate of attenuation of 12 dB per octave; it can be ordered under No.3122 108 54130.



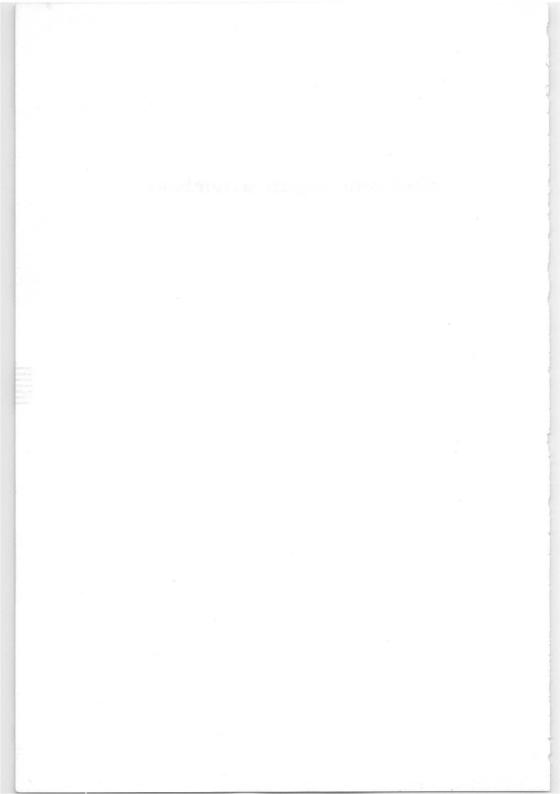








Electronic organ assemblies



## INTRODUCTION

As the only supplier of a complete range of assemblies for electronic church and concert organs, we are aware of special responsibilities. Not only must the units be exceptionally well designed and constructed but also, as a range, permit of infinite variety in their end product - the electronic organ. Further, our customers must be confident of a prompt and continuing supply and of first-class technical assistance. These we guarantee.

We recognize that voicing an organ is a matter of personal taste and are therefore unwilling to inflict our taste on an organ-builder. We supply basic functions that for the most part only need interconnecting, and leave the organ-builder free to develop his taste in voicing, number of key-boards, number and kind of stops, sound character etc.

To this end the transistorised units are complete in themselves and pose no technical problems for the user. By adding equalizing networks and formant circuits, the organ-builder can voice an organ to his or his customer's needs. We can advise on the choice of networks as we can on any other aspect of building electronic organs for churches or concert-halls.

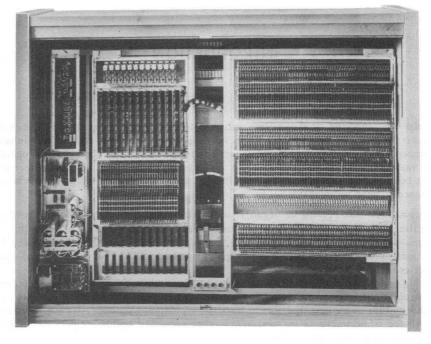
Although the electronic organs built with our assemblies are much cheaper than equivalent pipe-organs of the same scope, we can truthfully say that it is very difficult to distinguish their sound characters from those of pipe-organs.

Our Instruction Manual 'Electronic Organ Assemblies' is available to electronic organ builders; it gives details of how to use our assemblies to the best advantage. As an example we describe the construction of a two manual, full pedal, organ of twenty-one stops; this is just an example, organs built withour assemblies can have any number of keyboards, any number of stops, and can be given the voicing and character that suits the individual builder and his customers.

Do not hesitate to consult us; we are happy to advise on any aspect of the design and construction of electronic organs of professional standing.



INTRODUCTION



Typical layout for a small (2 manual) organ.

A 51473

noise	oscillator unit		
+ choir	frequency divider	manual II unit	
effect unit	unit	manual I unit	
	pedal unit		
power		mixture pre-stage unit	
supplies	register unit 1		
	register unit 2	mixture unit	

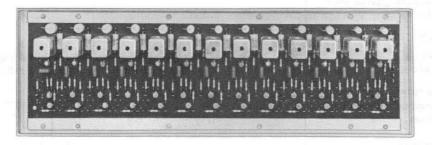
Block diagram of above organ.

October 1968

E4

# 4322 026 37640

# SET OF 12 + 1 OSCILLATORS



## DESCRIPTION

This unit contains 13 oscillator circuits for the frequencies between 4096 Hz and 8192 Hz, spaced in 12 steps according to the equal tempered scale.

The frequencies are generated as sine waves, but converted to square waves to drive the frequency dividers and to feed the input of the gating circuits of the highest octave. The inductance in each oscillator circuit can be fine tuned within a range of at least 250 Hz above and below the nominal frequency.

## MECHANICAL AND ENVIRONMENTAL DATA

Overall dimensions	396 mm x 123 mm x 45 mm
Weight	800 g
Ambient temperature range	
storage :	-20 °C to +70 °C
operating:	+5 °C to +50 °C
Max. relative humidity	80%

#### ELECTRICAL DATA

Note: A positive current value indicates a current flowing toward the circuit.

Power supply	$V_P = +6V \pm 10\%$ ; $I_P = 18 \text{ mA}$
	$V_{\rm N}$ = -6V ± 10%; $I_{\rm N}$ = -22 mA
Frequency range	4096 Hz to 8192 Hz in 12 steps
	according to equal tempered scale
Frequency adjustment	$\pm$ 250 Hz per oscillator
Stability/temperature	$\leq 0.1 \% / ^{\circ}C$

RZ 23681-19

# 4322 026 37640

## SET OF 12 + 1 OSCILLATORS

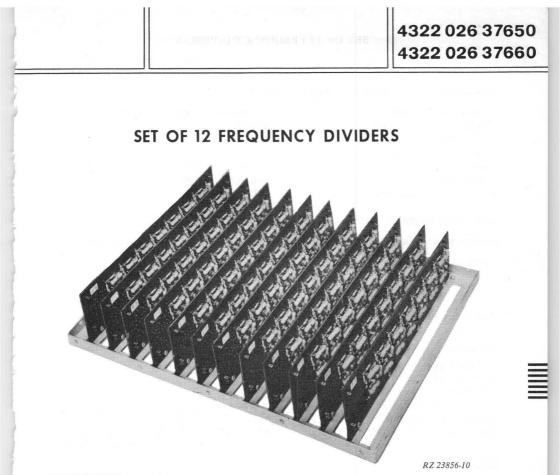
Output data	at collector	at emitter
Output level "negative low"		
voltage load current transient charge over	-V = max0.25V <sub>N</sub> -I = max. 0.9 mA	max0.01V <sub>N</sub> max. 0.08 mA
3 V in 1 μs	2.5 nC	
Output level "negative high"		
voltage load current	-V = min0.95V <sub>N</sub> +I = max. 0.03 mA	min0.17V <sub>N</sub> max. 0.1 mA
Rise time trigger edge	$t_r = max. 1 \mu s$	
Tolerance between half pulse periods	$t_1/t_2 = 0.7 \text{ to } 1.3$	
Input data		t <sub>1</sub> t <sub>2</sub> 7253290
From noise and choir effect unit:		

voltage min. 1 current max.

min. 1 V<sub>p-p</sub> max. 0.5 mA<sub>p-p</sub>

October 1968

E6



#### DESCRIPTION

The frequency dividers are a series of transistor flip-flops, each stage being triggered by the preceding, or in the case of the first stage, by the master oscillators. The set comprises twelve sub-units, each responsible for one note of the octave, and containing seven or eight stages. The first stage halves the frequency of the associated oscillator to give a note of the  $c_4$  octave, the second stage for the  $c_3$  octave, and so on down to the contra octave, or in the case of an eight stage divider the sub contra. Both seven and eight stage dividers are standard, the last named being needed if a 32' pitch is included in the pedal unit.

> Catalogue number 7 stages: 4322 026 37650 Catalogue number 8 stages: 4322 026 37660

# 4322 026 37650 4322 026 37660

## SET OF 12 FREQUENCY DIVIDERS

#### MECHANICAL AND ENVIRONMENTAL DATA

Overall dimensions	396 mm x 289 mm x 75 mm
Weight 7-stage version	2100 g
8-stage version	2150 g
Ambient temperature range	
storage :	-20 °C to +70 °C
operating:	+5 °C to +50 °C
Max. relative humidity	80%

#### ELECTRICAL DATA

Note: A positive current value indicates a current flowing toward the circuit.

Power supply 7-stage version

8-stage version

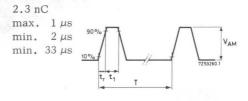
Frequency range

Input data

Voltage  $V_{AM}$ Transient charge over 3 V in 1  $\mu$ s Rise time trigger edge  $t_r$ Length of driving pulse  $t_1$ Time between two pulses T

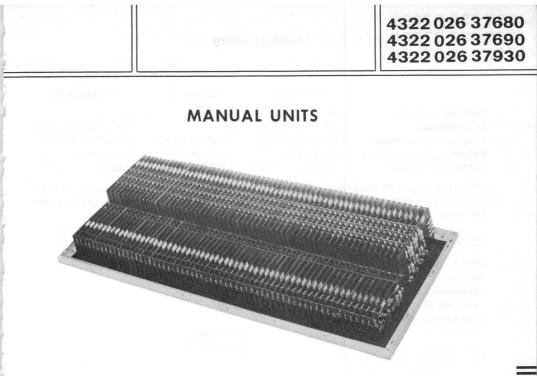
Output data

Output level "negative low" voltage load current Output level "negative high" voltage load current min.  $-0.7V_N$ ; max.  $-0.85V_N$ 



-V = max. 0.2 V +I<sub>O</sub> = max. 0 mA

 $-V = min. -0.15V_N$  $+I_O = max. 0.1 mA$ 



#### DESCRIPTION

RZ 23856-5

In design and print-lay-out the three versions are identical, they differ only in the facilities provided.

The main printed wiring board carries 61 sub-units, each sub-unit being connected to a particular key on the keyboard. The sub-units are in two parts: one having provision for 5 gates to control the admission of tones to the stop circuits; the other having a network to delay the response of certain pitches, plus facilities to insert wind-noise and gate the chiff.

Each gate controls a particular pitch and can have two outputs, a saw-tooth for the open diapason and reed characters, and a square wave for the flute stops.

When a key is depressed, all associated gates are opened and all outputs are admitted to the stop circuits, where the stop switches determine which output shall become audible. The outputs are fed to the stop-circuits via equalising networks that over the full compass of the keyboard pre-shape the tone to the main characters, so that a single voicing network in each stop circuit can determine the specific character of the individual voices.

In the second part of the sub-units, three networks are shared among the five pitches to delay the gating of a note for a specific period depending on its pitch. The same unit also gates the two chiff frequencies, obtained by strapping the chiff input to a selected output of the frequency dividers. The chiff frequency will be heard in advance of the note played, in the same way that partials precede the fundamental in pipe organs.

Versions I and II are not fully equipped as far as the gating circuits are concerned experience having shown that the majority of organs do not need all the facilities available. Version III is fully equipped.

# 4322 026 37680 4322 026 37690 4322 026 37930

MANUAL UNITS

Version I	Version II	Version III
4	4	5
	8'	16'-8'-4'-2'-2 <sup>2</sup> /3'
8'-4'-2'-22/3'	8'-4'-2'-2 <sup>2</sup> /3'	16'-8'-4'-2'-2 <sup>2</sup> /3'
8'-4'-22/3'	8'-4'-2'	16'-8'-4'-2'-22/3'
4322 026 37680	4322 026 37690	4322 026 37930
	4 8'-4'-2'-22/3' 8'-4'-2'-22/3' 8'-4'-22/3'	$\begin{array}{ccccccc} 4 & & & 4 \\ 8'-4'-2'-2^2/3' & & 8' \\ 8'-4'-2'-2^2/3' & & 8'-4'-2'-2^2/3' \\ 8'-4'-2^2/3' & & 8'-4'-2' \end{array}$

All versions can be used for pitches one octave higher than those designated, this is of greatest interest for version III. This unit is so versatile as to be suited to any keyboard - great organ, swell organ, solo organ, etc.

## MECHANICAL AND ENVIRONMENTAL DATA

Overall dimensions	671 mm x 276 mm x 75 mm
Weight	
versions I and II	5200 g
version III	5500 g
Ambient temperature range	
storage :	-20 to +70 °C
operating:	+5 to +50 °C
Max. relative humidity	80%

#### ELECTRICAL DATA

Note: A positive current value indicates a current flowing toward the circuit.

#### Gating circuits

Power supply

 $V_{\rm N}$  = -6 V  $\pm$  10%  $I_{\rm N}$  = -0.7 mA for each gate

## Input data for each gate

Output level "negative low"		
voltage	$-V_{G} = min0.15V_{N}$	max V <sub>N</sub>
current	$-I_{G} = max. 0.014 \text{ mA}$ (at V	$V_{\rm G} = 0.15 V_{\rm N}$ )
Output level "negative high"		0
voltage	$-V_{G} = max. 0.2 V$	min. 0 V

## MANUAL UNITS

# 4322 026 37680 4322 026 37690 4322 026 37930

Output data

Output level "negative low"

Output level "negative high"

square wave output	saw-tooth output
$-V = maxV_N - \Delta V$	max. 0 V
$\Delta V = \frac{4.4}{62 - n} V$ (n = number of operated keys)	
$-V = -V_N$	$-V = min. 0 - \Delta V$
	$\Delta V = \frac{3}{62 - n} V$ (n = number of operated keys)

RC time delay circuits

Power supply

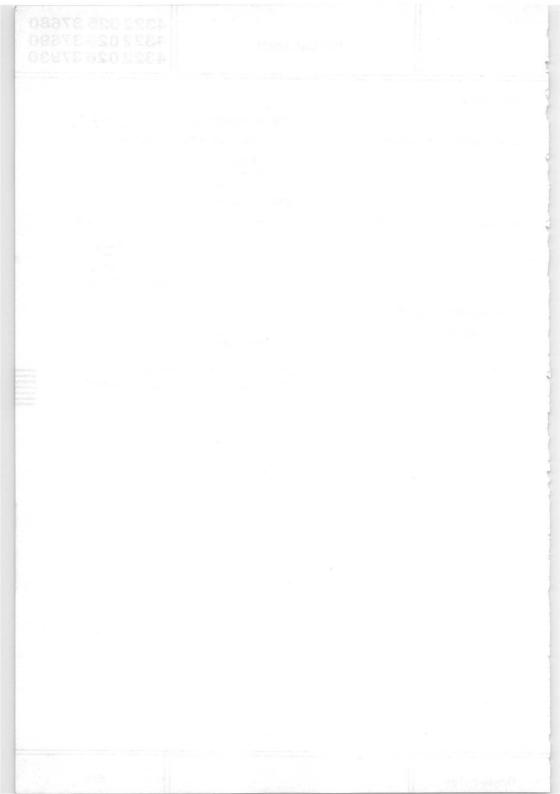
Time delays

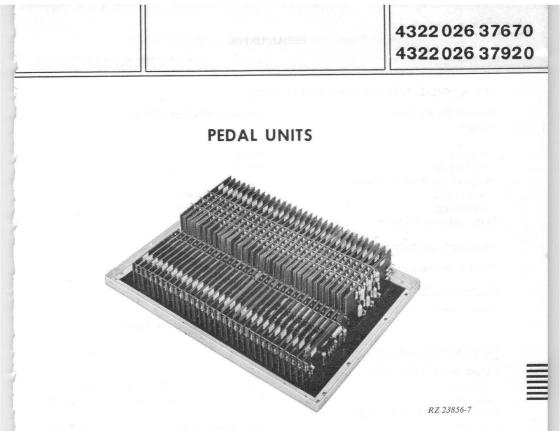
 $V_{\rm N}$  = -1.5 V ± 10%  $I_{\rm N}$  = -0.5 mA

between 2 ms and 25 ms (approx., depending on pitch and position in unit)

October 1968

E11





## DESCRIPTION

This unit is identical to the manual units as far as functions are concerned. The main printed-wiring board, however, has only 32 sub-units (each in two parts) corresponding to the number of keys in the pedal.

In version I the first part of the sub-units is equipped with only three gating circuits, each with both square wave and saw-tooth wave outputs, for the pitches 16', 8' and 4'. The second part of each sub-unit has 2 delay circuits and one gating circuit for the chiff frequency (instead of three and two as on the manual units). Version II is fully equipped.

	Version I	Version II		
Number of gates Gate-pitches Outputs square wave Outputs saw-tooth wave Catalogue number	3 16' - 8' - 4' 16' - 8' - 4' 16' - 8' - 4' 4322 026 37670	5 32' - 16' - 8' - 4' - 5 <sup>1</sup> /3' 32' - 16' - 8' - 4' - 5 <sup>1</sup> /3' 32' - 16' - 8' - 4' - 5 <sup>1</sup> /3' 4322 026 37920		
U				

# 432202637670 432202637920

#### PEDAL UNITS

#### MECHANICAL AND ENVIRONMENTAL DATA

Overall dimensions Weight	396 mm x 276 mm x 75
version I	2800 g
version II	2900 g
Ambient temperature range	
storage :	-20 °C to +70 °C
operating:	+5 °C to +50 °C
Max. relative humidity	80%

## ELECTRICAL DATA

Note: A positive current value indicates a current flowing toward the circuit.

#### Gating circuits

Power supply

 $V_N$  = -6 V ± 10% I<sub>N</sub> = -0.7 mA for each gate

Input data for each gate
Output level "negative low"
voltage
current
Output level "negative high"
voltage

-VG	Ξ	min.	-0.15	VN	; ma	ax.	-V	V	
			0.014						V <sub>N</sub> )

mm

 $-V_{G} = \max. 0.2 V$  min. 0 V

Output data

Output level "negative low"

Output level "negative high"

square wave output	saw-tooth output
$-V = maxV_N - \Delta V$	max. 0 V
$\Delta V = \frac{4.4}{33 - n} V$ (n = number of operated keys)	
$-V = -V_N$	$-V = \min. 0 - \Delta V$
	$\Delta V = \frac{3}{33 - n} V$ (n = number of operated keys)

#### RC time delay circuits

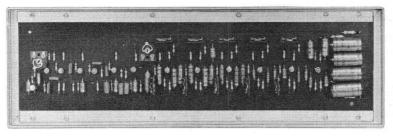
Power supply

Time delays

 $V_N$  = -1.5 V  $\pm$  10%  $I_N$  = -0.5 mA between 8 ms and 50 ms (nominal)

E14

## NOISE GENERATOR AND CHOIR-EFFECT UNIT



RZ 23681-21

#### DESCRIPTION

The noise and choir-effect circuits are combined on a single printed wiring board. The noise generator provides the background hiss that simulates the wind-noise of a pipe-organ, and is fed to the manual and pedal gating circuits via the resistor/ capacitor time delay circuits.

The choir-effect unit consists of 5 individual oscillators with separately adjustable frequencies and amplitudes; these are fed to the master oscillators, where they randomly modulate the generated frequencies to prevent over-purity of tone. The third oscillator can be used as tremulant if required.

Catalogue number: 4322 026 37730

#### MECHANICAL AND ENVIRONMENTAL DATA

Overall dimensions396 mm x 123 mm x 25 mmWeight700 gAmbient temperature range-20 °C to +70 °Cstorage :-20 °C to +70 °Coperating:+5 °C to +50 °CMax. relative humidity80%

# 4322 026 37730

## NOISE GENERATOR AND CHOIR-EFFECT UNIT

#### ELECTRICAL DATA

Note: A positive current value indicates a current flowing toward the circuit.

Power supply

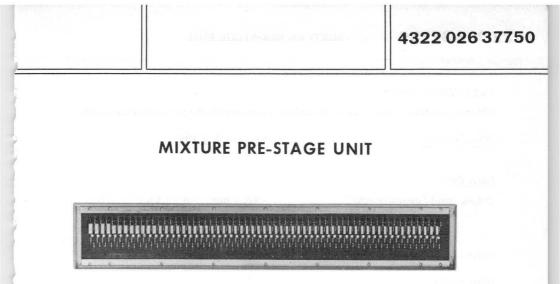
Noise generator

Noise frequency band Noise amplitude  $V_P = +6 V \pm 10\%$ ;  $I_P = 16 mA$  $V_N = -6 V \pm 10\%$ ;  $I_N = -16 mA$ 

20 kHz at least adjustable between 0 and 300 mV loaded with two manual and one pedal units

Choir-effect unit

Adjustable frequency range Output voltage Output current between 0.5 Hz and 10 Hz min. 2 Vp-p max. 1.5 mAp-p



RZ 23681-17

This unit consists of  $61\ {\rm separate}\ {\rm stages}\ {\rm each}\ {\rm shaping}\ {\rm a}\ {\rm particular}\ {\rm frequency}\ {\rm for}\ {\rm the}\ {\rm main}\ {\rm mixture}\ {\rm unit}\ .$ 

The inputs are square waves direct from the master oscillators and frequency dividers; the frequencies used depend upon the type of mixture or cymbal to be constructed (based on 2' and  $\frac{1}{2}$ ' or  $1^{1}/3$ ' and 1/3' etc.) The outputs are saw-tooth waveforms to suit the open diapason character of the mixture stops.

Catalogue number: 4322 026 37750

#### MECHANICAL AND ENVIRONMENTAL DATA

Overall dimensions Weight Ambient temperature range storage : operating: Max. relative humidity 671 mm x 114 mm x 15 mm 1050 g

-20 °C to +70 °C +5 °C to +50 °C 80%

# 4322 026 37750

#### MIXTURE PRE-STAGE UNIT

#### ELECTRICAL DATA

Note: A positive current value indicates a current flowing toward the circuit.

Power supply

Input data

Output level "negative low"

 $V_{\rm N} = -6 V \pm 10\%$  $I_{\rm N} = -85 \text{ mA}$ 

 $\begin{array}{l} -V_{G} = \min. \ -0.15 \ V_{N} \\ = \max. \ -V_{N} \\ -I_{G} = \max. \ 0.05 \ \text{mA} \ (\text{per stage} \\ \text{at } V_{G} = 0.15 \ V_{N}) \\ -V_{G} = \min. \ 0 \ V \ \max. \ 0.2 \ V \end{array}$ 

Output level "negative high"

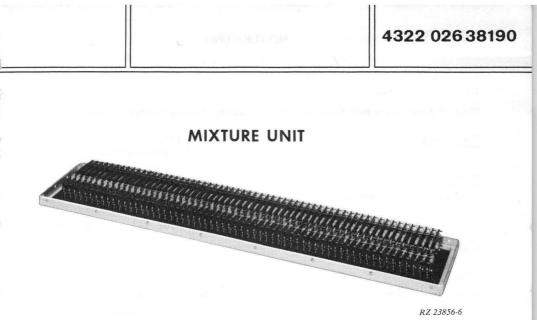
Output data

Output level "negative low"

Output level "negative high"

 $-V_Q$  = min. 0 V

 $-V_Q = min. -0.15 V_N$ + $I_O = max. 0.03 mA (per stage)$ 



#### DESCRIPTION

This unit has 61 separate sub-units (one per key on the keyboard) each of which has two circuits, a four-input and a three-input mixture. The mixtures are quite separate, generally they are gated from different keyboards. If desired the outputs can be strapped to form chords of up to seven notes. The gates must then be strapped as well.

The unit is so arranged that, by mixing outputs from the pre-stage, the organ buildder can construct chords to suit his own taste.

Although the stages are basically similar, there are differences in component values along the keyboard, to compensate for the frequency dependence of the ear's sensitivity, and to meet specific voicing requirements. No equalising networks are needed, just a single voicing network in the stop circuits.

Catalogue number: 4322 026 38190

#### MECHANICAL AND ENVIRONMENTAL DATA

Overall dimensions	671 mm x 143 mm x 38 mm
Weight	1800 g
Ambient temperature range	
storage	-20 °C to +70 °C
operating	+5 °C to +50 °C
Max. relative humidity	80%

# 4322 026 38190

#### MIXTURE UNIT

## ELECTRICAL DATA

Note: A positive current value indicates a current flowing toward the circuit.

Power supply

Input data Output level "negative low"

Output level "negative high"

Output data Output level "negative low"

Output level "negative high" RC time delay  $V_{\rm N}$  = -6 V ± 10%  $I_{\rm N}$  = -1 mA (for each gate)

 $\label{eq:VG} \begin{array}{l} -V_G = \min. & -0.15 \ V_N \\ = \max. & -0.25 \ V_N \\ -I_G = \max. & 0.027 \ \text{mA} \ (\text{per sub-unit}) \\ -V_G = \min. & 0 \ V, \ \max. \ 0.15 \ V \end{array}$ 

 $-V_Q = max. -V_N -\Delta V$  $\Delta V = \frac{2.04}{62 - n} V$ (n = number of operated keys)

 $-V_O = min. -V_N$ 

between 4 ms and 10 ms (actual value depends on position in unit)



RZ 23856-11

#### DESCRIPTION

Each stop-unit panel contains ll plug-in printed wiring boards mounted on a chassis. Each printed wiring board contains two stop circuits that can be used separately or together.

They are completely equipped except for those components that affect voice, these may be inserted to suit particular needs and personal taste.

The circuits contain provision for an input from the equalizing networks and an input for a chiff frequency. A potentiometer enables the volume of the stop to be adjusted to suit the organ's location.

Catalogue number: 4322 026 37720

# 4322 026 37720

#### STOP UNIT

## MECHANICAL AND ENVIRONMENTAL DATA

Overall dimensions	396 mm x 110 mm x 140 mm
Weight	1050 g
Ambient temperature range	
storage :	-20 °C to +70 °C
operating:	+5 °C to +50 °C
Max. relative humidity	80%

#### ELECTRICAL DATA

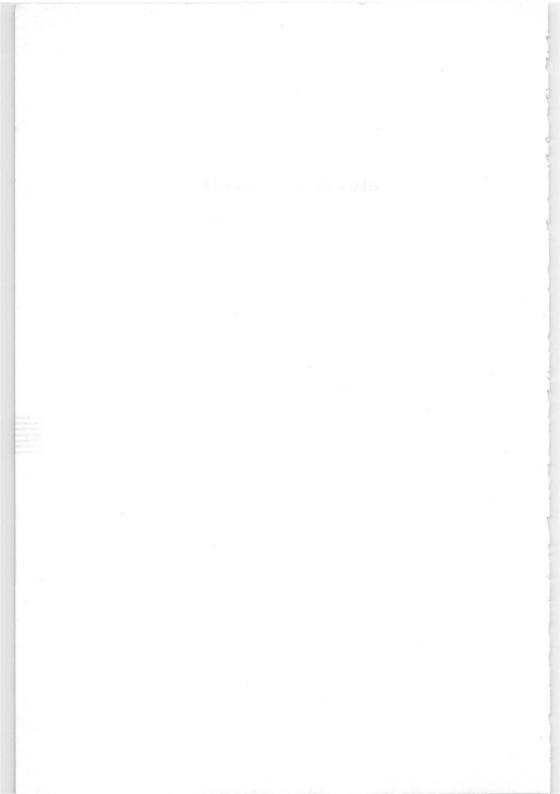
Note: A positive current value indicates a current flowing toward the circuit.

Power supply voltage current Amplification

 $\begin{array}{l} V_N = -6 \ V \pm 10\% \\ I_N = -0.3 \ \text{mA} \ \text{(for each stop-circuit)} \\ V_{out} = \min. \ 30 \ x \ V_{in} \end{array}$ 

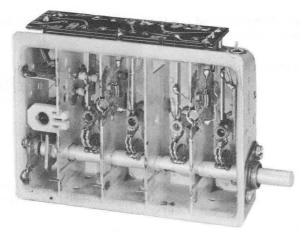
**Television tuners** 





# AT 6381/01 AT 6381/03

## UHF TELEVISION TUNERS



System Frequency range Intermediate frequencies picture sound Equipped with transistors CCIR RZ 20305-3 470 - 890 MHz (bands IV and V)

38.9 MHz 33.4 MHz

## GENERAL

These continiously variable UHF transistor tuners are designed for the reception of television signals in the UHF bands IV and V covering the frequency range of 470 – 890 MHz. The tuners with indication /01 are equipped with transistors AF 139 in both RF and mixeroscillator stages; the /03 versions are equipped with transistors AF 186 in the stages mentioned. Moreover the /03 versions have a damping resistor of 100 $\Omega$ , located near the Lecher system.

Tuning is achieved by a 4-gang variable capacitor, which is coupled to  $1/4\,\lambda$  -Lecher wires.

The spindle of the capacitor is brought out directly through the tuner case, permitting the use of various forms of drives, e.g. push buttons. When no push buttons are used a suitable reduction gear should be mounted on to the spindle, which will assist in reducing the direct axial spindle torque.

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F3

#### UHF TELEVISION TUNERS

AT 6381/01 AT 6381/03

3122 108 59471 3122 108 59480

Inside the case a stop has been mounted by which the spindle rotation is limited to approx.  $180^{\circ}$ . This stop can be removed for motor tuning in case  $360^{\circ}$  angle rotation is required (clockwise or counter-clockwise). When slow motion dials are used the gearing should be about 1 : 40.

Thanks to the use of transistors and  $1/4 \lambda$ -Lecher wires an overall reduction in the size of the tuners has been made possible.

TECHNICAL PERFORMANCE

Transistors

Supply

Mechanical drive

Frequency range

RF bandwidth Intermediate frequencies

Aerial impedance Standing wave ratio Maximum permissible input voltage

Gain

Gain reduction Noise

Image frequency rejection

RF amplifier :  $\overline{\text{AF 139}}$   $\overline{\text{AF 186}}$ Mixer-oscillator: AF 139 AF 186

Vosc VRF } 12∨ (9.5∨ min) I<sub>total</sub> ~ 8mA (without AGC)

Direct to tuner spindle. C<sub>max</sub> = spindle fully turned in clockwise direction Max. permissible axial torque on the spindle = 40 Ncm

470–890 MHz (Angle of rotation approximately 180 °; frequency dependency approximately linear)

10-20 MHz at the 3 dB points

Picture IF 38.9 MHz Sound IF 33.4 MHz

The oscillator frequency is higher than the receiving frequency. The IF filter on the tuner is adjusted to approximately 36.5 MHz.

 $300 \Omega$  symmetrical

p < 3

50 mV<sub>emf</sub> at  $300\Omega$ 

>14 dB (for an IF bandwidth of 6 MHz at the 3 dB points)

> 30 dB (forward AGC)

at 470 MHz  $\leq$  10 dB (average 8.5 dB) at 800 MHz  $\leq$  11 dB (average 9.5 dB) at 860 MHz  $\leq$  12 dB (average 10.5 dB) at 890 MHz  $\leq$  13 dB (average 11 dB)

>43 dB

3122 108 59471 3122 108 59480 UHF TELEVISION TUNERS

# AT 6381/01 AT 6381/03

IF rejection

IF output

Oscillator frequency stability

>60 dB

Capacitive foot coupling (capacity in the tuner  $\sim\!42~\mathrm{pF})$ 

 ${\rm \Delta}f_{\text{OSC}} \leq \pm 150 \ kHz$  at supply-voltage variations of  $\pm 10 \ \%$  .

 $\Delta f_{\rm OSC} <\!500$  kHz, measured between 0 and 60 min after switching on and a rise of the ambient temperature from 25 °C to 40 °C.

Difference in amplitudes between picture and sound carriers

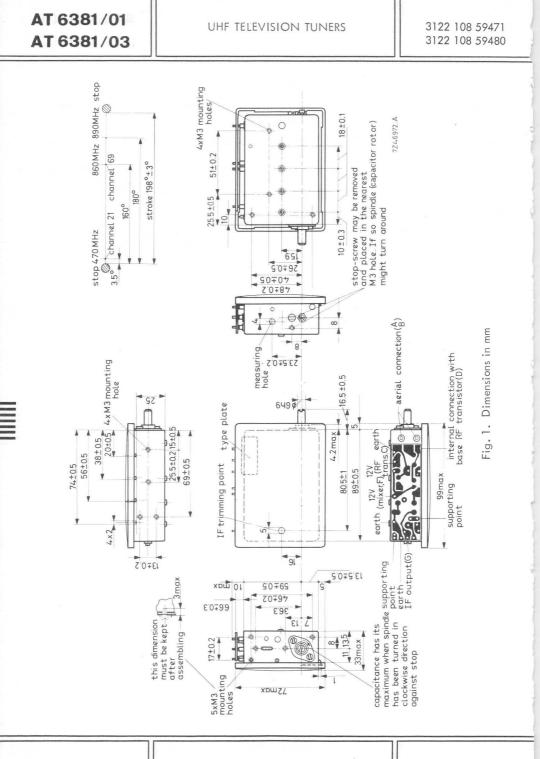
 $\leq$  2 dB at nominal gain  $\leq$  4 dB at a gain reduction of 20 dB

Maximum permissible case temperature

60 °C (at nominal value of the supply voltage)

VERSIONS

AT6381/02,	for	Great Britain	3122	108 59490
AT6381/30,	for	France	3122	108 59510
AT6381/38,	for	Italy and the FCC system	3122	108 59500



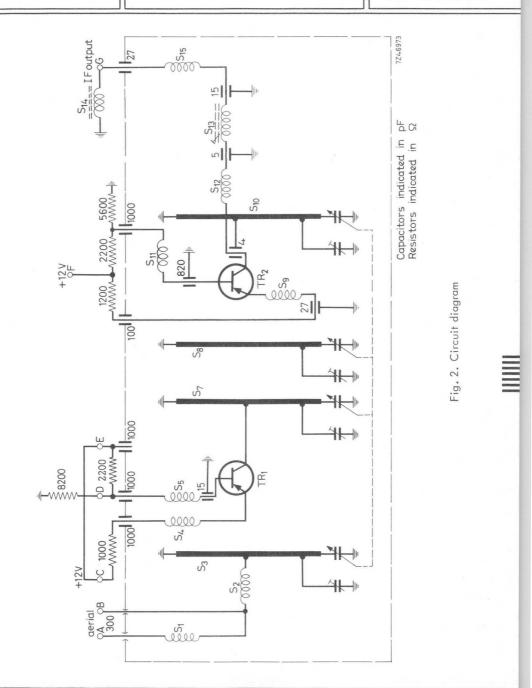
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3122 108 59471 3122 108 59480

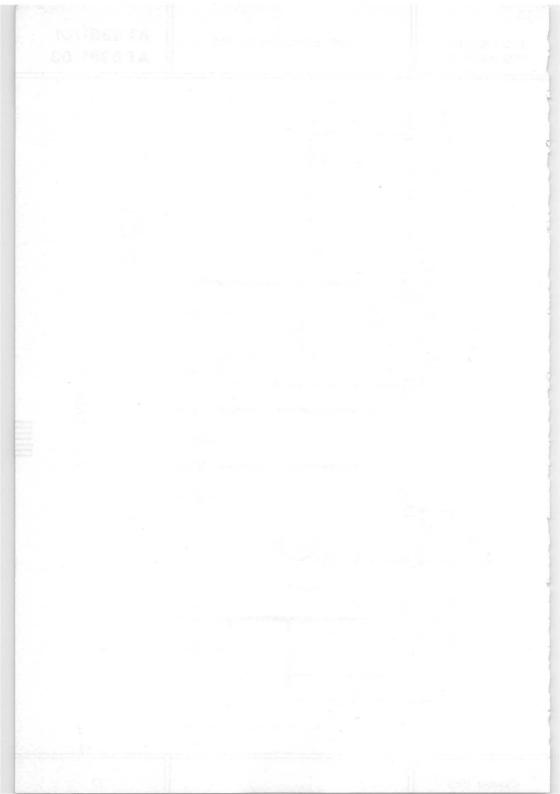
## UHF TELEVISION TUNERS

# AT 6381/01 AT 6381/03

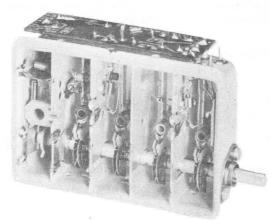


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F7



# U.H.F. TELEVISION TUNER



RZ23508-1

System Frequency range Intermediate frequencies picture sound Equipped with transistors C.C.I.R. 470-890 MHz (bands IV and V)

38.9 MHz 33.4 MHz

#### GENERAL

This continuously variable u.h.f. transistor tuner is designed for the reception of television signals in the u.h.f. bands IV and V covering the frequency range of  $470-890~\mathrm{MHz}$ .

The r.f. stage operates with a transistor AF 239; in the mixer-oscillator stage a transistor AF 139 is used.

Tuning is achieved by a 4-gang variable capacitor, which is coupled to  $1/4\,\lambda\text{-}$  Lecher wires.

The spindle of the capacitor is brought out directly through the tuner case, permitting the use of various forms of drives, e.g. push buttons. When no push buttons are used a suitable reduction gear should be mounted on to the spindle, which will assist in reducing the direct axial spindle torque.

Inside the case a stop has been mounted by which the spindle rotation is limited to approximately  $180^{\circ}$ . This stop can be removed for motor tuning in case  $360^{\circ}$  angle rotation is required (clockwise or counter-clockwise). When slow motion dials are used the gearing should be about 1 : 40.

Thanks to the use of transistors and 1/4  $\lambda-Lecher$  wires an overall reduction in the size of the tuner has been made possible.

#### TECHNICAL PERFORMANCE

Transistors r.f. amplifier mixer-oscillator	AF 239 AF 139
Supply voltages r.f. amplifier oscillator	+12 V (minimum +9.5 V) +12 V (minimum +9.5 V)
Total supply current without a.g.c.	approximately 8 mA
Frequency range	470 - 890 MHz
Intermediate frequencies picture sound	38.9 MHz 33.4 MHz The oscillator frequency is higher than the signal frequency. The i.f. filter is adjusted to approxi- mately 36.5 MHz.
R.F. bandwidth at 3 dB	10 - 18 MHz
Gain for an i.f. bandwidth of 7 MHz at 3 dB	> 18 dB
Gain reduction (forward a.g.c.)	> 30 dB
Maximum permissible input voltage without modulation distortion at a cross modulation factor of 1%	50 mV <sub>emf</sub> at 300 Ω 20 mV <sub>emf</sub> at 300 Ω
Aerial impedance	300 Ω
Standing wave ratio	p < 3
Noise, at 470 MHz at 600 MHz at 800 MHz at 860 MHz at 890 MHz	average value 7.0 dB (max. 8.5 dB) average value 7.0 dB (max. 8.0 dB) average value 7.0 dB (max. 8.5 dB) average value 8.5 dB (max. 10.0 dB) average value 9.0 dB (max. 11.0 dB)

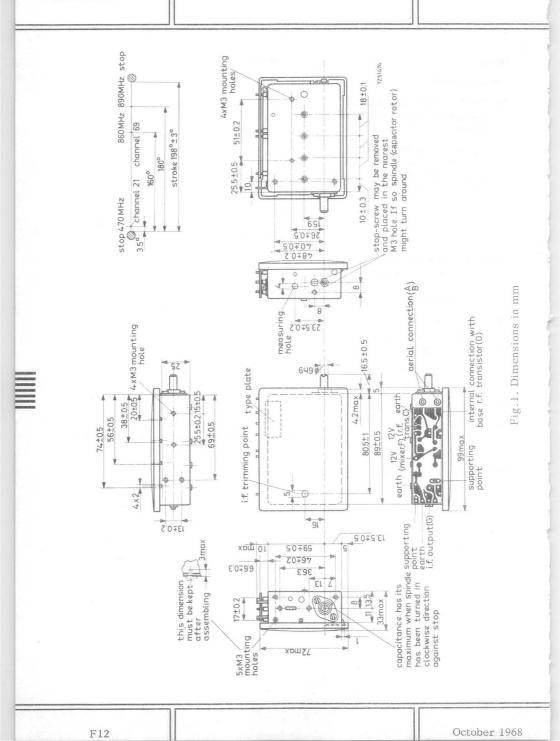
October 1968

F10

Image frequency rejection	> 46 dB
I.F. rejection	> 60 dB
Oscillator frequency stability at supply-voltage variations of $\pm 10\%$	$\leq \pm 150$ kHz
between 0 and 60 min after switching on and a rise of the ambient temperature from 25 °C to 40 °C	< 500 kHz
I.F. output	capacitive foot coupling. Capacitance in the tuner is approxi- mately 42 pF.
Difference in amplitude between picture carrier and sound carrier at nominal gain at a gain reduction of 20 dB	$\leq 2 \text{ dB}$ $\leq 4 \text{ dB}$
Maximum permissible case temperature at the nominal value of the supply voltage	60 °C
Frequency variation with the angle of rotation	approximately linear
Maximum angle of rotation	1800
Mechanical drive	direct to tuner spindle. ( $C_{max}$ = spindle fully turned in clock wise direction.)
Permissible axial spindle torque	≤ 40 Ncm

F11

in clock-



## U.H.F. TELEVISION TUNER

AT6382/01

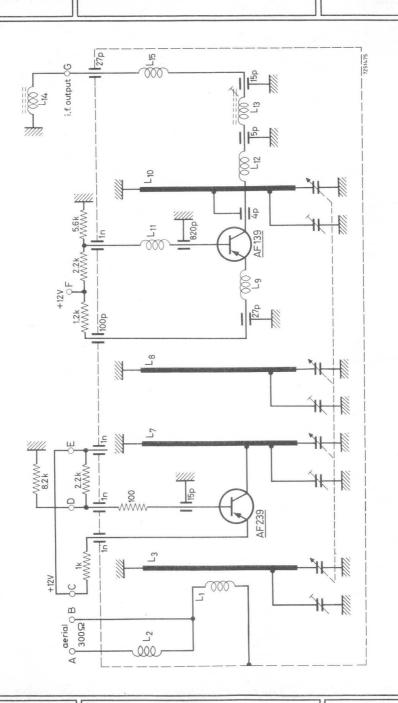
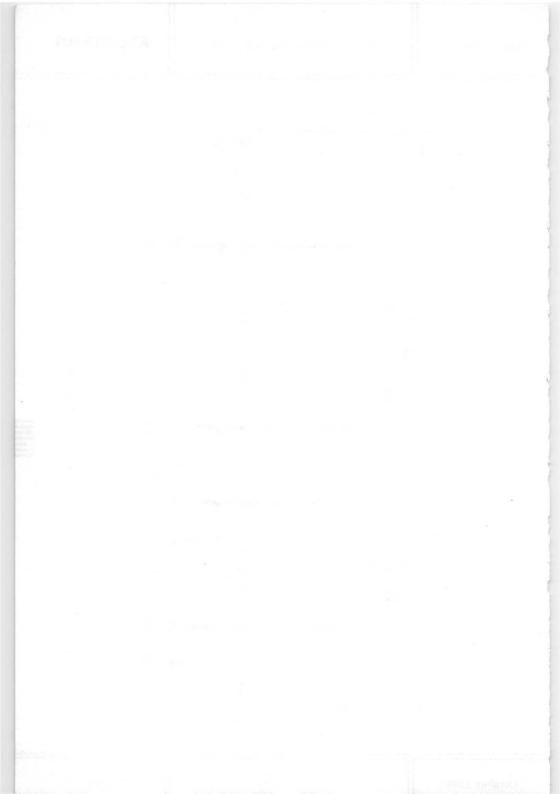
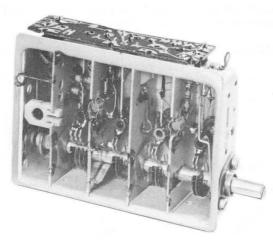


Fig.2. Circuit diagram

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## **U.H.F. TELEVISION TUNER**



RZ 23096-1

System Frequency range Intermediate frequencies picture sound Equipped with transistors French u.h.f. 470 - 890 MHz (bands IV and V)

32.7 MHz 39.2 MHz

#### GENERAL

This continuously variable u.h.f. transistor tuner is designed for the reception of the French u.h.f. channels in the bands IV and V covering the frequency range of 470-890 MHz.

The r.f. stage operates with a transistor AF 239; in the mixer-oscillator stage a transistor AF 139 is used.

Tuning is achieved by a 4-gang variable capacitor, which is coupled to 1/4  $\lambda-$  Lecher wires.

The spindle of the capacitor is brought out directly through the tuner case, permitting the use of various forms of drives, e.g. push buttons. When no push buttons are used a suitable reduction gear should be mounted on to the spindle, which will assist in reducing the direct axial spindle torque.

Inside the case a stop has been mounted by which the spindle rotation is limited to approximately  $180^{\circ}$ . This stop can be removed for motor tuning in case  $360^{\circ}$  angle rotation is required (clockwise or counter-clockwise). When slow motion dials are used the gearing should be about 1 : 40.

Thanks to the use of transistors and 1/4  $\lambda$ -Lecher wires an overall reduction in the size of the tuner has been made possible.

#### TECHNICAL PERFORMANCE

AF 239 AF 139
+12 V (minimum +9.5 V) +12 V (minimum +9.5 V)
approximately 8 mA
470-890 MHz
32.7 MHz 39.2 MHz The oscillator frequency is lower than the signal frequency. The i.f. filter is adjusted to approxi- mately 36.5 MHz.
10 - 14 MHz
> 24 dB
> 30 dB
25 mV <sub>emf</sub> at 75 $\Omega$
75 Ω
p < 3
average value 6.5 dB (max. 7.5 dB) average value 6.5 dB (max. 7.0 dB) average value 6.5 dB (max. 7.0 dB) average value 8.0 dB (max. 9.0 dB) average value 8.5 dB (max. 10.0 dB)

3122 108 68120

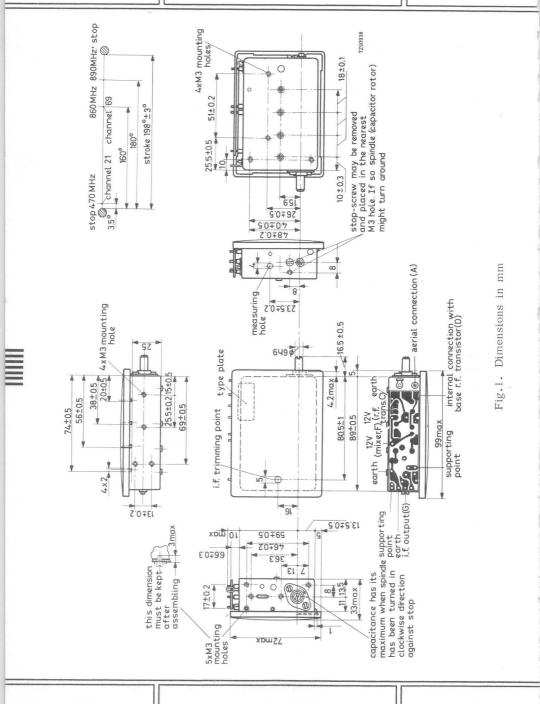
AT 6382/30

Image frequency rejection	> 46 dB
I.F. rejection	> 60 dB
Oscillator frequency stability at supply-voltage variations of $\pm 10\%$	<±150 kHz
between 0 and 60 min after switching on and a rise of the ambient temperature from 25 <sup>o</sup> C to 40 <sup>o</sup> C	< 500 kHz
I.F. output	capacitive foot coupling. Capacitance in the tuner is approxi- mately 42 pF.
Difference in amplitude between picture carrier and sound carrier at nominal gain at a gain reduction of 20 dB	<u>&lt; 2 dB</u>
Maximum permissible case temperature at the nominal value of the supply voltage	60 <sup>0</sup> C
Frequency variation with the angle of rotation	approximately linear
Maximum angle of rotation	180 <sup>0</sup>
Mechanical drive	direct to tuner spindle. (C <sub>max</sub> = spindle fully turned in clock- wise direction.)
Permissible axial spindle torque	<u>&lt;</u> 40 Ncm

F17

#### U.H.F. TELEVISION TUNER

3122 108 68120

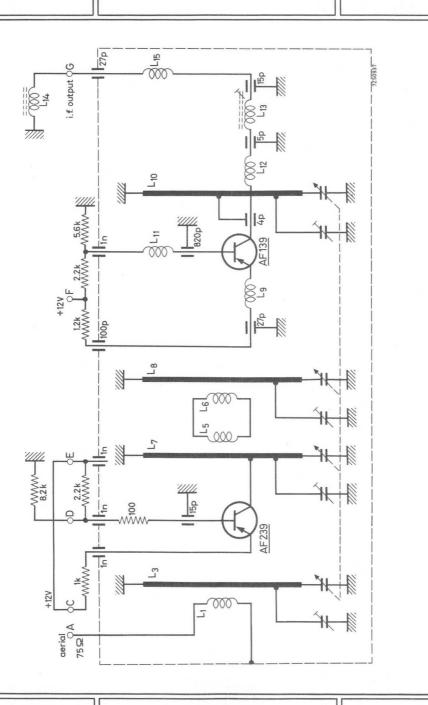


F18

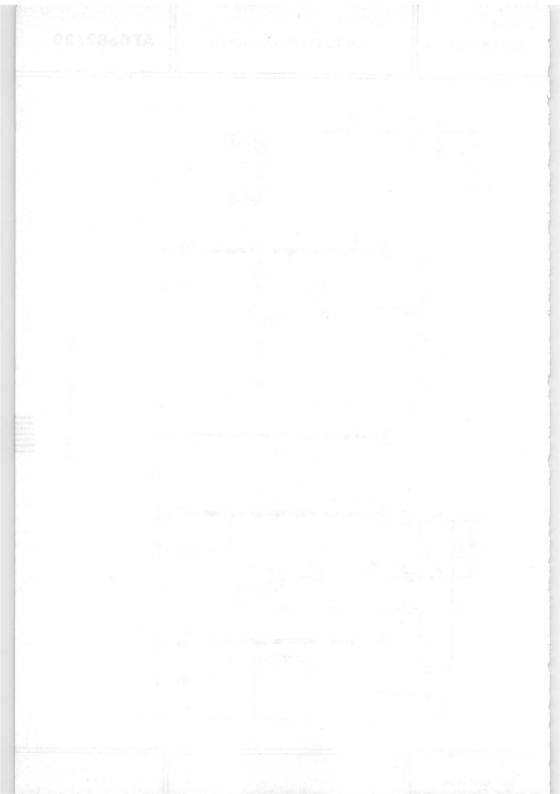
October 1968

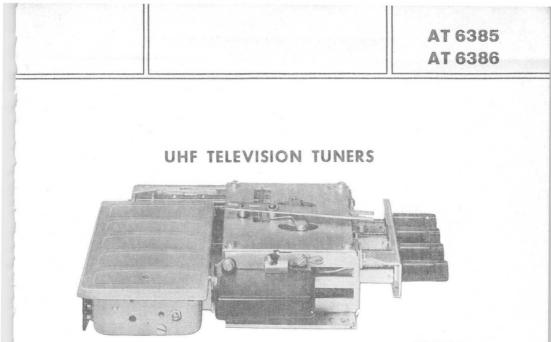
AT 6382/30

Fig.2. Circuit diagram



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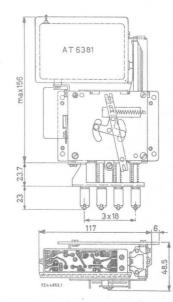


RZ 18528-1

These tuners are push-button versions of the AT 6381/01 and AT 6381/03. The tuners AT 6385/01 and AT 6385/03 are fitted with a VHF/UHF switch, while tuners AT 6386/01 and AT 6386/03 have not.

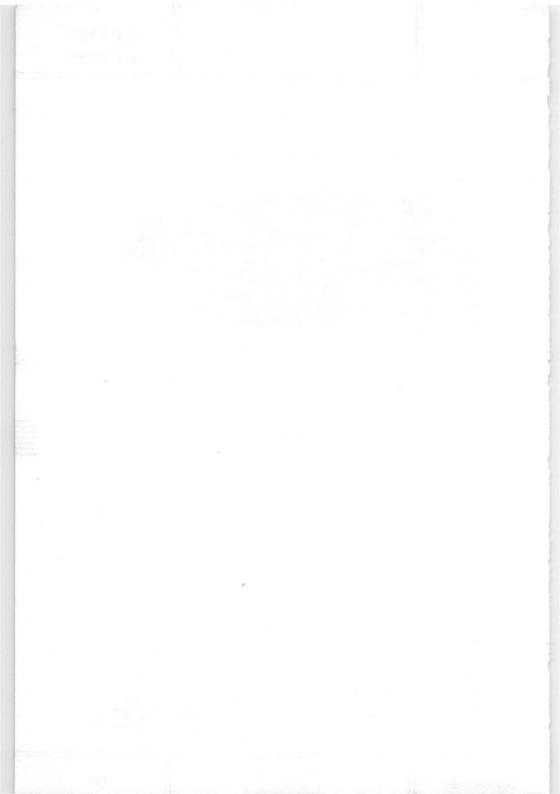
Up to four selections are possible, each of which may be pre-adjusted to any UHF channel. For information on all other properties of the tuners, see the data on the UHF television tuners AT 6381/01 and AT 6381/03.

Dimensions in mm



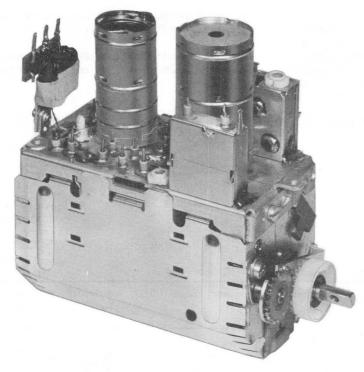
#### Catalog numbers

AT6385/01	3122 108 51050
AT6385/03	3122 108 00440
AT6386/01	3122 108 54380
AT6386/03	3122 108 54610



## AT 7650/90

# VHF TELEVISION TUNER



System Frequency ranges

Intermediate frequencies picture sound Equipped with tubes CCIR RZ 20117-3 47 - 68 MHz (band I) 174 - 223 MHz (band III)

38.9 MHz 33.4 MHz

#### GENERAL

This small VHF tuner has a 13-position turret switch equipped with 10 VHF-CCIR channel strips (channels 2–11) covering the frequency bands I and III (47–68 MHz and 174–223 MHz respectively).

The tuner has a compact and simplified memomatic fine-tuning device at the front of the tuner, which is operated from the spindle of the turret; it can be adjusted to each individual channel.

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## AT 7650/90

In the RF stage a PC 900 in neutrodyne configuration is used; the oscillator/mixer stage operates with a PCF 801.

This tuner is supplied with a bridge circuit for coupling the IF output voltage of a UHF tuner to the first grid of the pentode part of the PCF 801: in this case this tube operates as an IF amplifier tube.

There are two separate supply voltage connections (+135V) available (one for the RF stage and oscillator stage, one for the mixer stage), so that UHF/VHF reception can be effected by means of a simple D.C. supply switch.

Mixer stage

#### TECHNICAL PERFORMANCE

Tubes

Supply

 $V_{c} = 12 V$ PC900 (RF amplifier) PCF801, triode part (oscillator) | I PCF801, pentode part (mixer) RF and oscillator stages: Vb= 135 V

Imax = 25 mA (point A via resistor of 1 MΩ to earth)  $: V_{b} = 135 V$  $I_{max} = 11 \text{ mA}$ 

 $= 300 \, mA$ 

Tuning ranges

band	channel (switch positior		quency range (MI	Hz) carrie pictur	r frequency (MHz) e sound
	1				-
	2		47 - 54	48.2	5 53.75
	3		54-61	55.2	5 60.75
	4		61 - 68	62.2	5 67.75
111	5		174 - 181	175.2	5 180.75
	6		181 - 188	182.2	5 187.75
	7		188 - 195	189.2	5 194.75
	8		195 - 202	196.2	5 201.75
	9		202 - 209	203.2	5 208.75
	10		209 - 216	210.2	5 215.75
	11		216 - 223	217.2	5 222.75
	12		-	-	-
	13		-		
e tuning	range	1.		$\Delta f = 2 $ $\Delta f = 2.5 $	
bandwid	th			≤ 10 MHz ) ≤ 15 MHz )	at the 3 dB points

F24

3122 996 68400

VHF TELEVISION TUNER

AT 7650/90

#### Tilt of the bandpass curves IF frequencies

The RF bandwidth is measured at the testpoint H (which is external connected to earth via a resistor of 220 k $\Omega$ ) of the mixer grid with the oscillator in operation and  $V_{agc} = -1.4 V$ . In Fig. 1 the ideal bandpass curves together with the tolerated deviations are shown.  $\leq 20\%$  for all channels at  $V_{agc} = -1.4 V$ Picture-carrier frequency: 38.9 MHz Sound-carrier frequency : 33.4 MHz The oscillator frequency lies beyond the receiving frequency. The IF primary coil on the tuner is adjusted to approximately 36.5 MHz

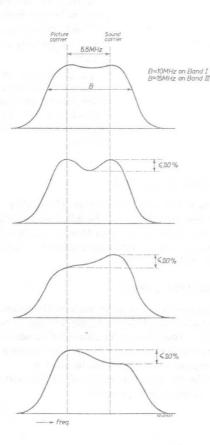


Fig. 1

October 1968

## AT 7650/90

#### VHF TELEVISION TUNER

3122 996 68400

Aerial input impedance Reflections Gain

Gain of the pentode part of the PCF801 used as an IF amplifier Noise

Image frequency rejection

IF rejection

Reset accuracy

Oscillator frequency stability

Radiation

300 Ω symmetrical ≤ 40% at maximum gain 35 dB from aerial-emf to the grid of the first IF stage (for an IF bandwidth of 6.5 MHz at the 3dB points and flat within 5%)

20 dB Band I :  $\leq$  3.5 kTo Band III:  $\leq$  6.5 kTo Band I :  $\geq$  60 dB Band III:  $\geq$  54 dB Band I :  $\geq$  40 dB symmetrical  $\}$  for both pic-Band III:  $\geq$  60 dB symmetrical  $\}$  ture and sound When switching from one channel to another and back again  $\Delta$  fosc < 100 kHz

 $\Delta\,f_{osc}$  =± 150 kHz at variations of V  $_{b}$  osc of ± 10 %

 $\Delta$  f<sub>osc</sub>  $\leq 250$  kHz , measured between 2 minutes and 60 minutes after switching on and an ambient temperature rise from 20  $^\circ$  C to 55  $^\circ$ C. The radiation from the tuner complies with the requirements specified by the German Post Office.

#### ADJUSTMENT OF THE SUPPLY VOLTAGE

When the tuner is used as a VHF mixer (not as an IF amplifier for UHF reception) the supply voltage for the mixer at point L must be adjusted to +135 V; the supply voltage for the RF amplifier and the oscillator at point M must also be adjusted to +135 V. Moreover point A must be connected to earth via a resistor of  $1M\Omega$ . (This resistor is necessary to prevent overloading of the PC900).

#### TESTING OF THE IF BANDPASS CURVES

For testing the IF bandpass curves use must be made of the testpoint N. The tuner has to be set in one of the channels of band III; the supply voltage at point M must be switched off (oscillator switched off). Point F must be connected to earth.

When the tuner is used as a VHF mixer, point H must be connected to earth via a resistor of 220 k $\Omega$ ; the AGC voltage must be connected to point A.

When used as an IF amplifier for UHF the resistor of  $220 k\Omega$  must be switched off and the AGC voltage must be switched over to point H.

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3122 996 68400

### CATALOG NUMBER OF THE CHANNEL STRIPS

channel	indication	catalog number	channel	indication	catalog number
2	E2V	3122 997 57290	7	E7V	3122 997 57340
3	E3V	3122 997 57300	8	E8V	3122 997 57350
4	E4V	3122 997 57310	9	E9V	3122 997 57360
5	E5V	3122 997 57320	10	E10V	3122 997 57370
6	E6V	3122 997 57330	11	EIIV	3122 997 57380

### TUNER VERSIONS

type	for	catalog number
AT7650/11	New Zealand	3122 108 54651
AT7650/18	the FCC system	3122 108 50091
AT7650/21	Great Britain	3122 108 50061
AT7650/25	France	3122 108 50111
AT7650/38	Italy (Italian IF)	3122 108 50081
AT7650/39	Italy (CCIR IF)	3122 108 50071
AT7650/80	Germany (11 channels)	3122 108 54071
AT7650/82	Austria	3122 108 50021
AT7650/84	Finland	3122 108 50031
AT7650/86	Belgium	3122 108 50051

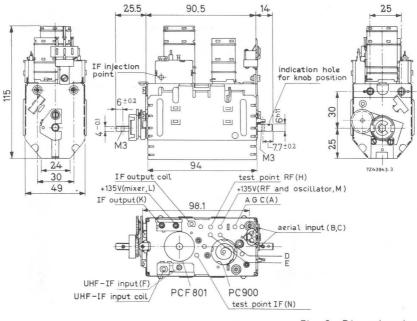
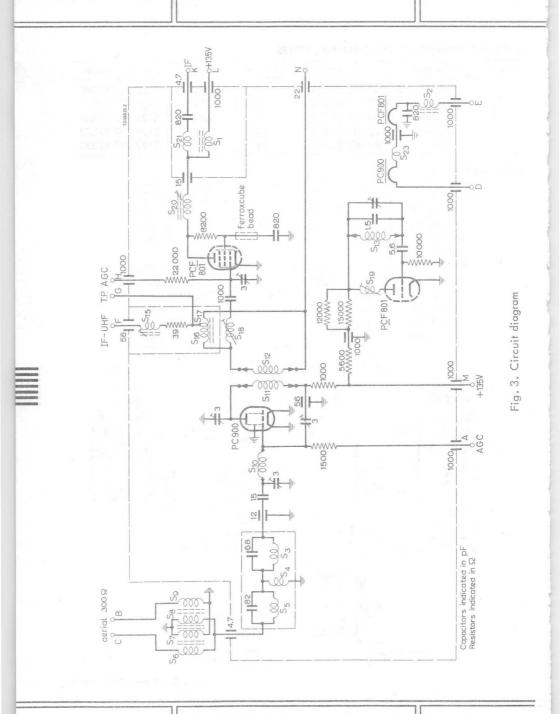


Fig. 2. Dimensions in mm

# AT 7650/90

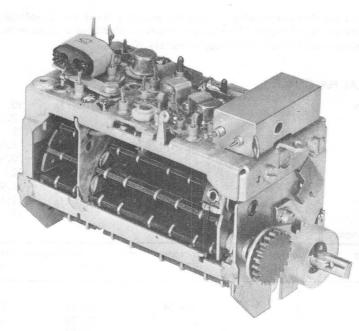
#### VHF TELEVISION TUNER

3122 996 68400



AT 7652/80T

## VHF TELEVISION TUNER



System Frequency ranges

Intermediate frequencies picture sound Equipped with transistors

RZ 20305-5 CCIR 47-68 MHz (band 1) 174-223 MHz (band 111)

38.9 MHz 33.4 MHz

#### GENERAL

This VHF transistor tuner has a 13-position turret switch equipped with 10 VHF-CCIR channel strips (channels 2-11) covering the frequency bands I and III (47 - 68 MHz and 174-223 MHz respectively).

The tuner has the same memomatic fine-tuning system as used in the VHF tuner AT7650/90; it can be adjusted to each individual channel.

The RF stage operates with a transistor AF180<sup>1)</sup>. In the mixer stage and in the oscillator stage a transistor AF178 is used.

1) Known as AF180 double star

## AT 7652/80T

Forward AGC can be applied to the RF stage by means of which a gain reduction can be obtained of  $\sim 40~\text{dB}$  .

The tuner is supplied with a bridge circuit for coupling the IF output voltage of a UHF tuner to the emitter of the AF 178 (mixer); in this case this transistor operates as an IF amplifier giving an additional gain of approximately 10 dB.

#### TECHNICAL PERFORMANCE

Transistors

AF180 (RF amplifie	r): I <sub>B</sub>	$\sim$	50	μA
	IE	=	2.5	mA
	Vago	=	12	$\vee$
AF178 (oscillator)	: IE	~	1.85	
	IB		0.92	2 mA
	Vb	=	12	V
AF178 (mixer)	: 1 <sub>E</sub>		1.9	
	IB		1.15	σmΑ
	Vb	=	12	$\vee$

**Tuning** ranges

band	channel (switch position)	frequency range (MHz)	carrier frequenc picture	cy (MHz) sound
1	1	-	-	-
	2	47 - 54	48.25	53.75
	3	54 - 61	55.25	60.75
	4	61 - 68	62.25	67.75
111	5	174 - 181	175.25	180.75
	6	181 - 188	182.25	187.75
	7	188 - 195	189.25	194.75
	8	195 - 202	196.25	201.75
	9	202 - 209	203.25	208.75
	10	209 - 216	210.25	215.75
	11	216 - 223	217.25	222.75
	12	-	-	-
	13	-	-	-
ne tuning	range		f = 2.5 - 5 MHz f = 2.5 - 8 MHz	
bandwid	th	The RF band	4 MHz 2 MHz } at the 3d pass curves are adj	B points justable a
		$I_{E} = 2.5 \text{ mA}$		
t of the b	pandpass curves	< 25 % for a	II channels	

3122 108 60160

VHF TELEVISION TUNER

AT 7652/80T

#### IF frequencies

Aerial input impedance Reflections Gain

Gain reduction

Noise

Image frequency rejection

IF rejection

Reset accuracy

Minimum oscillator voltage Oscillator frequency stability Picture-carrier frequency : 38.9 MHz Sound-carrier frequency : 33.4 MHz The oscillator frequency lies beyond the receiving frequency. The IF coil on the tuner is adjusted to approximately 36.5 MHz  $300 \Omega$  symmetrical

 $\leq$  40% at maximum gain and I<sub>E</sub> = 2.5 mA 26 dB from aerial – emf to the first IF stage (for an IF bandwidth of 6.5 MHz at the 3 dB points and flat within 5%)

 $\begin{array}{ccccccc} 40 \text{ dB at } V_{agc} \sim & 8 & V \\ & I_{agc} \sim & 0.66 \text{ mA} \\ & I_B & \sim 180 & \mu\text{A} \\ & I_E & \sim & 8 & \text{mA} \\ \end{array}$  Band I :  $\leq 5 \text{ k } T_o$ Band III :  $\leq 9 \text{ k } T_o$ 

Band I :>32 dB  $ext{agc} = 12V$  and an in-Band III :>46 dB  $ext{bgc}$  signal  $\leq 100 \ \mu V$ 

Band I :>40 dB ) at  $V_{agc} = 12 V$ ; for both Band III :>60 dB ) picture and sound When switching from one channel to another and back again :  $\Delta f_{osc} < 100 \text{ kHz}$ 100 mV

Band I :  $\Delta f_{osc} \leq -150 \text{ kHz}$  and  $\leq +120 \text{ kHz}$ at a voltage variation from 12 V to 10 V. Band III :  $\Delta f_{osc} \leq -500 \text{ kHz}$  and  $\leq +400 \text{ kHz}$ at a voltage variation from 12 V to 14 V.  $\Delta f_{osc} \leq 400 \text{ kHz}$ , measured between 0 and 30 minutes after switching on and an ambient temperature rise from 25 °C to 55 °C.

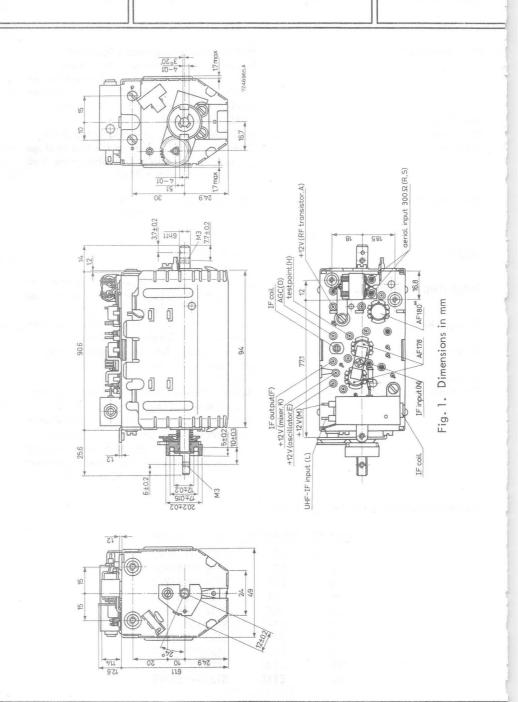
#### CATALOG NUMBERS OF THE CHANNEL STRIPS

channel	indication	catalog number
2	E2T	3122 108 51820
3	E3T	3122 108 5 1830
4	E4T	3122 108 51840
5	E5T	312210851850
6	E6T	3122 108 51860
7	E7T	3122 108 51870
8	E8T	312210851880
9	E9T	3122 108 51890
10	EIOT	3122 108 51900
11	EllT	3122 108 51910

# AT 7652/80T

### VHF TELEVISION TUNER

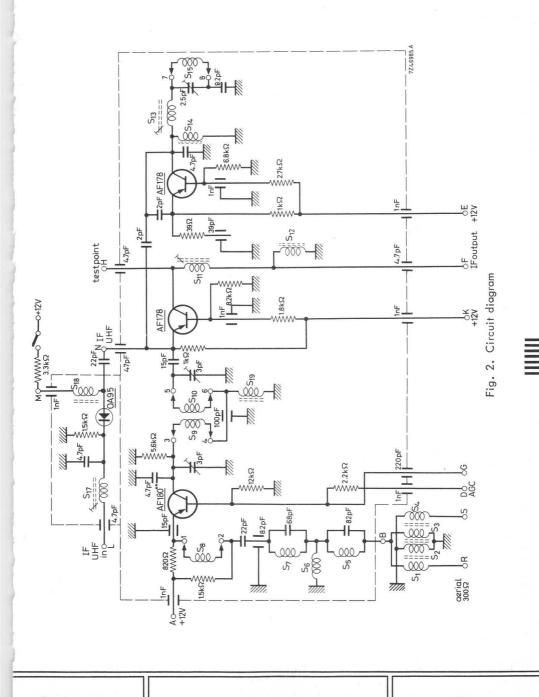
3122 108 60160



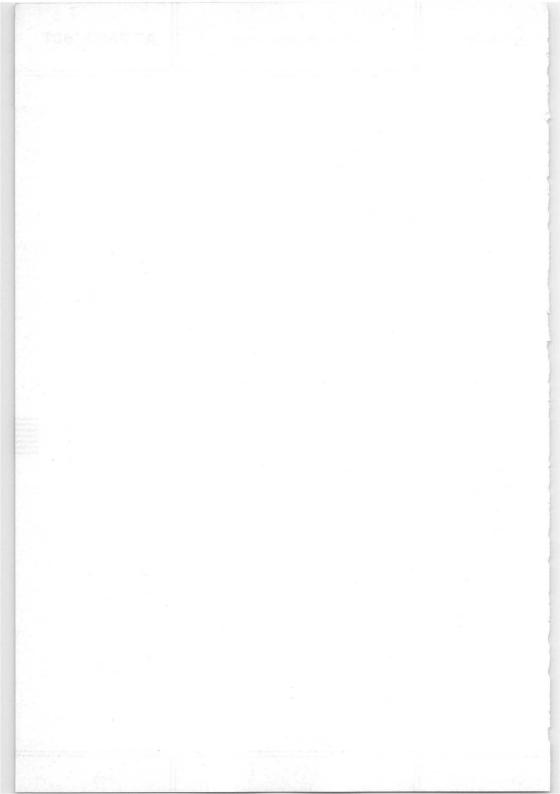
### 3122 108 60160

#### VHF TELEVISION TUNER

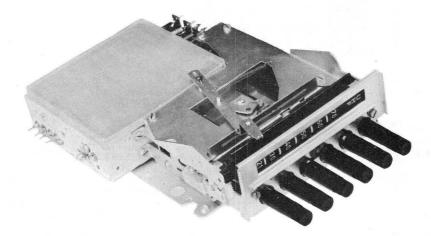
AT 7652/80T



October 1968



# **VHF/UHF TELEVISION TUNER**



RZ 22666-1

System Frequency ranges

Intermediate frequencies picture sound With push-button unit Equipped with transistors CCIR 47 - 68 MHz (band I) 174 - 230 MHz (band III) 470 - 890 MHz (bands IV and V)

38.9 MHz 33.4 MHz

#### APPLICATION

This push-button television tuner has been developed for reception of television signals in the bands I, III, IV and V (CCIR system).

#### CONSTRUCTION

The tuner is fitted with a push-button unit. Up to six selections are possible, each of which may be pre-adjusted to any VHF or UHF channel. However for reception of colour television it is advisable to use the push-buttons 1 and 2 (see Fig. 1).

The band selection slide switch (7, Fig. 1) is operated by a push-button which must be first fully depressed and then turned.

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41.5

35.5

32

0

0

0

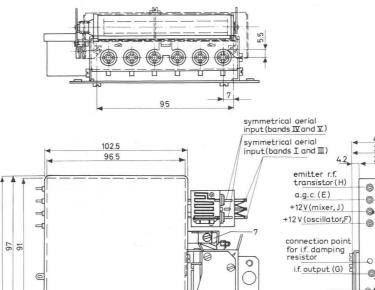
38.7

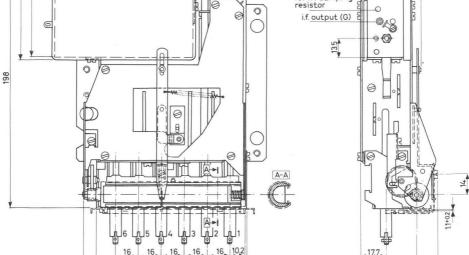
54

0

hole for fixing the band selection switch

Ail dimensions are given in mm.





7250453

104.8

114

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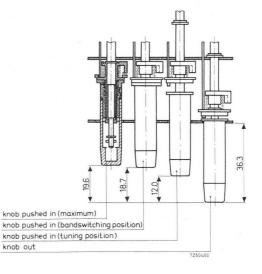
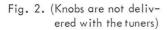
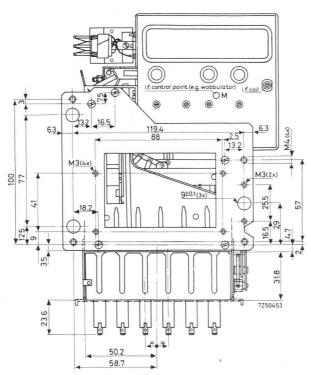


Fig. 1





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It has the following five positions in the order given:

bands IV and V, band III, band I, reserve (for other systems) and test position(slide switch against limit). The band selection switch must be set in the test position when i.f. signals are injected for aligning the i.f. circuit of the tuner and the i.f. amplifier. It can be fixed in this position by means of a little pin (0.8 mm  $\phi$ ) through the aperture at the end of the switch.

The tuner is provided with a mounting plate, for building into the television receiver. To prevent large temperature variations it is recommended to mount the tuner not in the top of the housing.

For VHF and UHF reception the tuner has a separate r.f. amplifier, mixer and oscillator.

It is possible to mount a filter on the tuner to give an extra rejection of strong unwanted signals (e.g. f.m. signals). For ordering this filter use the catalog number 3122 108 65030.

The tuners are delivered without knobs, scale, cover plate and pointer. For suggestions on these parts, see the figures 8 to 11 inclusive.

### TECHNICAL PERFORMANCE

Transistors

r.f. amplifier mixer oscillator Supply voltages r.f. amplifier oscillator Total supply current without a.g.c. with a.g.c. Frequency ranges

Intermediate frequencies picture sound

R.F. bandwidth at 3dB band I band III bands IV and V AF 239 AF 139 AF 139

+ 12V (minimum +9.5V) + 12V (minimum +9.5V)

approximately 11 mA approximately 17 mA 47 - 68 MHz (band I) 174 - 230 MHz (band III) 470 - 890 MHz (bands IV and V)

38.9 MHz33.4 MHzThe oscillator frequency is higher than the signal frequency.The i.f. filter is adjusted to approximately 36.5 MHz.

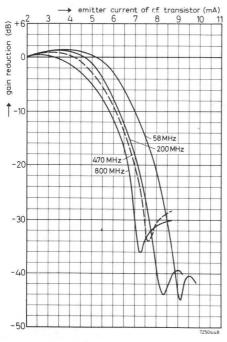
8 - 12 MHz 8 - 14 MHz 8 - 18 MHz 3122 108 65520

AT 7672/90

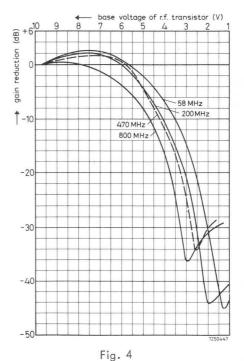
Gain for an i.f. bandwidth of 7 MHz at 3 dB bands I and III bands IV and V Gain reduction (see Figs 3 and 4) bands I and III bands IV and V Maximum permissible input voltage Aerial impedance **Reflection** factor Noise, band I band III at 470 MHz at 650 MHz at 800 MHz at 860 MHz at 890 MHz

 $\geq 22 \text{ dB (average value 26 dB)}$   $\geq 18 \text{ dB (average value 24 dB)}$   $\geq 40 \text{ dB}$   $\geq 30 \text{ dB}$   $\leq 40\%$   $\leq 7.0 \text{ dB (average value 5.5 \text{ dB})}$   $\leq 7.5 \text{ dB (average value 6 \text{ dB})}$   $\leq 9.0 \text{ dB (average value 6 \text{ dB})}$   $\leq 9.0 \text{ dB (average value 7 \text{ dB})}$   $\leq 10.0 \text{ dB (average value 8 \text{ dB})}$  $\leq 11.0 \text{ dB (average value 9.5 \text{ dB})}$ 

< 12.0dB (average value 10dB)







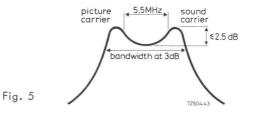
## VHF/UHF TELEVISION TUNER

3122 108 65520

Image frequency rejection	
band I	≥ 60 dB
band III	≥ 56 dB
bands IV and V	≥ 50 dB
I.F. rejection	
band I	≥ 34 dB
band III	≥ 60 dB
bands IV and V	$\geq$ 60 dB
Oscillator frequency stability	
at a supply voltage variation from	
12 to 10V or from 12 to 14V	$\leq$ 250 kHz/V
at a temperature variation of 25 °C	
band I	< 300 kHz
band III	<u>&lt;</u> 700 kHz
bands IV and V	≤ 1 MHz
Reset accuracy	<u>&lt;</u> 250 kHz
I.F. output	bottom coupled band pass filter.
	Capacitance in the tuner is approximately 20 pF

Difference in amplitude between picture carrier and sound carrier at nominal gain

< 2.5 dB



Frequency variation with the angle of	
rotation, measured without push-button	
unit	

	angle of rotation (deg)	frequency (MHz)
band I	20 ± 3 169 ± 3	51 65
band III	25 <u>+</u> 3 124 <u>+</u> 3 148 <u>+</u> 3	178 220 227
bands IV and V	8.5 180	470 ± 2 892 ± 3

3122 108 65520

Maximum permissible ambient temperature at the nominal value of the supply voltage Radiation

60 °C

in conformity with the requirements of VDE 0872 and of CISPR. See table below

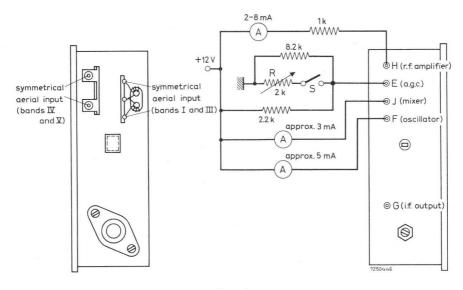
т. — — — — — — — — — — — — — — — — — — —	distance	requirement
fundamental wave of channels 2, 3 and 4 second harmonic of channels 2, 3 and 4	30 m 30 m	≤ 50 μV/m ≤ 30 μV/m
fundamental wave of channels 5 and 6 second harmonic of channels 8 to 11 inclusive third harmonic of channels 5 to 11 inclusive fundamental wave of u.h.f. channels	30 m 10 m 10 m 10 m	≤ 150 μV/m ≤ 90 μV/m ≤ 90 μV/m ≤ 90 μV/m ≤ 450 μV/m

### MEASUREMENTS

### Conditions

The supply circuit must be connected as given in Fig. 6. The a.g.c. voltage can be adjusted by means of potentiometer R (switch S closed). The r.f. signals should be applied to the symmetrical aerial inputs.

The aerial input impedance is  $300 \Omega$ .





#### Gain measurements

The circuit of Fig. 7 should be connected to the i.f. output of the tuner (point G), to form an i.f. bandpass filter and i.f. detector. The coupling capacitance (approximately 39 pF) and the damping resistance (approximately 2700  $\Omega$ ) should be so chosen that at 36.15 MHz the bandwidth curve is 7 MHz at 3 dB down, flat within 5%. The gain is defined as  $\frac{e_{ko}}{emf_{300}}$  (emf<sub>300</sub> measured at the aerial input terminals).

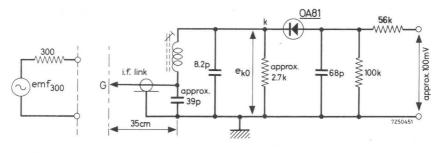
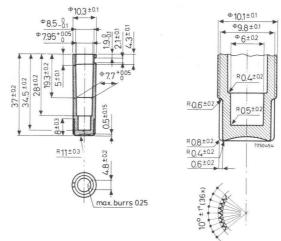


Fig. 7

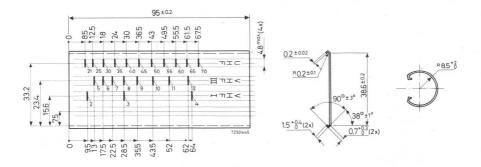
### SUGGESTIONS FOR ADDITIONAL PARTS

All dimensions are given in mm.

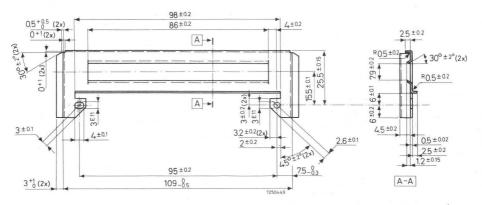




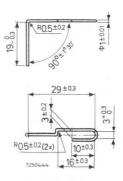
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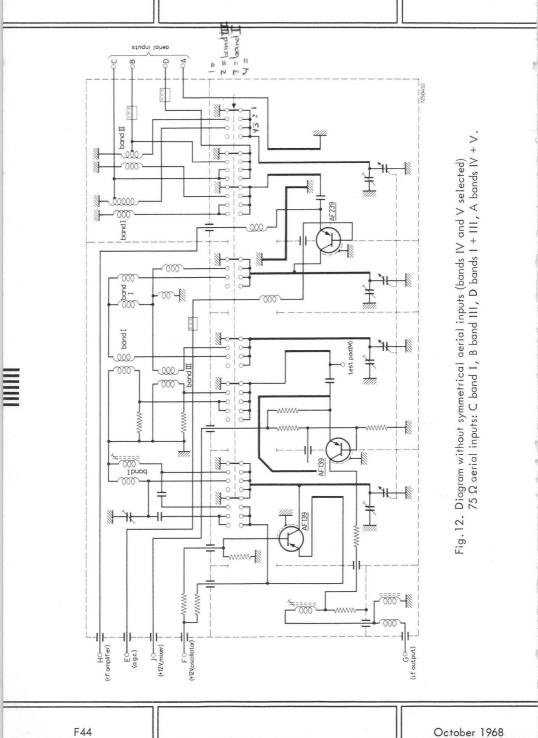






### VHF/UHF TELEVISION TUNER

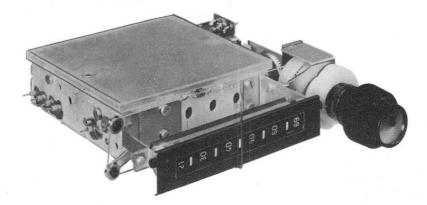
3122 108 65520



3122 108 82000

## V.H.F./U.H.F. TELEVISION TUNER

f 317,50 Radio Twen the.



RZ 24108-11

Standard system Frequency ranges

47 - 68 MHz (band I) 174 - 230 MHz (band III) 470 - 890 MHz (bands IV and V)

Intermediate frequencies picture sound

38.9 MHz 33.4 MHz

C.C.I.R.

Tuning by means of two concentric knobs

Equipped with transistors

### APPLICATION

This v.h.f./u.h.f. television tuner has been developed for reception of television signals in the bands I, III, IV and V (C.C.I.R. system).

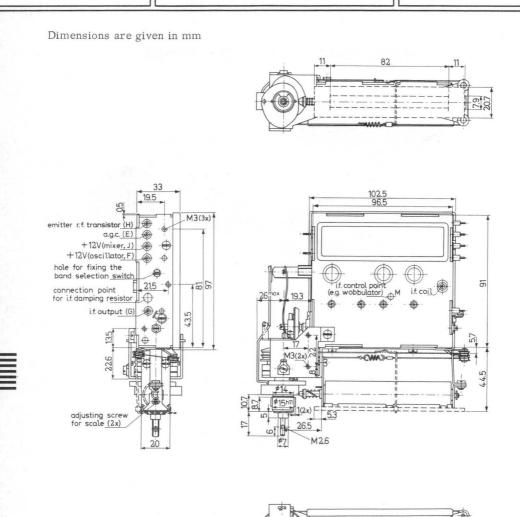
#### CONSTRUCTION

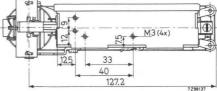
The tuner is fitted with a tuning device with two concentric knobs. With the aid of the outer knob a disc can be operated, which in its turn is setting the band selection slide switch to the desired band. With the inner knob, a channel out of this band can now be chosen. By slightly pushing the inner knob the tuner can be coarse tuned. After release of the knob, fine tuning is possible. The device is coupled to an indication mechanism consisting of a drum, onto which a scale can be fitted, and a pointer.

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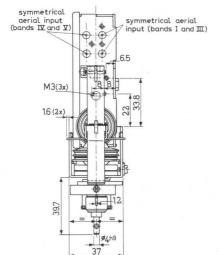
AT7680/90

3122 108 82000





October 1968





October 1968

# AT7680/90

The band selection switch has the following five positions in the order given; bands IV and V, band III, band I, reserve (for other systems) and test position (slide switch against limit). It must be set in the test position when i.f. signals are injected for aligning the i.f. circuit of the tuner and the i.f. amplifier. It can be fixed in this position by means of a little pin  $(0.8 \text{ mm } \mathscr{O})$  through the aperture at the end of the switch.

To prevent large temperature variations it is recommended to mount the tuner not in the top of the housing.

For v.h.f. and u.h.f. reception the tuner has a separate r.f. amplifier, mixer and oscillator.

It is possible to mount a filter on the tuner to give an extra rejection of strong unwanted signals (e.g. f.m. signals). For ordering this filter use the catalog number 3122 108 65030.

The tuner is delivered without knobs, scale, cover plate and pointer.

#### TECHNICAL PERFORMANCE

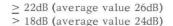
Transistors	
r.f. amplifier	AF 239
mixer	AF 139
oscillator	AF 139
Supply voltages	
r.f. amplifier	+12V (minimum $+9.5V$ )
oscillator	+ 12V (minimum $+ 9.5V$ )
Total supply current	
without a.g.c.	approximately 11 mA
with a.g.c.	approximately 17 mA
Frequency ranges	47 - 68 MHz (band 1)
	174 - 230 MHz (band III)
	470 - 890 MHz (bands IV and V)
Intermediate frequencies	\$
picture	38.9 MHz
sound	33.4 MHz
	The oscillator frequency is higher than
	the signal frequency.
	The i.f. filter is adjusted to approxi-
	mately 36.5 MHz
R.F. bandwidth at 3 dB	matery sere min
band I	8 - 12 MHz
band III	8 - 14 MHz
bands IV and V	8 - 18 MHz

#### 3122 108 82000

AT7680/90

Gain for an i.f. bandwidth of 7 MHz at 3 dB bands I and III bands IV and V Gain reduction (see Figs. 2 and 3) bands I and III bands IV and V Maximum permissible input voltage Aerial impedance V.S.W.R. Noise, band I band III at 470 MHz at 650 MHz at 800 MHz at 860 MHz

at 890 MHz



> 40dB

- $\ge$  30dB
- 18 mV
- $300\,\Omega$ , symmetrical

< 2.5

- $\leq$  7.0 dB (average value 5.5 dB)
- $\leq$  7.5 dB (average value 6 dB)
- $\leq$  9.0 dB (average value 6 dB)
- $\leq$  9.0 dB (average value 7 dB)
- $\leq$  10.0 dB (average value 8 dB)
- $\leq$  11.0 dB (average value 9.5 dB)
- $\leq$  12.0 dB (average value 10 dB)

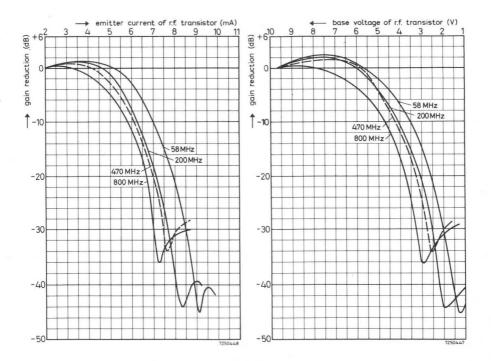


Fig. 2

Fig. 3

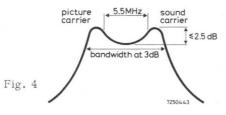
# AT7680/90

#### 3122 108 82000

Image frequency rejection		
band I	$\geq$ 60 dB	
band III	$\geq$ 56 dB	
bands IV and V	$\geq 50 \text{ dB}$	
I.F. rejection		
band I	≥ 34 dB	
band III	$\geq$ 60 dB	
bands IV and V	$\geq$ 60 dB	
Oscillator frequency stability		
at a supply voltage variation from		
12  to  10  V or from 12 to 14 $V$	$\leq 250 \text{ kHz/V}$	
at a temperature variation of 15 °C		
band I	<u>&lt;</u> 300 kHz	
band III		
bands IV andV	$\leq$ 500 kHz	
I.F. output	bottom coupled band pass filter	
	Capacitance in the tuner is approximat	
	20 pF	

Difference in amplitude between picture carrier and sound carrier at nominal gain

< 2.5 dB



Frequency variation with the angle of rotation, measured without fine tuning system

	angle of rotation (deg)	frequency (MHz)
band I	$20 \pm 3$ 169 \pm 3	51 65
band III	$25 \pm 3$ 124 \pm 3 148 \pm 3	178 220 227
bands IV and V	8.5 180	$470 \pm 2 \\ 892 \pm 3$

Maximum permissible ambient temperature at the nominal value of the supply voltage Radiation

60 °C

in conformity with the requirements of VDE 0872 and of CISPR. See table below

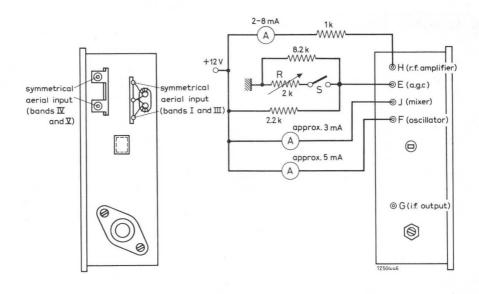
	distance	requirement
fundamental wave of channels 2, 3 and 4 second harmonic of channels 2, 3 and 4 fundamental wave of channels 5 and 6 second harmonic of channels 8 to 11 inclusive	30 m 30 m 30 m 10 m	$ \leq 50 \ \mu V/m \\ \leq 30 \ \mu V/m \\ \leq 150 \ \mu V/m \\ \leq 90 \ \mu V/m $
third harmonic of channels 5 to 11 inclusive fundamental wave of u.h.f. channels	10 m 10 m	$ \leq 90 \ \mu V/m \\ \leq 450 \ \mu V/m $

#### MEASUREMENTS

#### Conditions

The supply circuit must be connected as given in Fig. 5.

The a.g.c. voltage can be adjusted by means of potentiometer R (switch S closed). The r.f. signals should be applied to the symmetrical aerial inputs. The aerial input impedance is  $300 \Omega$ .





#### Gain measurements

The circuit of Fig. 6 should be connected to the i.f. output of the tuner (point G), to form an i.f. bandpass filter and i.f. detector. The coupling capacitance (approximately 39 pF) and the damping resistance (approximately 2700  $\Omega$ ) should be so chosen that at 36.15 MHz the bandwidth curve is 7 MHz at 3 dB down, flat within 5%. The gain is defined as  $e_{k0}$  (emf<sub>300</sub> measured at the aerial input terminals).

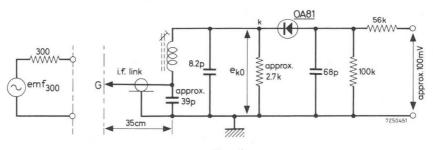


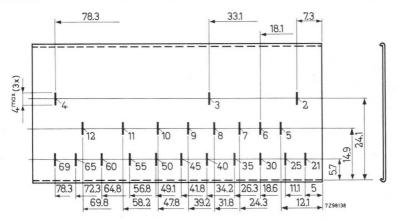
Fig. 6

#### VERSIONS

type number	system	aerial impedance	catalog number
AT 7680/20	English (tuner equipped with silicon transistors)	75 Ω	
AT 7680/25	French	75 Ω	
AT 7680/38	Italian (Italian i.f.)	300 Ω	
AT 7680/39	Italian (C.C.I.R. i.f.)	300 Ω	3122 108 82190
AT 7680/86	5-system Belgian	300 Ω	3122 108 81990
AT 7681/90	C.C.I.R.	75 Ω (v.h.f.) 300 Ω (u.h.f.)	
AT 7682/90	C.C.I.R. (tuner equipped with suppression filter)	300 Ω	3122 108 81510

AT7680/90

SUGGESTION FOR ADDITIONAL PART

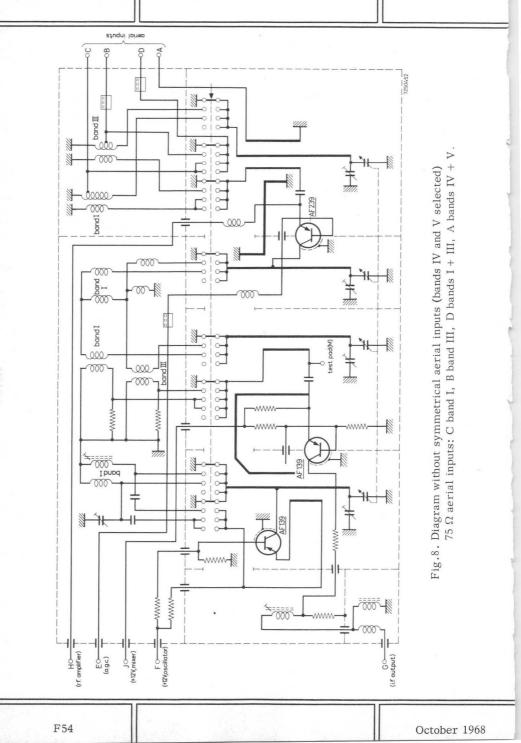




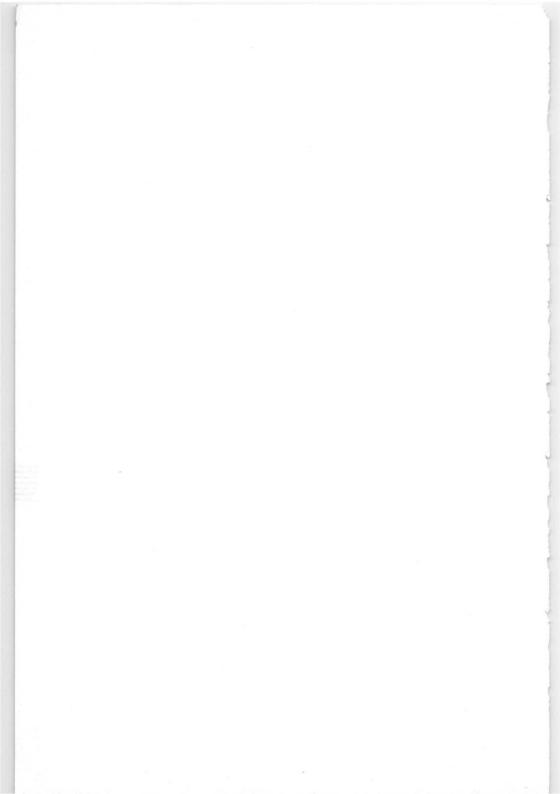
## AT7680/90

### V.H.F./U.H.F. TELEVISION TUNER

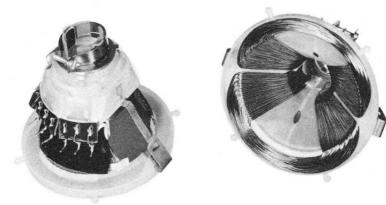
#### 3122 108 82000



# Components for black and white television



# DEFLECTION UNIT



RZ 20526-2

For transistor-equipped television receivers

# APPLICATION

This deflection unit is designed for use with the 11 inch 90° picture tube A28-14W and the 12 inch 90° picture tube A31-20W, in conjunction with the line-output transformer AT2042/01 and the linearity control unit AT4036 in transistor-equipped television sets.

### CONSTRUCTION

The saddle-shaped line deflection coils are moulded so that the deflection centre is well within the conical part of the picture tube.

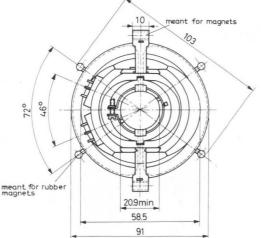
The frame deflection coils are wound on a ferroxcube yoke ring which is flared so that the frame and line deflection centres coincide. The provision of separate connecting points makes it possible to connect the frame deflection coils either in series or in parallel.

At the rear, the line and frame deflection coils, as well as the yoke ring, are potted in polyester resin.

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Dimensions in mm



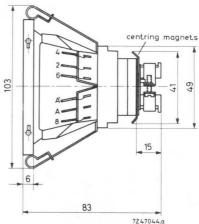
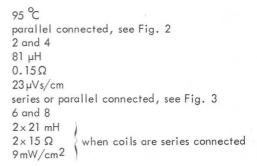
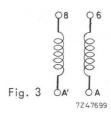


Fig. 1

# TECHNICAL PERFORMANCE

Maximum working temperature Line deflection coils Connecting terminals Inductance Resistance Sensitivity Frame deflection coils Connecting terminals Inductance Resistance Sensitivity





00000 772.47/6.96

Fig. 2

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G4

62

DEFLECTION UNIT

AT 1020 / 01

#### MOUNTING

The unit should be mounted as far forward as possible on the neck of the picture tube, so that it touches the cone.

External circuit connection is made to soldering tags, positioned as indicated in Fig. 1. If the frame deflection coils are to be connected in series, tags A and A' must be interconnected; for parallel connection, tag 8 must be connected with tag A, and tag 6 with tag A'.

To orient the raster correctly, the unit may be rotated by hand on the neck of the picture tube, with which it makes a slip fit. A screw-tightened clamping ring, cooperative with a pair of rubber friction shoes, permits it to be locked, both axially and radially, in the desired position.

# CENTRING THE BEAM

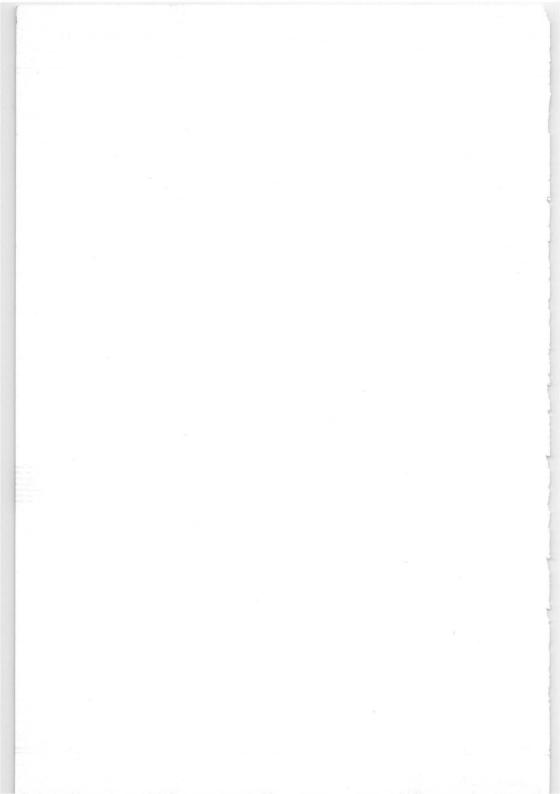
With the deflection unit mounted on the picture tube and clamped in position, the beam can be centred by rotating two, independently movable, steel magnet discs positioned adjacent the clamping ring.

#### RASTER ADJUSTMENT POSSIBILITIES

Vertical pin-cushion distortion can be corrected by small ferroxdure rods, which can be mounted on the deflection unit brackets. Limited correction of asymmetrical vertical pincushion distortion can be achieved by unequal rotation of the rods.

The shape of the corners of the raster can be adjusted by means of small rubber magnets having a centre hole to fit the pins on the rim of the deflection unit.

Both the ferroxdure rods (catalog number 4312 020 60101) and the rubber magnets (catalog number 3122 104 02721) can be supplied on request.



# DEFLECTION UNIT





RZ 20526-2

# For tube-equipped television receivers

#### APPLICATION

This deflection unit is designed for use with the 11 inch 90° picture tube A28-14W and the 12 inch 90° picture tube A31-20W, in conjunction with the line-output transformer AT2043 and the linearity control unit AT4037 in tube-equipped television receivers.

### CONSTRUCTION

The saddle-shaped line deflection coils are moulded so that the deflection centre is well within the conical part of the picture tube.

The frame deflection coils are wound on a ferroxcube yoke ring which is flared so that the frame and line deflection centres coincide.

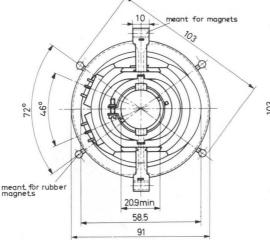
At the rear the line and frame deflection coils, as well as the yoke ring, are potted in polyester resin.

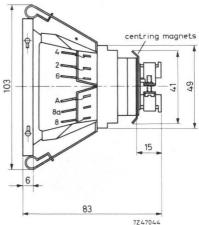
The unit is equipped with a built-in NTC-thermistor (with a parallel connected carbon resistor) connected in series with the frame coils in order to compensate for temperature dependence of the coils. By this, in frame-output circuits with voltage feedback for linearising the saw-tooth voltage a constant deflection current and so a constant picture height has been obtained throughout the temperature range 25 °C to 85 °C.

For frame-output circuits using current feedback it is possible to make connection to the frame coils without the NTC-thermistor.

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Dimensions in mm





# Fig. 1

# TECHNICAL PERFORMANCE

Maximum working temperature Line deflection coils Connecting terminals Inductance Resistance Sensitivity Frame deflection coils Connecting terminals Inductance Resistance

Sensitivity

95  $^{\circ}$ C parallel connected, see Fig. 2 2 and 4 1.7 mH 3.6  $\Omega$ 108  $\mu$ Vs/cm series connected, see Fig. 3 6 and 8a (centre tap at A) 42 mH 30 $\Omega$ , between connecting terminals 6 and 8 38 $\Omega$ , between connecting terminals 6 and 8

 $\overbrace{2}^{7247698}$  Fig. 2 Fig. 3

 $9 \text{ mW/cm}^2$ 

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### MOUNTING

The unit should be mounted as far forward as possible on the neck of the picture tube, so that it touches the cone.

External circuit connection is made to soldering tags, positioned as indicated in Fig. 1.

To orient the raster correctly, the unit may be rotated by hand on the neck of the picture tube, with which it makes a slip fit. A screw-tightened clamping ring, cooperative with a pair of rubber friction shoes, permits it to be locked, both axially and radially, in the desired position.

# CENTRING THE BEAM

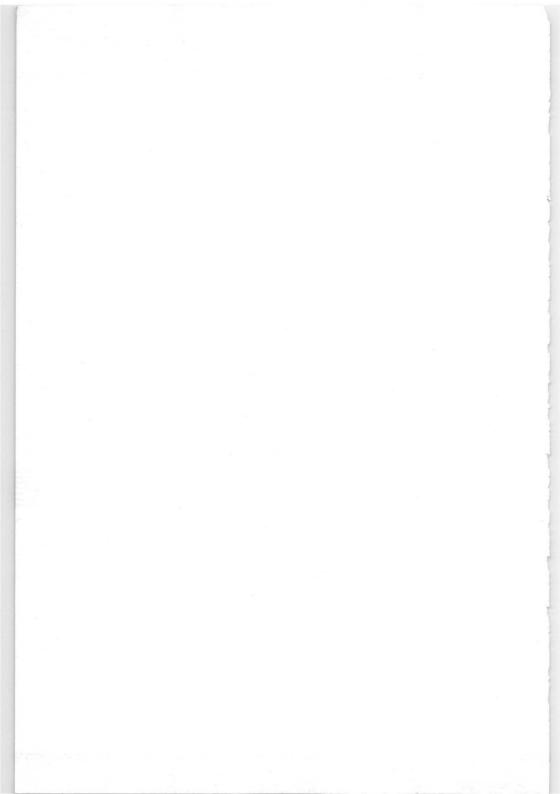
With the deflection unit mounted on the picture tube and clamped in position, the beam can be centred by rotating two, independently movable, steel magnet discs positioned adjacent the clamping ring.

# RASTER ADJUSTMENT POSSIBILITIES

Vertical pin-cushion distortion can be corrected by small ferroxdure rods, which can be mounted on the deflection unit brackets. Limited correction of asymmetrical vertical pincushion distortion can be achieved by unequal rotation of the rods.

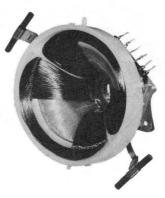
The shape of the corners of the raster can be adjusted by means of small rubber magnets having a centre hole to fit the pins on the rim of the deflection unit.

Both the ferroxdure rods (catalog number 4312 020 60101) and the rubber magnets (catalog number 3122 104 02721) can be supplied on request.



# **DEFLECTION UNIT**





RZ 20980-1

# For tube-equipped television receivers

### APPLICATION

This deflection unit has been designed for use with 110° (114°) picture tubes with a neck diameter of 28 mm in conjunction with the line-output transformer AT2025/01 and the linearity control unit AT4034/01 in tube-equipped television receivers.

### CONSTRUCTION

The saddle-shaped line deflection coils are moulded so that the deflection centre is well within the conical part of the picture tube.

The frame deflection coils are wound on a ferroxcube yoke ring which is flared so that the frame and line deflection centres coincide.

At the rear the line and frame deflection coils, as well as the yoke ring, are potted in polyester resin.

The unit is equipped with a built-in NTC thermistor connected in series with the frame deflection coils in order to compensate for temperature dependence of the coils. By this, in frame-output circuits with voltage feedback for linearising the saw-tooth voltage a constant deflection current and so a constant picture height has been obtained up to temperatures of 95 °C.

For frame-output circuits using current feedback it is possible to make connection to the frame coils without the NTC thermistor.

October 1968

Dimensions in mm

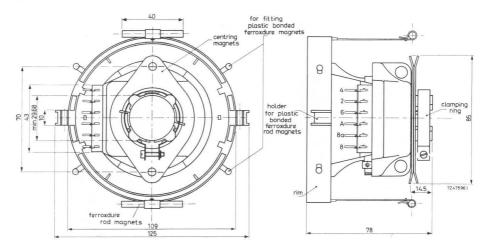


Fig. 1

### TECHNICAL PERFORMANCE

Maximum working temperature Line deflection coils Connecting terminals Inductance Resistance Deflection current at 18 kV for a deviation of 495 mm Sensitivity Frame deflection coils Connecting terminals Inductance Resistance between terminals 6 and 8 between terminals 6 and 8a at 25 °C Deflection current at 18 kV for a deviation of 390 mm Sensitivity

95 <sup>O</sup>C parallel connected, see Fig. 2 2 and 4 2.9 mH 4.6 Ω

2.29 A<sub>p-p</sub>
135 μVs/cm
series connected, see Fig. 3
6 and 8 (centre tap at A)
82 mH
38 Ω

#### 48 Ω

0.44 A<sub>p-p</sub> 4.8 mW/cm2

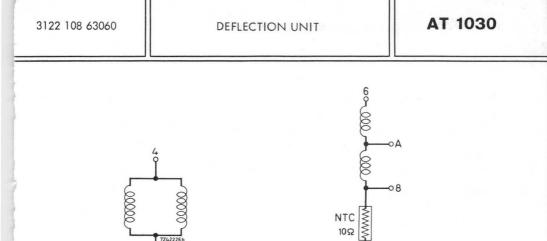


Fig. 2

#### MOUNTING

The unit should be mounted as far forward as possible on the neck of the picture tube, so that it touches the cone.

External circuit connection is made to soldering tags, positioned as indicated in Fig. 1.

To orient the raster correctly, the unit may be rotated by hand on the neck of the picture tube, with which it makes a slip fit. A screw-tightened clamping ring, cooperative with a pair of rubber friction shoes, permits it to be locked, both axially and radially, in the desired position.

# ADJUSTMENT POSSIBILITIES

#### Vertical pin-cushion distortion

Vertical pin-cushion distortion can be corrected by small ferroxdure rod magnets, which have been mounted on the deflection unit brackets. Limited correction of asymmetrical vertical pin-cushion distortion can be achieved by unequal rotation of these magnets.

#### Eccentricity of the picture tube

After adjustment of the linearity of the deflection current, the eccentricity of the picture tube and the deflection unit can be corrected by means of two independently movable centring magnets. These magnets are diametrically magnetised. By turning the magnets with respect to each other the magnetic force of the resultant field of both magnets is adjusted. The direction of the resultant magnetic field is adjusted by turning the magnets simultaneously.

It should be noted that these centring magnets can not be used for compensating the effects of non-linearity or of phase differences between synchronisation and time base, as otherwise the correction needed becomes excessive and, even if the correction is within the range of the magnets, curved lines may appear in the centre of the raster.

7Z42226a 2

8a

Fig. 3

#### Horizontal pin-cushion distortion

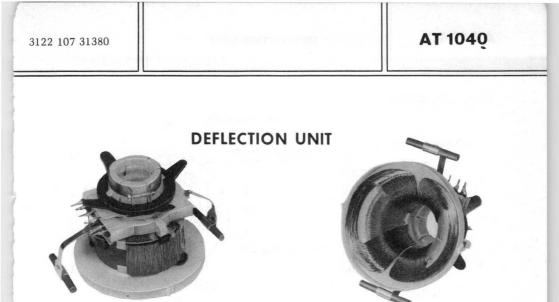
Horizontal pin-cushion distortion can be corrected by two rod magnets of plastic bonded ferroxdure, which can be mounted on the two holders on the rim.

When the deflection unit is used in conjunction with a 19 inch picture tube the use of these rod magnets is necessary to get an optimum raster.

These rod magnets can be supplied on request (catalog number 3122 104 90360).

# Shape of the corners of the raster

The shape of the corners can be adjusted by means of small plastic bonded ferroxdure magnets having a centre hole to fit the pins on the rim of the deflection unit. These four magnets can be supplied on request (catalog number 3122 104 93540).



RZ 24284-13

RZ 24284-14

For tube-equipped and transistor-equipped television receivers

### APPLICATION

This deflection unit has been designed for use with 110° (114°) picture tubes with a neck diameter of 28 mm. The unit can be driven by the line-output transformer AT2036 (standard), the AT2036/25 (which has auxiliary windings for  $3x110 V_p$ ) or the AT2034 (819/625 lines) in tube-equipped television sets, and by the AT2045 in fully transistorised television sets.

The standard frame output transformer is the AT3513, which can be used for tube and transistor-equipped television sets.

The linearity control is accomplished by the unit AT4042/02.

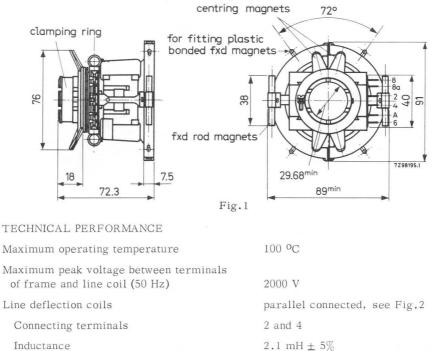
#### CONSTRUCTION

The frame deflection coils are wound on a ferroxcube yoke ring which is flared so that the frame and line deflection centres coincide.

The unit is equipped with a built-in NTC thermistor and a parallel resistor connected in series with the frame deflection coils in order to compensate for temperature dependence of the coils. By this, in frame-output circuits with voltage feedback for linearising the saw-tooth voltage a constant deflection current and so a constant picture height has been obtained up to temperatures of 100  $^{\rm O}$ C.

For frame-output circuits using current feedback it is possible to make connection to the frame coils without the temperature compensating network.

Dimensions in mm



Resistance

Peak to peak current

Frame deflection coils

Connecting terminals

Inductance

Resistance between terminals 6 and 8 between terminals 6 and 8a at 25 °C 2 and 4 2.1 mH  $\pm$  5% 3.9  $\Omega \pm$  10% 2.82 A  $\pm$  2.5% <sup>1</sup>) series connected, see Fig.3 6 and 8 (centre tap at A) 66 mH  $\pm$  10% 30  $\Omega \pm$  8% 44  $\Omega$  <sup>2</sup>)

Peak to peak current

545 mA <u>+</u> 5% <sup>3</sup>)

- 1) At 18 kV accelerator voltage and a deviation of  $495\,\mathrm{mm}$  on the 23 inch reference picture tube.
- 2) Variation of total circuit resistance within 10 to 95 °C is  $\pm 0.1~\Omega$  when using the output transformer AT3513.
- 3) At 18 kV accelerator voltage and a deviation of 390 mm on the 23 inch reference picture tube.

Characteristics measured at 18 kV accelerator voltage on a 23 inch reference picture tube:

Pin cushion distortion

Trapezium distortion

Barrel pattern distortion

Line asymmetry

Frame asymmetry

Eccentricity of deflection centre

Adjustment range of centring magnets

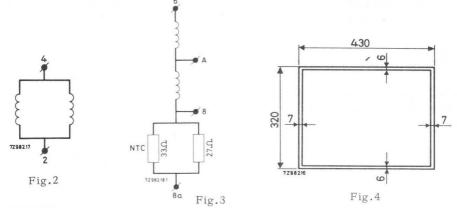
Geometry distortion 4)

3.5% 4) 3.5% 4) none 4) 1.5% 4) < 2 mm 4) > 5 mm diameter

< 45 mm diameter

< 15 mm diameter

Fig.4. The edges of the raster fall between the rectangles.



#### MOUNTING

The unit should be mounted as far forward as possible on the neck of the picture tube, so that it touches the cone.

External circuit connection is made to soldering tags, positioned as indicated in Fig.1.

To orient the raster correctly, the unit may be rotated by hand on the neck of the picture tube, with which it makes a slip fit. A screw-tightened clamping ring permits it to be locked, both axially and radially, in the desired position.

4) Measured without correction magnets.

### ADJUSTMENT FACILITIES

#### Vertical pin-cushion distortion

Vertical pin-cushion distortion can be corrected by small ferroxdure rod magnets, which have been mounted on the deflection unit brackets. Limited correction of a-symmetrical vertical pin-cushion distortion can be achieved by unequal rotation of these magnets.

#### Eccentricity of the picture tube

After adjustment of the linearity of the deflection current, the eccentricity of the picture tube and the deflection unit can be corrected by means of two independently movable centring magnets of plastic-bonded ferroxdure. These magnets are dia-metrically magnetised. By turning the magnets with respect to each other the magnetic force of the resultant field of both magnets is adjusted. The direction of the resultant magnetic field is adjusted by turning the magnets simultaneously.

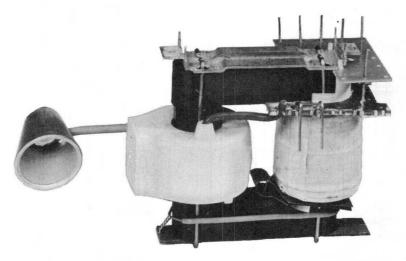
It should be noted that these centring magnets can not be used for compensating the effects of non-linearity or of phase differences between synchronisation and time base, as otherwise the correction needed becomes excessive and, even if the correction is within the range of the magnets, curved lines may appear in the centre of the raster.

#### Notes

To correct the corners of the raster small plastic bonded ferroxdure magnets can be supplied on request (catalog number 3122 104 94120).

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# LINE-OUTPUT TRANSFORMER



For tube-equipped television receivers Without auxiliary winding RZ 17574-1

#### APPLICATION

This line-output transformer has been developed to provide the required scanning amplitude for 19" or 23" picture tubes in television receivers presenting 625 lines at 50 frames per second (CCIR) or 525 lines at 60 frames per second (USA).

It is intended for use in conjunction with deflection unit AT 1030, linearity control unit AT 4034/01, line-output tube PL504, rectifying tube DY802 and booster diode PY 88. The EHT is stabilised at 18 kV.

# CONSTRUCTION

The magnetic circuit of the transformer comprises a ferroxcube U-core and a ferroxcube I-core. The primary winding 5-8 and the secondary windings 1-2 and 3-4 (see Fig. 2) are polyester dipped and situated on one leg of the core.

The EHT winding is polyester encapsulated and situated on the other leg.

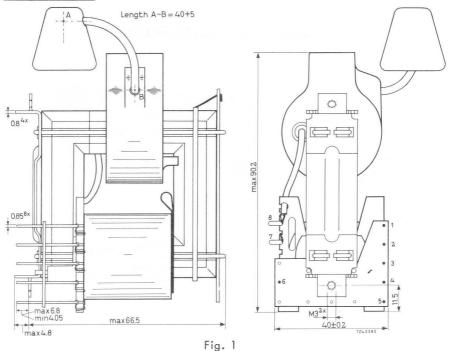
The transformer has been provided with four mounting pins and two threaded holes for mounting.

External circuit connection is made to connecting pins, positioned as indicated in Fig. 1.

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AT 2025/01





# ELECTRICAL DATA (see Fig. 2)

The electrical data are measured with a booster load at connection (5) of 1 mA and a capacitance of 100 pF between connections (1) and (4) at different values of capacitor C.4.

C 4	0	pF	120	) pF	270	Э́рF	
Beam current <sup>1)</sup>	35	400	35	400	35	400	μA
Supply voltage <sup>2)</sup>	240		240	225	240		V
Booster voltage	640		650	618	660		V
EHT voltage	18.1		18.0	16.4	17.6		kV
Overscan 1)	+ 6		+ 9		+12		%
Stability down to	194	205	195	205	197	208	V
Flyback ratio	17.2		17.5		17.9		%
Internal resistance of EHT		≤4.5		<u>≤</u> 4.5		$\leq$ 4.5	MΩ

A beam current increase of 200 μA results in an amplitude increase of maximum 2%.
 Internal resistance of power supply = 250 Ω.

3122 108 39100

LINE-OUTPUT TRANSFORMER

AT 2025/01

C 4	0	pF	120	) pF	270	) pF	
PY 88							
Average booster current	103		100	135	104		mA
Peak booster current	215	230	220	235	230	245	mA
Booster current at end of							
scan	5	60	5	50	5	55	mA
PL 504							
Peak cathode current	280	360	280	360	280	360	mA
Peak anode current			255	330			mA
Average screen-grid							
current			10	13			mA
Average screen-grid							
voltage			227	209			V
Anode dissipation				9			W
Screen-grid dissipation				3			W

The transformer core should not be left "floating", but must be connected to the chassis.

Driving pulse of the PL 504:

Cut-off time at least 19% at - 100V

Peak voltage higher than - 120 V

Slope of leading edge of driving pulse less than  $2\mu s$  per 100V. The shape of the driving pulse in the conducting period of the PL 504 should be such that the booster current at end-of-scan (measured with zero beam current) just does not disappear.

The maximum load on the transformer, including the booster load (but excluding the load of the VDR stabilization circuit) should not exceed 2.5W. This load results in a current increase of about 15mA.

The maximum capacitive load is (with a view to parasitic oscillations after flyback):

between (1) and (2) : 270 pF, absolute maximum permissible is e.g. (with C4 = 120 pF) :

270 pF between (1) (2) and 330 pF between (3) (4).

2) and	or:	120	pF	between	(1)	(2)
4).		390	pF	between	(3)	(4).

#### Line-output stage (see Fig. 2)

C1	4700 pF ceramic
C2	1500 pF ceramic
C3	270 pF ceramic,1000∨ <sub>dc</sub> 0-270 pF ceramic,2000∨ <sub>p-p</sub> ,
C4	0-270 pF ceramic, 2000 ∨ p-p,
	amplitude adjustment
C5	22000 pF paper } 1300∨, booster 56000 pF paper } capacitors
C7	56000 pF paper ) capacitors
C6	0.18 μF (5 %) 0.20 μF (5 %)
C8	0.20 µF (5%)
1) T	

ooster
nent

1) The picture width depends on this value.

2) With low supply voltage, dissipation may exceed 1 W.

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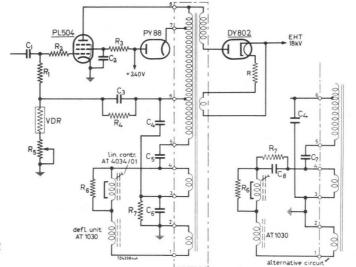
G21

and

# AT 2025/01

#### LINE-OUTPUT TRANSFORMER

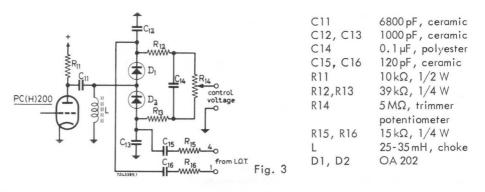
Fig. 2a





The operation of the transformer is influenced by its surroundings. Variations in electrical characteristics due to the influence of surrounding components, shields and circuitry can be compensated to a certain degree by selecting the right value for the capacitor C4 parallel to part of the transformer primary.

The deflection unit is connected to a secondary which is separated from the primary by the booster capacitor C 5. Pulses for blanking, synchronisation, etc. are to be taken directly from the deflection unit connections. There is no auxiliary winding on this transformer. A circuit diagram of a flywheel synchronisation circuit is given below.



The split secondary offers two possibilities to the setmaker. If the transformer is connected according to Fig. 2a, the conventional circuit is obtained, with booster capacitor C7 = 56 nF and S-correction capacitor  $C8 = 200 \text{ nF} (\pm 5\%)$ .

If, however, the S-correction capacitor is placed between the two halves of the secondary (C6 in Fig. 2), the booster capacitance has to be reduced considerably (22nF instead of 56nF) because the parabola voltages on C6 and C5 are of opposite sign. Besides, the S-correction capacitor has to be reduced (180nF). This means an important saving in cost.

From connection (3) a parabola-shaped voltage of 90  $\rm V_{p-p}$  can be taken for use in the TV set.

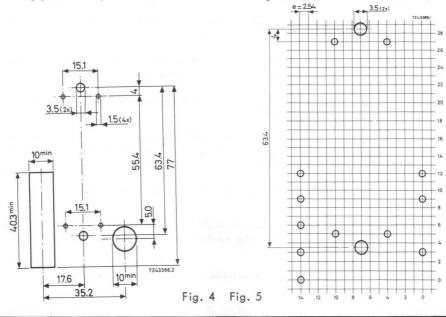
If the resistive load on connection (3) is about  $2700 \Omega$  or less, the resistor R7 (damping resistor against dynatron oscillations) can be omitted. The load resistance should, however, not be lower than about  $820 \Omega$ .

If the boosted d.c. voltage is needed elsewhere in the set, it has to be filtered from the booster parabola voltage and from the flyback peaks.

### MOUNTING

The transformer can be mounted on either a printed-wiring board or a metal chassis. The latter should be apertured as shown in the mounting diagram, Fig. 4, to pass the pins. The transformer is secured by two 3mm screws. The mounting pins can be bent or soldered.

When mounted on a printed-wiring board the transformer is secured by means of its four mounting pins and two 3mm screws. The fit of the connecting pins in a printed-wiring grid with a pitch of 0.1" is illustrated in Fig. 5.



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AT 2025/01

Like the other connections, those to the PL 504 and PY 88 can be soldered to the printed-wiring board. If bent upwards (as supplied) they are very suitable for direct connection to the anode caps of these tubes.

A tube socket for the DY802 (type AT7130) comprising a resistor (R, Fig.2) of 1.6 Ω is available; for ordering this socket the catalog number 3122 107 31240 should be used. See also the relevant data sheet.

Certain minimum distances between the transformer and neighbouring components and shields must be maintained.

- The radial distance between the EHT coils and any flat metal part (free from sharp edges) should be at least 25 mm.

The axial distance from the EHT coil should be at least 15 mm.

- The distance from the EHT cap and lead should be at least 25 mm.
- The distance between the primary coil and any flat and smooth metal part should be at least 10 mm.
- The distance between the upper edge of the DY802 socket and the primary coil should be at least 7 mm.

In the design of a printed-wiring board and also of a handwired chassis the following peak pulse voltages should be taken into account:

Connection	(1)		:	-	500 V <sub>p-p</sub>
	(5),	(4)	:	+	500 Vp-p
	(6)				1100 Vp-p

The capacitance of the leads to the PL 504 and PY 88 caps should be less than 2 pF.

Note: The transformer and the leads and components carrying high tension pulses should be kept free from metal particles, solder drops etc.

The operating temperature of the transformer coils and the core should not exceed 95 °C under worst circumstances, i.e. taking into account:

overvoltage

- low atmospheric pressure (at high altitudes) implying bad cooling by convection

- high room temperature (up to 45 °C).

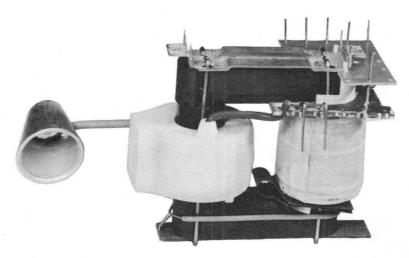
Direct heat radiation from the PL 504 and PY 88 anodes to the transformer and the heater cable should be avoided by a screen. (If this screen is made from insulating material, it should be placed at least 15 mm from the coils.)

The socket of the DY802 should not be exposed to any direct heat radiation from the PL 504 and the PY 88.

The heater cable should be able to withstand 95 °C without the risk of the copper core damaging the insulating material under mechanical stress; a p.v.c. sleeve for mechanical protection is sufficient.

Ample cool air circulation should be provided around the transformer.

# LINE-OUTPUT TRANSFORMER



RZ 17574-1

For tube-equipped television receivers Without auxiliary winding

### APPLICATION

This line-output transformer has been developed to provide the required scanning amplitude for 17, 19, 20, 23 or 24 inch picture tubes in television receivers presenting 625 lines at 50 frames per second (CCIR) or 525 lines at 60 frames per second (USA).

It is intended for use in conjunction with deflection unit AT1040, linearity control unit AT4042/02, line-output tube PL504, rectifying tube DY802 and booster diode PY88. The EHT is stabilised at 18 kV.

#### CONSTRUCTION

The magnetic circuit of the transformer comprises a ferroxcube U-core and a ferroxcube I-core. The primary winding 5-8 and the secondary windings 1-2 and 3-4 (see Fig.2) are polyester dipped and situated on one leg of the core.

The EHT winding is polyester encapsulated and situated on the other leg.

The transformer has been provided with four mounting pins and two threaded holes for mounting.

External circuit connection is made to connecting pins, positioned as indicated in Fig.1.

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#### Dimensions in mm

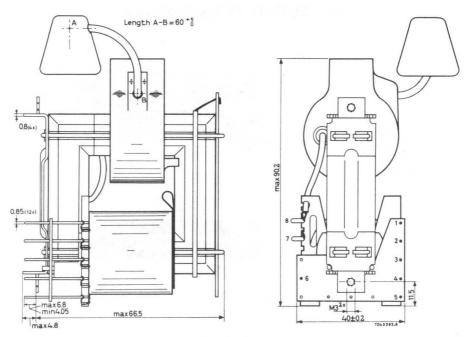


Fig.1

#### ELECTRICAL DATA (see Fig.2)

The electrical data are measured with a booster load at connection (5) of 1 mA and a capacitance of 100 pF between connections (1) and (4), at different values of capacitor C4.

C4	120	120 pF		270 pF		390 pF	
Beam current <sup>1</sup> )	35	400	35	400	35	400	μA
Supply voltage 2)	240	234	240	234	240	234	V
Booster voltage	632	616	640	622	648	632	V
EHT voltage	18.3	17.0	18.2	16.9	18.1	16.8	kV
Overscan 1)	+7		+9		+11		%
Stability down to	212	217	215	220	217	222	V
Flyback ratio	16.8		17		17.2		%
Internal resistance of EHT		$\leq 4.5$		$\leq 4.5$		$\leq 4.5$	MΩ

 $^{\rm I}$  ) A beam current increase of 200  $\mu {\rm A}$  results in an amplitude increase of maximum 2% .

2) Internal resistance of power supply = 180  $\Omega$ .

C4	120 pF	270	) pF	390 pF		
PY88						
Average booster current	110 150	109	149	110	150	mA
Peak booster current	250	250		250		mA
Booster current at end						
of scan	50	50		50		mA
Peak booster voltage		5,4				kV
PL504				-		
Peak cathode current		280	330			mA
Peak anode current		270	320			mA
Average screen-grid						
current		10				mA
Average screen-grid						
voltage		220				V
Anode dissipation			11.5			W
Screen-grid dissipation		3				W
Peak anode voltage		6.8				kV

The transformer core should not be left "floating", but must be connected to the chassis.

Driving pulse of the PL504:

Cut-off time at least 19% at -100 V

Peak voltage higher than -120 V

Slope of leading edge of driving pulse less than  $2 \ \mu s$  per 100 V. The shape of the driving pulse in the conducting period of the PL504 should be such that the booster current at end-of-scan (measured with zero beam current) just does not disappear.

The maximum load on the transformer, including the booster load (but excluding the load of the VDR stabilization circuit) should not exceed 2.5 W. This load results in a current increase of about 15 mA.

The maximum capacitive load is (with a view to parasitic oscillations after flyback):

to be established

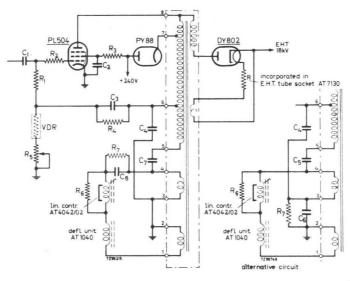
#### Line-output stage (see Fig.2)

C1	4700 pF ceramic	R1	2.2 MΩ, 1200 V <sub>p-p</sub>
C2	22000 pF ceramic	R2	1000 Ω, 1/4 W
C3	270 pF ceramic, 1000 V <sub>dc</sub>	R3	2200 Ω, 2 W <sup>2</sup> )
C4	120-390 pF ceramic, 2000 V <sub>p-p</sub> ,	R4	10 MΩ, 1200 V <sub>dc</sub>
	amplitude adjustment	R5	$0.5 M\Omega$ , potentiometer, booster
C5	27000 pF) paper, 1300 V		voltage adjustment
C7	56000 pF booster capacitors	R6	1500 Ω, 1 W
C6		R7	2700 Ω, 1 W
C6 C8	$0.22 \ \mu F(5\%) \\ 0.27 \ \mu F(5\%) \\ S \text{-correctors}^{1}$	VDR	2322 564 90014 (910 V)

1) The picture width depends on this value.

2) With low supply voltage, dissipation may exceed 1 W.

3122 108 32410

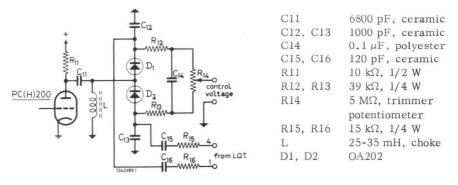


# Fig.2.

Fig.2a

The operation of the transformer is influenced by its surroundings. Variations in electrical characteristics due to the influence of surrounding components, shields and circuitry can be compensated to a certain degree by selecting the right value for the capacitor C4.

The deflection unit is connected to a secondary which is separated from the primary by the booster capacitor C7. Pulses for blanking, synchronisation, etc. are to be taken directly from the deflection unit connections. There is no auxiliary winding on this transformer. A circuit diagram of a flywheel synchronisation circuit is given below.





The split secondary offers two possibilities to the setmaker. If the transformer is connected according to Fig.2, the conventional circuit is obtained, with booster capacitor C7 = 56 nF and S-correction capacitor C8 = 270 nF ( $\pm 5\%$ ).

If, however, the S-correction capacitor is placed between the two halves of the secondary (C6 in Fig.2a), the booster capacitance has to be reduced considerably (27 nF instead of 56 nF) because the parabola voltages on C6 and C5 are of opposite sign. Besides, the S-correction capacitor has to be reduced (220 nF). This means an important saving in cost.

From connection (3) a parabola-shaped voltage of 90  $\rm V_{p-p}$  can be taken for use in the TV set.

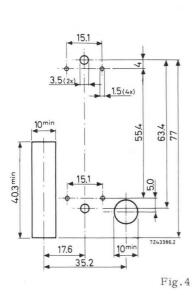
If the resistive load on connection (3) is about 2700  $\Omega$  or less, the resistor R7 (damping resistor against dynatron oscillations) can be omitted. The load resistance should, however, not be lower than about 820  $\Omega$ .

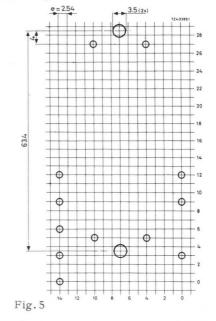
If the boosted d.c. voltage is needed elsewhere in the set, it has to be filtered from the booster parabola voltage and from the flyback peaks.

#### MOUNTING

The transformer can be mounted on either a printed-wiring board or a metal chassis. The latter should be apertured as shown in the mounting diagram, Fig.4, to pass the pins. The transformer is secured by two 3 mm screws. The mounting pins can be bent or soldered.

When mounted on a printed-wiring board the transformer is secured by means of its four mounting pins and two 3 mm screws. The fit of the connecting pins in a printed-wiring grid with a pitch of 0.1 inch is illustrated in Fig.5.





Like the other connections, those to the PL504 and PY88 can be soldered to the printed-wiring board. If bent upwards (as supplied) they are very suitable for direct connection to the anode caps of these tubes.

A tube socket for the DY802 (type AT7130) comprising a resistor (R, Fig.2) of 1.6  $\Omega$  is available, for ordering this socket use the catalog number 3122 107 31240. See also the relevant data sheet.

Certain minimum distances between the transformer and neighbouring components and shields must be maintained.

- The radial distance between the EHT coils and any flat metal part (free from sharp edges) should be at least 25 mm.
  - The axial distance from the EHT coil should be at least 15 mm.
- The distance from the EHT cap and lead should be at least 25 mm.
- The distance between the primary coil and any flat and smooth metal part should be at least 10 mm.
- The distance between the upper edge of the DY802 socket and the primary coil should be at least 7 mm.

In the design of a printed-wiring board and also of a handwired chassis the following peak pulse voltages should be taken into account:

Connection	(1)		:	-	500	Vp-p
	(5),	(4)	:	$^+$	500	Vp-p
	(6)		:	+ .	1100	V <sub>p-p</sub>

The capacitance of the leads to the PL504 and PY88 caps should be less than 2 pF.

Note: The transformer and the leads and components carrying high tension pulses should be kept free from metal particles, solder drops etc.

The operating temperature of the transformer coils and the core should not exceed 95  $^{\rm o}{\rm C}$  under worst circumstances, i.e. taking into account:

- overvoltage

- low atmospheric pressure (at high altitudes) implying bad cooling by convection

- high room temperature (up to 45 °C).

Direct heat radiation from the PL504 and PY88 anodes to the transformer and the heater cable should be avoided by a screen. (If this screen is made from insulating material, it should be placed at least 15 mm from the coils.)

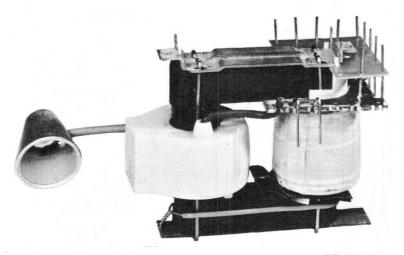
The socket of the DY802 should not be exposed to any direct heat radiation from the PL504 and the PY88.

The heater cable should be able to withstand 95  $^{\circ}$ C without the risk of the copper core damaging the insulating material under mechanical stress; a p.v.c. sleeve for mechanical protection is sufficient.

Ample cool air circulation should be provided around the transformer.

# AT 2036/25

# LINE-OUTPUT TRANSFORMER



RZ 17574-1R

For tube-equipped television receivers With auxiliary winding

#### APPLICATION

This line-output transformer has been developed to provide the required scanning amplitude for 17, 19, 20, 23 or 24 inch picture tubes in television receivers presenting 625 lines at 50 frames per second (CCIR) or 525 lines at 60 frames per second (USA).

It is intended for use in conjunction with deflection unit AT1040, linearity control unit AT4042/02, line-output tube PL504, rectifying tube DY802 and booster diode PY88. The EHT is stabilised at 18 kV.

### CONSTRUCTION

The magnetic circuit of the transformer comprises a ferroxcube U-core and a ferroxcube I-core. The primary winding 9-12, the secondary windings 5-6 and 7-8 and the auxiliary winding 1-4 (see Fig.2) are polyester dipped and situated on one leg of the core. The EHT winding is polyester encapsulated and situated on the other leg.

The transformer has been provided with four mounting pins and two threaded holes for mounting.

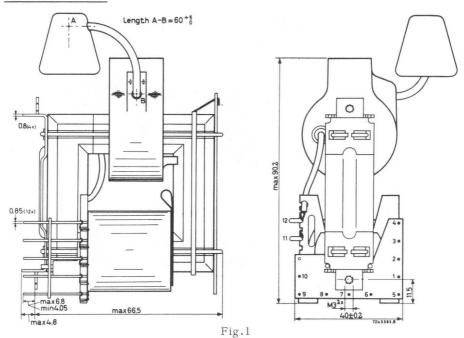
External circuit connection is made to connecting pins, positioned as indicated in Fig.1.

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3122 107 31760

Dimensions in mm



# → ELECTRICAL DATA (see Fig.2)

The electrical data are measured with a booster load at connection (9) of 1 mA and a capacitance of  $100 \, \text{pF}$  between connections (5) and (8) at different values of capacitor C4.

C4	120 pF		270	pF	390 pF		
Beam current <sup>1</sup> )	35	400	35	400	35	400	μΑ
Supply voltage 2)	240	234	240	234	240	234	V
Booster voltage	632	616	640	622	648	632	V
EHT voltage	18.9	17.0	18.2	16.9	18.1	16.8	kV
Overscan <sup>1</sup> )	+7		+9		+11		%
Stability down to	212	217	215	220	217	222	V
Flyback ratio	16.8		17		17.2		%
Internal resistance of EHT		$\leq 4.5$		$\leq 4.5$		$\leq 4.5$	MS

 $^1)$  A beam current increase of 200  $\mu A$  results in an amplitude increase of maximum 2%.

2) Internal resistance of power supply =  $180 \Omega$ .

3122 107 31760

AT 2036/25

C4	12	0 pF	270 pF		39	0 pF	
Auxiliary voltage between							
(1) and (2)			-	110			Vp-p
Auxiliary voltage between							
(3) and (2)			+	110			Vp-p
Auxiliary voltage between				220			37
(4) and (2)			+	220			Vp-p
PY88							
Average booster current	110	150	109	149	110	150	mA
Peak booster current	250		250	250	250		mA
Booster current at end							
of scan	50		50	100	50		mA
Peak booster voltage			5.4				kV
PL504							
Peak cathode current			280	330			mA
Peak anode current			270	320			mA
Average screen-grid							
current			10				mA
Average screen-grid			220				
voltage			220				V
Anode dissipation			3	11.5			W
Screen-grid dissipation Peak anode voltage			6.8				W kV

The transformer core should not be left "floating", but must be connected to the chassis.

Driving pulse of the PL504:

Cut-off time at least 19% at -100 V

Peak voltage higher than -120 V

Slope of leading edge of driving pulse less than  $2 \,\mu s$  per 100 V. The shape of the driving pulse in the conducting period of the PL504 should be such that the booster current at end-of-scan (measured with zero beam current) just does not disappear.

The maximum load on the transformer, including the booster load (but excluding the load of the VDR stabilization circuit) should not exceed 2.5 W. This load results in a current increase of about 15 mA.

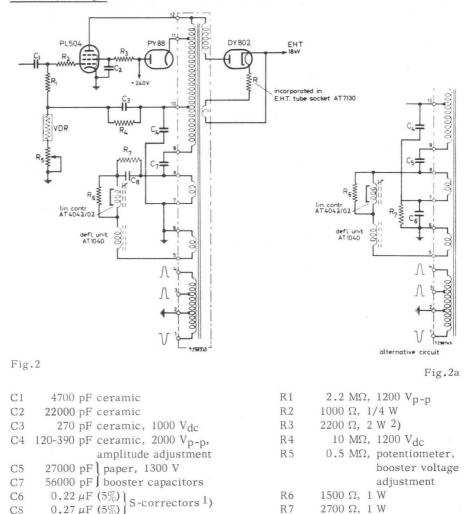
The maximum capacitive load is (with a view to parasitic oscillations after flyback):

to be established

AT 2036/25

#### 3122 107 31760

Line-output stage



1) The picture width depends on this value.

2) With low supply voltage, dissipation may exceed 1 W.

G34

2322 564 90014 (910 V)

VDR

The operation of the transformer is influenced by its surroundings. Variations in electrical characteristics due to the influence of surrounding components, shields and circuitry can be compensated to a certain degree by selecting the right value for the capacitor C4.

The deflection unit is connected to a secondary which is separated from the primary by the booster capacitor C7. Pulses for blanking, synchronisation, etc. are to be taken directly from the deflection unit connections. There is an auxiliary winding on this transformer, which delivers +110 V<sub>p-p</sub>, +220 V<sub>p-p</sub> and -110 V<sub>p-p</sub> if connection (2) is connected to earth. A circuit diagram of a flywheel synchronisation circuit is given below.

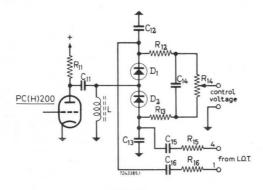


Fig.3

C11	6800 pF, ceramic
C12, C13	1000 pF, ceramic
C14	0.1 $\mu$ F, polyester
C15, C16	120 pF, ceramic
R11	10 kΩ, 1/2 W
R12, R13	39 kΩ, 1/4 W
R14	5 M $\Omega$ , trimmer potentiometer
R15, R16	15 kΩ, 1/4 W
L	25-35 mH, choke
D1, D2	OA202

The split secondary offers two possibilities to the setmaker. If the transformer is connected according to Fig.2, the conventional circuit is obtained, with booster capacitor C7 = 56 nF and S-correction capacitor C8 = 270 nF ( $\pm$  5%).

If, however, the S-correction capacitor is placed between the two halves of the secondary (C6 in Fig.2a), the booster capacitance has to be reduced considerably (27 nF instead of 56 nF) because the parabola voltages on C6 and C5 are of opposite sign. Besides, the S-correction capacitor has to be reduced (220 nF). This means an important saving in cost.

AT 2036/25

From connection (7) a parabola-shaped voltage of 90  $\rm V_{p-p}$  can be taken for use in the TV set.

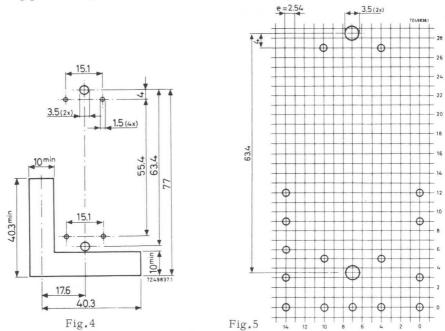
If the resistive load on connection (7) is about 2700  $\Omega$  or less, the resistor R7 (damping resistor against dynatron oscillations) can be omitted. The load resistance should, however, not be lower than about 820  $\Omega$ .

If the boosted d.c. voltage is needed elsewhere in the set, it has to be filtered from the booster parabola voltage and from the flyback peaks.

#### MOUNTING

The transformer can be mounted on either a printed-wiring board or a metal chassis. The latter should be apertured as shown in the mounting diagram, Fig.4, to pass the pins. The transformer is secured by two 3 mm screws. The mounting pins can be bent or soldered.

When mounted on a printed-wiring board the transformer is secured by means of its four mounting pins and two 3 mm screws. The fit of the connecting pins in a printed-wiring grid with a pitch of 0.1 inch is illustrated in Fig.5.



Like the other connections, those to the PL504 and PY88 can be soldered to the printed-wiring board. If bent upwards (as supplied) they are very suitable for direct connection to the anode caps of these tubes.

A tube socket for the DY802 (type AT7130) comprising a resistor (R, Fig.2) of 1.6  $\Omega$  is available; for ordering this socket use the catalog number 3122 107 31240. See also the relevant data sheet.

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Certain minimum distances between the transformer and neighbouring components and shields must be maintained.

- The radial distance between the EHT coils and any flat metal part (free from sharp edges) should be at least 25 mm.
- The axial distance from the EHT coil should be at least 15 mm.
- The distance from the EHT cap and lead should be at least 25  $\,\rm mm$  .
- The distance between the primary coil and any flat and smooth metal part should be at least 10 mm.
- The distance between the upper edge of the DY802 socket and the primary coil should be at least 7 mm.

In the design of a printed-wiring board and also of a handwired chassis the following peak pulse voltages should be taken into account:

Connection (1) :  $-110 V_{p-p}$ (3) :  $+110 V_{p-p}$ (4) :  $+220 V_{p-p}$ (5) :  $-500 V_{p-p}$ (9) :  $+500 V_{p-p}$ (10) :  $+1100 V_{p-p}$ 

The capacitance of the leads to the PL504 and PY88 caps should be less than 2 pF.

Note: The transformer and the leads and components carrying high tension pulses should be kept free from metal particles, solder drops etc.

The operating temperature of the transformer coils and the core should not exceed 95 oC under worst circumstances, i.e. taking into account:

- overvoltage

- low atmospheric pressure (at high altitudes) implying bad cooling by convection

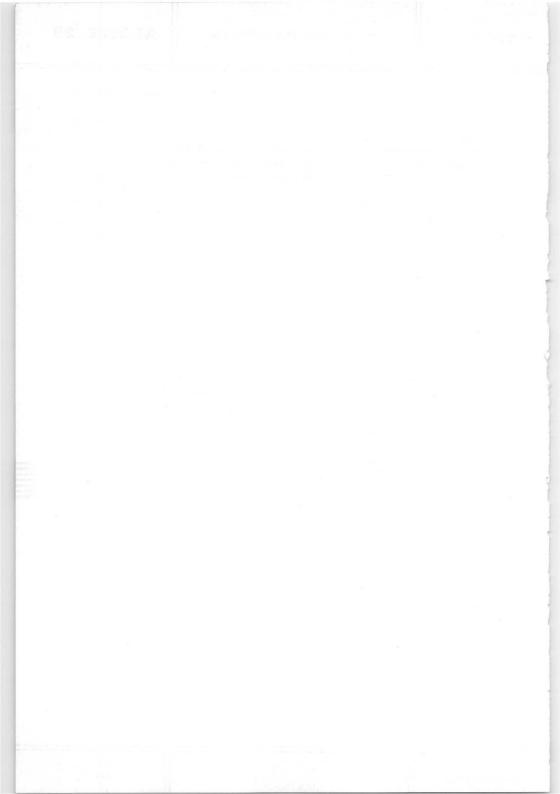
- high room temperature (up to 45 °C).

Direct heat radiation from the PL504 and PY88 anodes to the transformer and the heater cable should be avoided by a screen. (If this screen is made from insulating material, it should be placed at least 15 mm from the coils).

The socket of the DY802 should not be exposed to any direct heat radiation from the PL504 and the PY88.

The heater cable should be able to withstand 95  $^{\rm OC}$  without the risk of the copper core damaging the insulating material under mechanical stress; a p.v.c. sleeve for mechanical protection is sufficient.

Ample cool air circulation should be provided around the transformer.

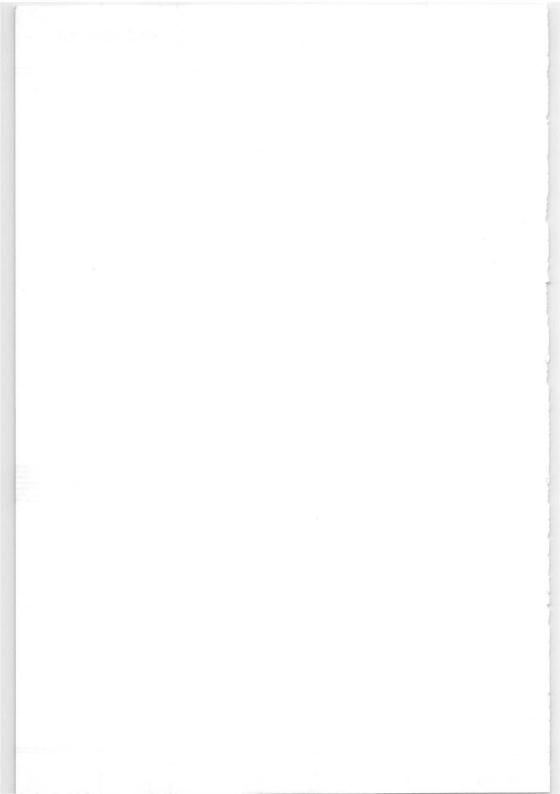


# AT 2036/36

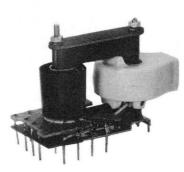
# LINE-OUTPUT TRANSFORMER

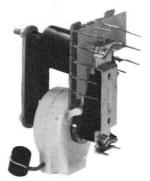
This line-output transformer is derived from the AT2036/25. Provided with an E.H.T. lead of 75 + 5 mm, without E.H.T. cap, it can be used with E.H.T. solid-state rectifier stacks.

For further data, see data sheets of the line-output transformer AT2036/25.



# LINE-OUTPUT TRANSFORMER





RZ 20305-1



# APPLICATION

This line-output transformer has been developed to provide the required scanning amplitude for the 11 inch 90° picture tube A28-14W and the 12 inch 90° picture tube A31-20W in transistor-equipped television receivers presenting 625 lines at 50 frames per second (C.C.I.R.) or 525 lines at 60 frames per second (U.S.A.). It is intended for use in conjunction with deflection unit AT1020/01, linearity control unit AT4036, line-output transistor AU103, parallel diode BY118 and rectifying tube DY51.

### CONSTRUCTION

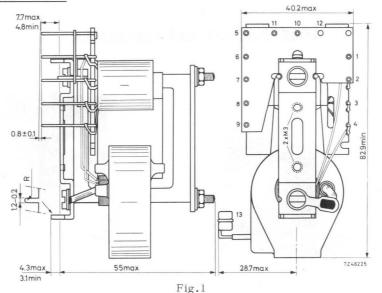
The magnetic circuit of the transformer comprises two ferroxcube U-cores. The primary winding 1-4 and the secondary windings 5-12 and 10-11 (see Fig.2) are situated on one leg of the transformer. On the opposite leg, the E.H.T. winding is situated. This winding is polyester-encapsulated and is terminated in a conductive rubber grommet in which the anode lead of the E.H.T. rectifier may be inserted.

The transformer has been provided with four mounting pins and two threaded holes for mounting.

External circuit connection is made to connecting pins, positioned as indicated in Fig.1.

### 3122 107 30370

#### Dimensions in mm



## - ELECTRICAL DATA

E.H.T. voltage (no load)	11 kV
Flyback ratio	17.5 %
Average current	0.52 A
Overscan	5 %

The values mentioned above have been measured with an extra winding on the transformer (load of 1 W) and including a heating power of the E.H.T. rectifier DY51 of 0.77 W.

#### Line-output stage

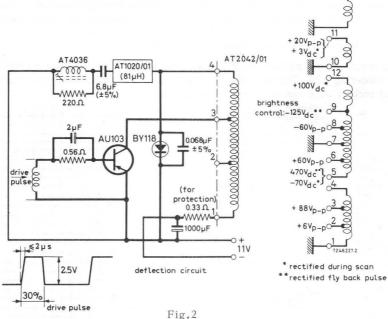
The line-output circuit of Fig.2 is designed around the line-output transistor AU103, the parallel diode BY118 and the E.H.T. rectifier DY51.

The circuit is fed from a stabilized power supply at 11 V and driven by a pulse of the shape shown.

The deflection unit AT1020/01 and the series connected adjustable linearity control unit AT4036 are connected in parallel with the diode BY118. The 0.068  $\mu F$  capacitor and the various parasitic capacitances of the transformer form, together with the inductances of the deflection unit and the transformer, a resonant LC circuit which determines the flyback time.

AT 2042/01

rectifier -C



1 1g.2

To damp ringing oscillations, the coil of the linearity control unit must be shunted by a 220  $\Omega$ , 1 W, carbon resistor. To prevent spurious oscillations, which would manifest themselves as ringing bars in the picture, the connecting leads should be as short as possible. In Fig.2 the critical leads are indicated by heavy lines. The 0.068  $\mu$ F capacitor, especially, should be closely connected to the parallel diode BY118.

The heater current for the DY51 may be supplied by two turns around the cross member of the transformer core, in series with a resistor of 0.5  $\Omega$ .

The supply voltage for the transistor in the video-output stage of the receiver and for the first anode and focus electrode of the picture tube is available at terminal 5.

The supply voltage for the brightness control of the picture tube is provided by the winding 9-12.

Symmetrical voltage pulses of 60 V for a.g.c. gating and horizontal synchronizing circuits are available at terminals 6 and 8.

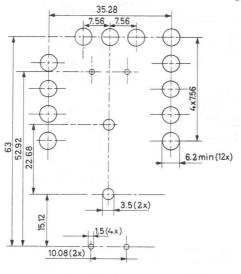
Where a d.c. voltage with low spread in value and low internal resistance is required, the best way to obtain it is by rectification during the scan. Less critical voltages can be obtained by pulse rectification during flyback.

## MOUNTING

The transformer can be mounted on either a printed-wiring board or a metal chassis. The latter should be provided with holes as shown in the mounting diagram, Fig.3.

The transformer is secured by two 3 mm screws.

When mounted on a printed-wiring board, the transformer is secured by means of four soldering lugs. The fit of the terminal pins in a printed-wiring grid with a pitch of 0.1 inch or 2.50 mm is illustrated in Fig.4.



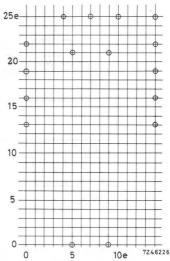




Fig.4 (e = 0.1 inch or 2.50 mm)

Whether it is board- or chassis-mounted the core of the transformer must be earthed.

A special tube socket for the DY51 rectifier (type number AT7108/50) is delivered with the line-output transformer. The socket includes a plate with soldering tags for making circuit connections to the tube, and can be secured to the transformer by means of a screw.

The following minimum distances between the transformer and neighbouring conductive surfaces must be maintained:

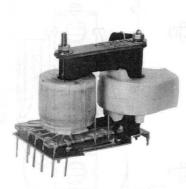
- radially from the E.H.T. winding, 18 mm
- axially from the E.H.T. winding, 10 mm
- radially and axially from the primary winding, 8 mm.

To avoid corona discharge, care must be taken that the anode lead of the E.H.T. rectifier does not protrude beyond the rubber grommet.

3122 108 39260

AT 2043

# LINE-OUTPUT TRANSFORMER





·RZ 20305-2

## For tube-equipped television receivers

### APPLICATION

This line-output transformer has been developed to provide the required scanning amplitude for the 11 inch 90° picture tube A28-14W and the 12 inch 90° picture tube A31-20W in tube-equipped television receivers presenting 625 lines at 50 frames per second (C.C.I.R.) or 525 lines at 60 frames per second (U.S.A.).

It is intended for use in conjunction with deflection unit AT1021/01, linearity control unit AT4037, line-output tube PL81, booster diode PY81 and rectifying tube DY51.

Thanks to the low deflection power requirement of the picture tubes mentioned above, the transformer losses are small and its operating temperature is, therefore, advantageously low, which is important in view of the use of semiconductor devices in the television receiver.

#### CONSTRUCTION

The magnetic circuit of the transformer comprises two ferroxcube U-cores. The primary winding 9-12, secondary windings 1-2 and 3-4 and auxiliary windings 5-6 and 7-8 (see Fig.2) are polyester dipped and situated on one leg of the core.

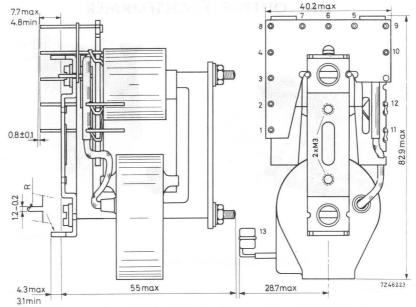
The E.H.T. winding 10-13 is polyester encapsulated and situated on the other leg. Terminal 13 is a conductive rubber grommet in which the anode lead of the E.H.T. rectifier may be inserted.

The transformer has been provided with four mounting pins and two threaded holes for mounting.

External circuit connection is made to connecting pins, positioned as indicated in Fig.1.

October 1968

### Dimensions in mm





## --- ELECTRICAL DATA

E.H.T. voltage (no load) Booster voltage Flyback ratio Average current Overscan Maximum load capability of auxiliary windings 5-6 and 7-8 11 kV 240 + 440 = 680 V 17.5 % 38 mA 5 %

0.7 W, during scan 0.3 W, during flyback

#### Line-output stage

The circuit of Fig.2 is designed around the line-output tube PL81, the booster diode PY81, and the E.H.T. rectifier DY51.

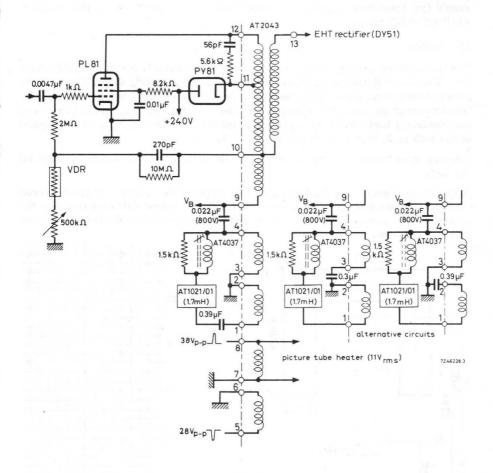
The stabilizing circuit for the supply voltage includes the voltage-dependent resistor 2322 564 90014, which operates down to a supply voltage of about 205 V.

The stabilizing circuit must be adjusted to the nominal value of the booster voltage (680 V) at the nominal value of the supply voltage (240 V) by means of the 500 k $\Omega$  potentiometer.

3122 108 39260

AT 2043

One terminal of the 0.022  $\mu$ F booster capacitor is connected to the positive terminal of the voltage supply, so that at an adjusted voltage of 440 V across the capacitor the total booster voltage is 680 V. The scanning amplitude and E.H.T. will then be correct, since the line-output transformer has been made for the proper ratio of booster voltage, E.H.T. and scanning amplitude, within narrow tolerances. The drive voltage must be adjusted so that the booster diode conducts throughout the whole scanning period, the booster current at the end of the scan ranging from 5 to 10 mA.





The deflection unit AT1021/01 and the adjustable linearity control unit AT4037 are connected to the secondary winding 1-4 of the line-output transformer. The split secondary winding offers the set manufacturer three possible modes of connection.

To minimize ringing oscillations after flyback, the linearity control unit AT4037 must be connected nearest to terminal 4, that is, to the "positive" side of the deflection unit AT1021/01. In addition, the coil of the linearity control unit must be shunted by a 1500  $\Omega$ , 1 W, carbon resistor.

The heater current for the DY51, may be supplied by a single turn around the cross member of the transformer core, without series resistor.

The heater supply for the picture tube is provided by the auxiliary winding 7-8, which delivers a peak-to-peak voltage of 38 V, corresponding to 11  $V_{\rm TMS}$ . Current supply for transistor circuits in hybrid receivers is provided by the auxiliary winding 5-6 (28  $V_{\rm p-p}$ ).

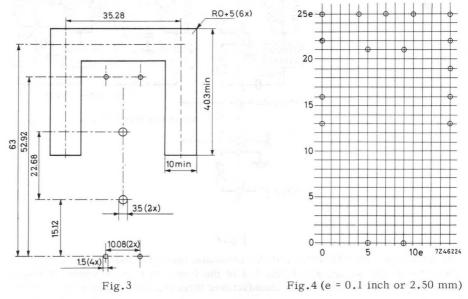
#### MOUNTING

The transformer can be mounted on either a printed-wiring board or a metal chassis. The latter should be apertured as shown in the mounting diagram, Fig.3, to pass the connecting pins. The transformer is secured by two 3 mm screws.

When mounted on a printed-wiring board, the transformer is secured by means of four soldering lugs. The fit of the terminal pins in a printed-wiring grid with a pitch of 0.1 inch or 2.50 mm is illustrated in Fig.4.

Whether it is board- or chassis-mounted, the core of the transformer must be earthed.

A special tube socket for the DY51 rectifier (type number AT7108/51) is delivered with the line-output transformer. The socket includes a plate with soldering tags for making circuit connections to the tube, and can be secured to the transformer by means of a screw.



The following minimum distances between the transformer and neighbouring conductive surfaces must be maintained:

- radially from the E.H.T. winding, 18 mm

- axially from the E.H.T. winding, 10 mm

- radially and axially from the primary winding, 8 mm.

To avoid corona discharge, care must be taken that the anode lead of the EHT rectifier does not protrude beyond the rubber grommet.



# FRAME-OUTPUT TRANSFORMER



RZ 24284-11

# For tube -equipped and transistorised television receivers

### APPLICATION

This frame-output transformer is intended for use with 19 and 23 inch  $110^{\circ}$  (114°) picture tubes, in conjunction with the deflection unit AT1040.

# CONSTRUCTION

The magnetic circuit of the transformer comprises two C-cores. The transformer has three separate windings; the tertiary winding can be used for voltage feedback. The transformer has been provided with four holes for mounting on either a printed-wiring board or a metal chassis.

External circuit connection is made to connecting pins, positioned as indicated in Fig.1.



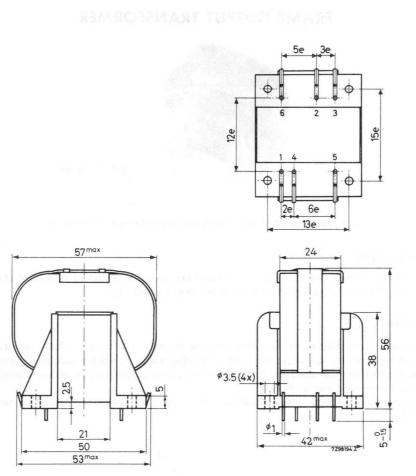
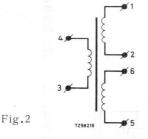


Fig.1. e = 2.52 mm, suitable for mounting on a grid with 2.54 mm (0.1") or 2.50 mm pitch.

August 1968

## 3122 107 31740

# ELECTRICAL DATA



Primary winding Connecting terminals Inductance

at a primary d.c. current of 55 mA at a primary d.c. current of 70 mA Resistance

Secondary winding Connecting terminals Resistance

Tertiary winding Connecting terminals Resistance

Transformation ratio  $\frac{Nprim}{N_{sec}}$ 

 $rac{Nprim}{N_{tert}}$ 

Maximum primary d.c. current Maximum primary peak voltage Maximum ambient temperature 6 H ± 10% 230  $\Omega$  ± 12% 3 and 4 9.7  $\Omega$  ± 12% 5 and 6 165  $\Omega$  ± 12% 5.6

 $7.5 H \pm 10\%$ 

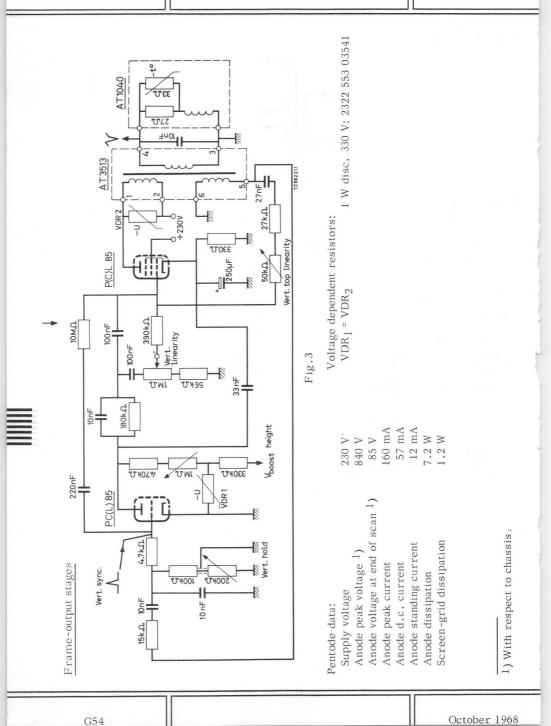
1 and 2

3.9

75 mA 1500 V 70 °C

# FRAME-OUTPUT TRANSFORMER

3122 107 31740

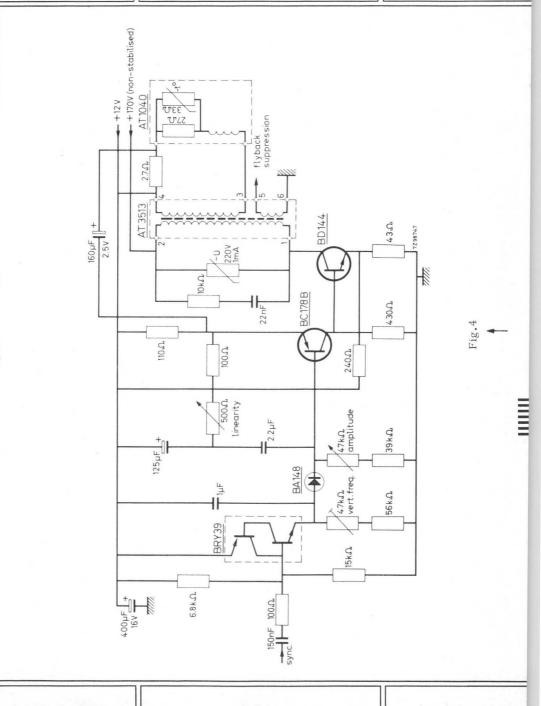


October 1968

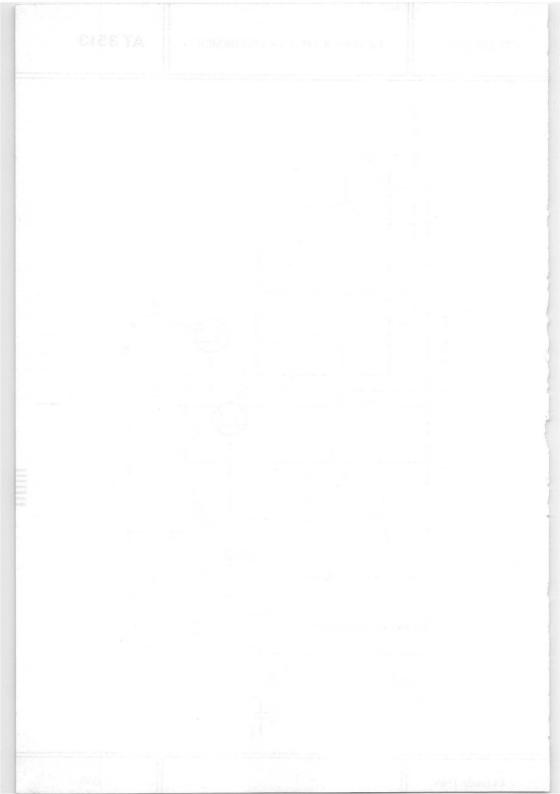
# 3122 107 31740

# FRAME -OUTPUT TRANSFORMER

AT 3513



October 1968



# ADJUSTABLE LINEARITY CONTROL UNIT



For tube-equipped television receivers

# APPLICATION

This unit has been designed for use in tube-equipped television receivers, to adjust the linearity of the line deflection. It can be used in combination with deflection unit AT 1030 and line-output transformer AT2025/01.

# CONSTRUCTION

This control unit consists of a coil wound on a ferroxcube rod, two ferroxdure magnets and one magnet of plastic bonded ferroxdure. The last mentioned magnet is placed around the ferroxcube rod, above the coil. One of the ferroxdure magnets has the shape of a half ring; it is placed around the ferroxcube rod under the coil. The other ferroxdure magnet is cylindrical; it is positioned parallel to and clamped against the ferroxcube rod opposite the first one. It is provided with a square hole to facilitate turning to adjust the biasing field and so the linearity of the line deflection. 

# AT 4034 / 01

# ADJUSTABLE LINEARITY CONTROL UNIT

# 3122 108 39180

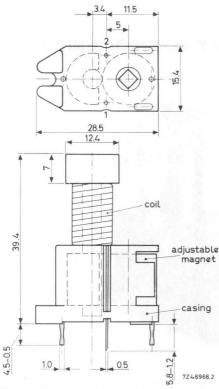


Fig. 1. Dimensions in mm

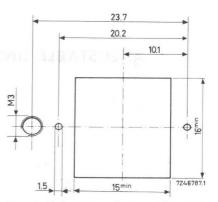
ELECTRICAL DATA

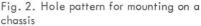
When a saw-tooth current (without S-correction) of 2.4  $A_{p-p}$ , frequency 15,625 Hz, flyback ratio 18%, flows through the linearity control unit (one connection point to earth), the correction voltage is adjustable between 12 V and 24 V.

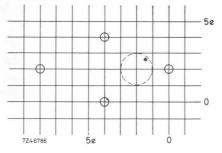
### MOUNTING

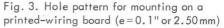
The unit can be mounted either on printed-wiring boards by means of its two connection pins and two mounting pins (see Fig. 3), or on metal chassis, by bending of the two mounting pins and/or by means of a screw through an aperture in the casing (see Fig. 2). To prevent distortion of the magnetic field no iron part should approach the magnetic parts anywhere nearer than 3 mm. The coil should be shunted with a 1 W carbon resistor of 1500  $\Omega$  to damp ringing phenomena.

\* Hole only necessary for bottom adjustment.









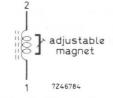


Fig. 4. Circuit diagram

3122 108 39180

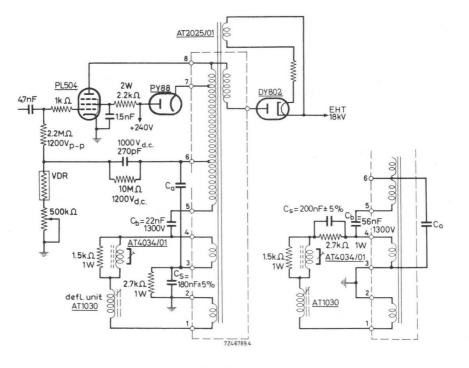
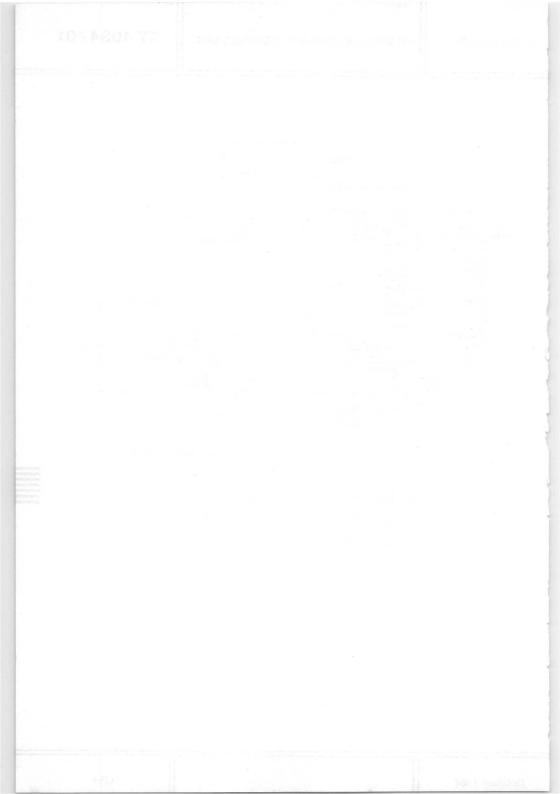


Fig. 5. Two versions of a line-output stage. C 0-270 pF, 2000 V<sub>p-p</sub>, amplitude adjustment C<sup>a</sup> booster capacitor C<sup>b</sup> S-corrector VDR = 2322 564 90014 (910 V)



# AT 4036 AT 4037

# ADJUSTABLE LINEARITY CONTROL UNITS





AT 4037

AT 4036

For tube-equipped (AT4037) and transistor-equipped (AT4036) television receivers

## APPLICATION

These linearity control units are designed to be used in television receivers, in combination with the 11 inch 90° picture tube A28-14W and the 12 inch 90° picture tube A31-20W.

The unit AT4036 is intended for use in transistor-equipped sets, in conjunction with the deflection unit AT1020/01 and the line-output transformer AT2042/01.

The unit AT4037 is intended for use in tube-equipped sets, in conjunction with the deflection unit AT1021/01 and the line-output transformer AT2043.

The difference between the two units lies only in the number of turns of the coils.

## CONSTRUCTION

The unit consists of a coil wound on a ferroxcube rod and two ferroxdure magnets. One of these magnets has the shape of a half ring and is placed around the ferroxcube rod under the coil. The other magnet is cylindrical; it is placed parallel to and clamped against the ferroxcube rod opposite the first one. This magnet is provided with a square hole to facilitate turning of it to adjust the biasing field and so the linearity of the line deflection.

October 1968

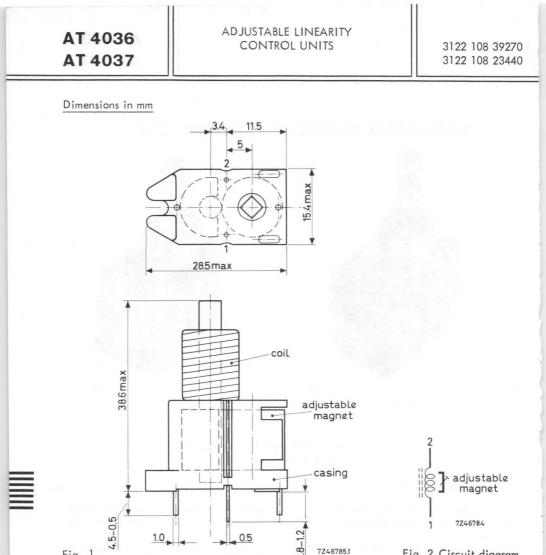




Fig. 2. Circuit diagram

ELECTRICAL DATA

# AT 4036

When a saw-tooth current (without S-correction) of  $6A_{p-p}$ , frequency 15,625 Hz, flyback ratio 18%, flows through the linearity control unit (one connection point to earth), the correction voltage is adjustable between 1.05V and 1.95V.

7Z46785.1

### AT 4037

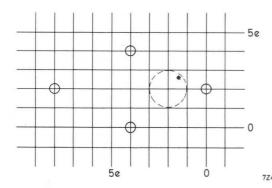
When a saw-tooth current (without S-correction) of 1.4Ap-p, frequency 15,625 Hz, flyback ratio 18%, flows through the linearity control unit (one connection point to earth), the correction voltage is adjustable between 5.3V and 9.5V.

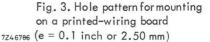
3122 108 39270 3122 108 23440 ADJUSTABLE LINEARITY CONTROL UNITS

AT 4036 AT 4037

# MOUNTING

The unit can be mounted either on printed-wiring boards by means of its two connection pins and two mounting pins (see Fig. 3), or on conventional panels by bending of the two mounting pins and/or by means of a screw through an aperture in the casing (see Fig. 4). To prevent distortion of the magnetic field no iron part should approach the magnetic parts anywhere nearer than 3mm. The coil should be shunted with a 1W carbon resistor to damp ringing phenomena.





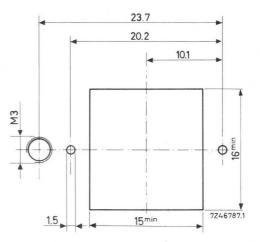


Fig. 4. Hole pattern for mounting on a chassis

\* Hole only necessary for bottom adjustment,

Proventik postano stanuted pristorian provensions alige (horizota) endante di siter no manisettiva straveni sovov ting pina bios filo () anto secono comi devent () atta tan na dela alta como en biosecendo () anto escale de la como de la com Recentente de la como d

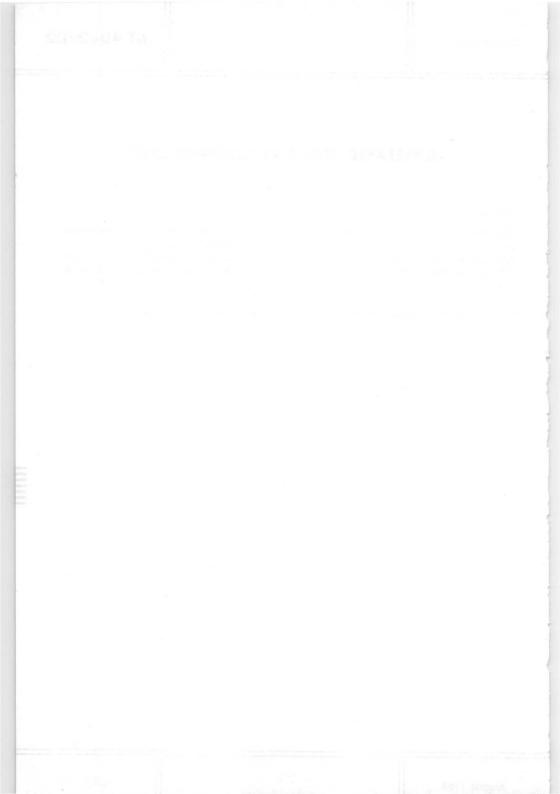
# ADJUSTABLE LINEARITY CONTROL UNIT

# APPLICATION

This unit is intended to be used in black and white, and in colour television sets equipped with tubes, to adjust the linearity of the line deflection.

In black and white television sets it can be used in conjunction with deflection unit AT1040 and line-output transformer AT2036, AT2036/25, AT2036/36, AT2034 or AT2045.

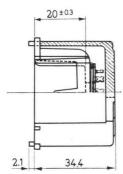
For further information see section "Components for colour television".

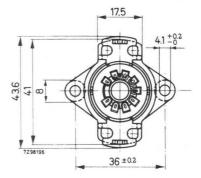


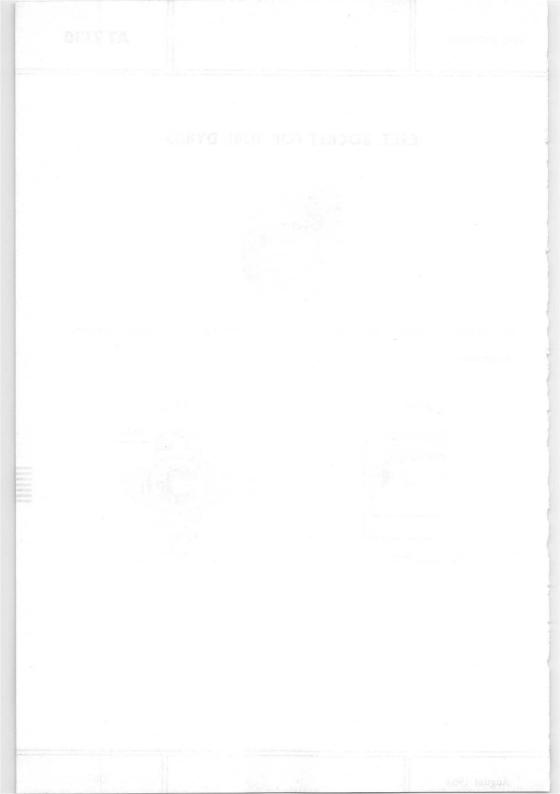
# E.H.T. SOCKET FOR TUBE DY802



The socket has been provided with a series resistor of 1.6  $\Omega$  in the heater circuit. Dimensions in mm

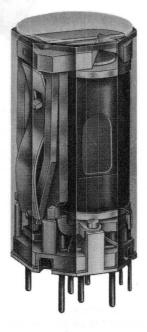






RELAYS





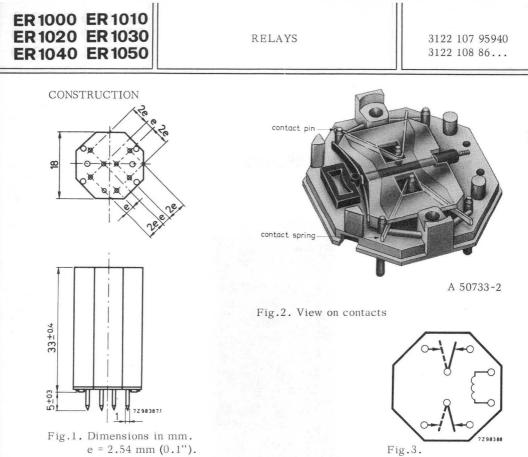
A 50733-1

# GENERAL

These relays find their application in a variety of electronic and electrical equipment, e.g. for system switching in universal television receivers.

They have been developed on the principle of only one spring acting on both the armature and the contacts. The switching action is positive owing to the minimum contact bounce; the contact capacitance is very low.

The sockets of the relays are provided with pins, which are arranged to fit printedwiring boards with a grid of 0.1".



# Rest position of relay

# Mounting

G70

The relays can be mounted in any position. The pin length is sufficient for board thicknesses up to 4 mm.

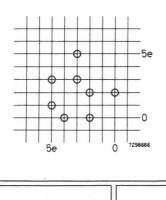


Fig.4. Hole pattern for mounting on a printed-wiring board (e = 0.1")

June 1968

3122	107	95940	
3122	108	86	

### RELAYS

10 g

20 g

no

tropic proof

minimum

400 °C during 5 s

# ER 1000 ER 1010 ER 1020 ER 1030 ER 1040 ER 1050

# TECHNICAL PERFORMANCE

General

Maximum permissible acceleration

Solderability

Weight

Operating (for d.c. voltage)

ER1000 **ER1010** ER1020 ER1030 ER1040 ER1050 24 Voltage <u>+15%</u> 55 36 12 3 Vdc · 6 Current +20%11 16.5 22 50 93 200 mA Power 600 600 530 600 mW nom. 600 560 Resistance at 20 °C nom. 5000 2200 1100 240 65 15 Ω Temperature rise of the coil 30 30 30 30 30 30 deg C nom. Temperature max. 100 100 100 100 100 100 OC Number of turns 15000 9600 7100 3300 1600 900

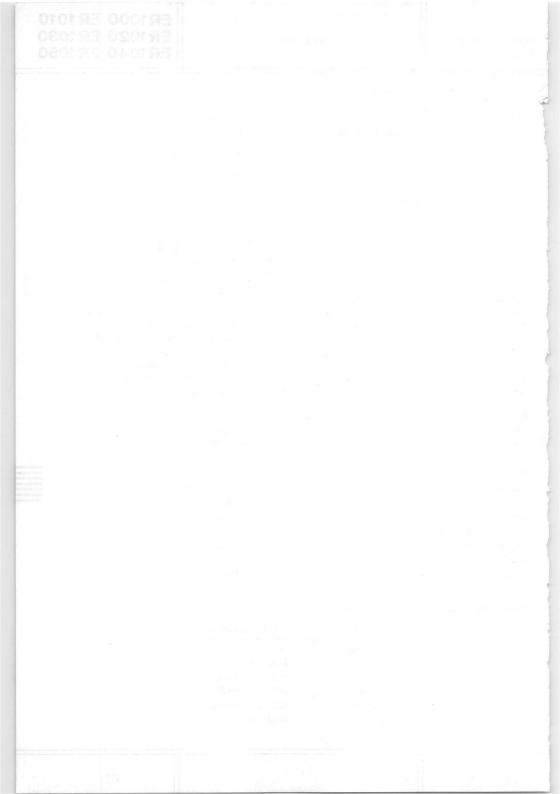
Security demands Climatic robustness Contact bounce

### Contact

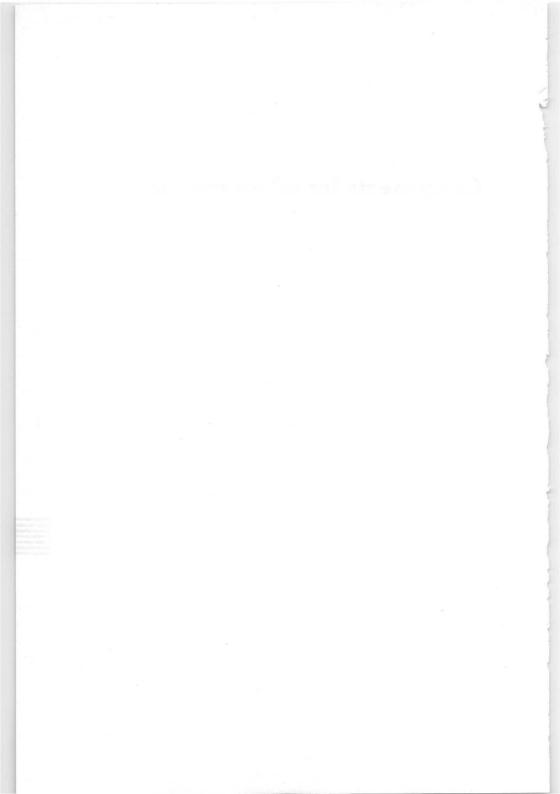
Minimum pressure	0.1 N/cm <sup>2</sup>
Voltage	300 V <sub>dc</sub>
Current	40 mA
Maximum resistance	100 mΩ
Minimum insulation resistance	40 MΩ
Maximum capacitance	2 pF
Number of operations	minimum $5 \ge 10^5$

## CATALOG NUMBERS (for ordering)

type number	catalog number
ER1000	3122 107 95940
ER1010	3122 108 86520
ER1020	3122 108 86510
ER1030	3122 108 86500
ER1040	3122 108 86490
ER1050	3122 108 86480



# Components for colour television



3122 107 30000 3122 107 30010

# AT 1022/04 AT 1022/06

NON-PREFERRED

**DEFLECTION UNITS** 



RZ 24284-8



RZ 24284-10

### APPLICATION

These deflection units have been designed for use with 22in and 25in 90° shadow mask colour picture tubes, in conjunction with line-output transformer AT2053/.. <sup>1</sup>) or line-deflection transformer AT2051/.. and E.H.T. transformer AT2052/.., and convergence unit AT1023/.., blue lateral unit AT1025/.. or AT1028.., linearity control unit AT4042/.. and transductor AT4041/...

<sup>1</sup>) future type

October 1968

3122 107 30000 3122 107 30010

#### MECHANICAL DATA

AT 1022/04

AT 1022/06

The saddle-shaped line and frame deflection coils as well as the yoke ring are mounted in a polypropylene ring. This set is built in a polypropylene coaxial housing provided with a guidance in which the set is movable in axial direction over 12 mm.

After the complete unit has been mounted on the colour tube the coils can be moved for purity adjustment and then secured by means of two winged nuts.

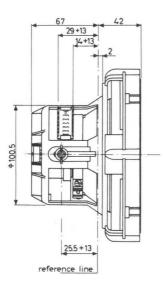
The moulding at the rear of the housing is extended so, that the convergence unit AT1023/.. can be easily mounted.

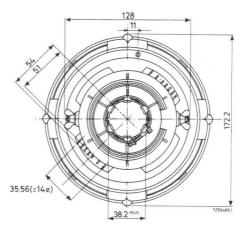
The unit is equipped with a built-in NTC thermistor which can be connected in series with the frame deflection coils in order to compensate for temperature dependence of the coils. By this, in frame-output circuits with voltage feedback for linearising the saw-tooth voltage a constant deflection current and so a constant picture height can be obtained up to temperatures of 95 °C.

The line deflection coils have been connected in parallel.

The provision of separate connecting points makes it possible to connect the frame deflection coils either in series or in parallel.

Dimensions in mm







AT 1022/04 AT 1022/06

#### Mounting

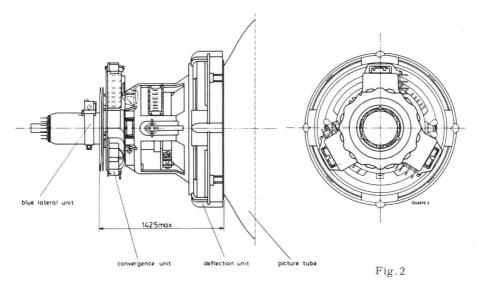
The housing should be mounted as far forward as possible on the neck of the picture tube, so that it touches the cone.

External circuit connection is made to soldering tags, positioned as indicated in Fig.3.

To orient the raster correctly, the housing may be rotated by hand on the neck of the picture tube, with which it makes a slip fit. A screw-tightened clamping ring, cooperative with rubber friction shoes, permits it to be locked radially in the desired position.

Subsequently the correct centre of deflection can be determined by moving the coil assembly in axial direction; it can be locked by means of the two winged nuts.

In Fig.2 an assembly consisting of deflection unit AT1022/.., convergence unit AT1023/.. and blue lateral unit AT1025/.. on a picture tube is given.



### ELECTRICAL DATA

Two versions are available, the AT1022/04 with a circuit (NTC thermistor of  $50 \Omega //$  resistor of 33  $\Omega$ ) compensating for temperature dependence in the case of series connected frame coils and the AT1022/06 with a circuit (NTC thermistor of  $6 \Omega //$  resistor of 12  $\Omega$ ) compensating for temperature dependence in the case of parallel connected frame coils.

AT 1022/04 AT 1022/06

### DEFLECTION UNITS

-					the second se
	Typical values		AT1022/	'04	AT1022/06
	Line deflection coils, parallel connected Inductance Resistance at 25 °C	1	2.95 mH 2.9 Ω	I	2.95 mH 2.9 Ω
	Deflection current at 25 kV, edge to edge scan in both directions Frame deflection coils, series connecte	d	2.6 Ap-	р	2.6 Ap-p
	Inductance Resistance at 25 °C Deflection current at 25 kV, edge to		114 mH 56 + 20*	*Ω	114 mH 56 Ω
	edge scan in both directions Frame deflection coils, parallel connect	ted	0.415 A	р-р	0.415 A <sub>p-p</sub>
	Inductance Resistance at 25 °C Deflection current at 25 kV, edge to		28 mH 14 Ω		28 mH 14 + 4**Ω
	edge scan in both directions Maximum working temperature		0.830 A 95 °C	р-р	0.830 A <sub>p-p</sub> 95 °C
	Connections (see Fig.3)	connecting	tags	0	ich have to be rconnected
	Line deflection coils (H) parallel connected	1 or 2 and 1' or 2'		1 and 2 1' and 1	
	parallel connected with balancing coil (e.g. AT4040/57)	l or 2 and c tap of balanc coil			(balancing tween 1' and
		1' or 2' and tap of balanc coil			2' (balancing tween 1 and
	Frame deflection coils (V), without NTC thermistor			,	
	series connected	3 and 3'		4 and 5 4' and 5 6 and 6	5'
	parallel connected	3 and 3'		3 and 4 5 and 6 3' and 6 5' and 6 6 and 6	4' 6'

\* NTC thermistor in parallel with a resistor of 33  $\Omega.$ 

\*\* NTC thermistor in parallel with a resistor of 12  $\Omega.$ 

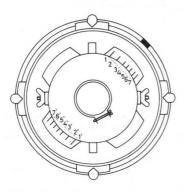
### 3122 107 30000 3122 107 30010

### DEFLECTION UNITS

# AT 1022/04 AT 1022/06

3' and 4' 5' and 6' 6' and 7'

Frame deflection coils (V), with NTC thermistor	connecting tags	tags which have to be interconnected
AT1022/04		
series connected coils	3 and 3'	4 and 5 6 and 7 4' and 5' 6' and 7'
AT1022/06		
parallel connected coils	3 and 3'	3 and 4
		5 and 6
		6 and 7



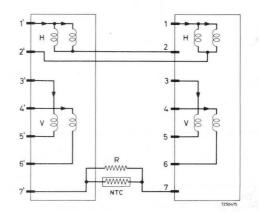


Fig.3

AT 1022/04	DEF LECTION UNITS	3122 107 30000
AT 1022/06		3122 107 30010

#### Misconvergence (dynamic convergence tolerances)

11

Misconvergence is defined as the distance between the centres of the red, blue and green beams on the screen using rectangular coordinates (see Fig.4). The centre is defined as the centre of the brightest portion of the beam.

The misconvergences listed in the table below, are given for a nominal  $25in 90^{\circ}$  colour picture tube equipped with a deflection unit AT1022/..., a convergence unit AT1023/... and a blue lateral unit AT1025/... or AT1028/..., at 25 kV. The values in the table are only valid provided that these units have been adjusted to optimum convergence on the lines BC and DE (See Fig. 5).

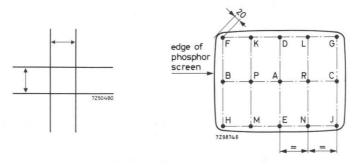


Fig.4

Fig.5 (Dimensions in mm)

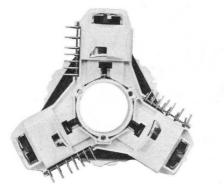
11

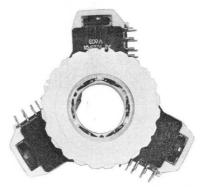
	~	misconvergence (in mm)			
location	colour	typical horizontal vertical		maximum horizontal vertical	
А	R to G to B to R	0	0	0	0
В, С	R to G B to R/G	0 < 0.5	0 < 0.5	0 1	0 1
D, E	R to G B to R/G	0 < 0.5	0 0	0 1	0 0
K, L, P, R, M, N	R to G to B to R	< 0.5	< 0.5	1	1
F, G, H, J	R to B to G to R	< 1.5	< 1.5	2	2



NON-PREFERRED

### **CONVERGENCE UNIT**





RZ 22858-5

RZ 22858-6

### APPLICATION

This unit is intended to be used with a 90° shadow mask colour picture tube, in conjunction with the deflection unit AT1022/.. and the blue lateral unit AT1025/.. or AT1028/.., to converge the three colour pictures statically and dynamically and to adjust the purity.

### AT 1023/..

#### CONVERGENCE UNIT

### MECHANICAL DATA

Dimensions in mm

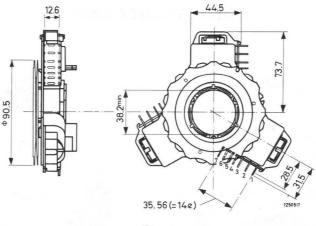


Fig. 1

#### Mounting

The convergence unit can easily be mounted on the deflection unit. To this end the three hooks of the convergence unit have to be placed in the circular slot at the rear of the deflection unit. Consequently the convergence unit must be turned to the right as fas as possible; then it is locked in axial direction by means of two retaining pins and a screw. When this screw is fastened, the convergence unit is also locked in radial direction.

The cover plate of the convergence unit is provided with three holes to facilitate fixing of cables.

AT 1023/...

In Fig.2 an assembly consisting of deflection unit, convergence unit and blue lateral unit on a picture tube is given.

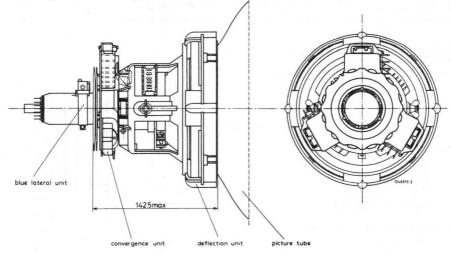


Fig.2

### ELECTRICAL DATA

Every convergence unit AT1023/.. consists of three identical parts, one for each colour; so the electrical data given for one part suit all three.

Dynamic convergence takes place by feeding the line and frame coils with parabolic and sawtooth currents respectively.

AT1023/01, catalog number 3122 107 30530

Line deflection coils, series connected		3 7 5 4
Inductance	0.42 mH	ΙΙ Ι.Ι
Resistance	$4 \Omega$	
Connecting tags	5 and 7	36 36
Frame deflection coils, series connected		
Inductance	1.44 H	
Resistance	170 Ω	2 7250477
Connecting tags	3 and 4	Fig.3

AT 1023/...

CONVERGENCE UNIT

### AT1023/02, catalog number 3122 107 30330

Electrically the same as AT1023/01, however without permanent magnets. Static convergence by means of a d.c. current through the frame coils.

### AT1023/05, catalog number 3122 107 30560

Line deflection coils, series connected Inductance Resistance Connecting tags Tags which have to be interconnected Line deflection coils, parallel connected Inductance Resistance Connecting tags Tags which have to be interconnected Frame deflection coils, parallel connected Inductance	0.42 mH 4 $\Omega$ 4 and 7 5 and 6 0.1 mH 1 $\Omega$ 4 and 6 4 and 5 6 and 7 0.36 H	1 7 4 1 00000000000000000000000000000000000
Resistance	42.5 Ω	0
Connecting tags	2 and 3	
AT1023/10, catalog number 3122 107 30540 Line deflection coils, series connected Inductance Resistance Connecting tags	4.7 mH 46 Ω 5 and 7	
Frame deflection coils, series connected Inductance Resistance Connecting tags Tags which have to be interconnected	1.44 H 170 Ω 1 and 4 2 and 3	
Frame deflection coils, parallel connected		7250478
Inductance	0.36 H	3 2

42.5 Ω

1 and 3

1 and 2 3 and 4 Fig.5

Resistance

Connecting tags

Tags which have to be interconnected

### AT 1023 / . .

### AT1023/12, catalog number 3122 107 30430

Line deflection coils, parallel connected Inductance Resistance Connecting tags	1.2 mH 11.5 Ω 6 and 7	
Frame deflection coils, series connected Inductance Resistance Connecting tags Tags which have to be interconnected	1.44 H 170 Ω 1 and 4 2 and 3	
Frame deflection coils, parallel connected Inductance Resistance Connecting tags Tags which have to be interconnected	0.36 H 42.5 Ω 1 and 3 1 and 2 3 and 4	Fig.6

### AT1023/13, catalog number 3122 107 31480

Electrically the same as AT1023/10, however without permanent magnets. Static convergence by means of a d.c. current through the frame coils.

### Purity adjustment

The purity can be adjusted by means of two independently movable magnets. These magnets are diametrically magnetised; when the notches of the magnets coincide the magnetic fields are in opposite phase. By turning the magnets with respect to each other the magnetic force of the resultant field of both magnets is adjusted. The direction of the resultant magnetic field is adjusted by turning the magnets simultaneously. The area of purity adjustment which can be obtained on the screen of the picture tube is given in Fig.7.

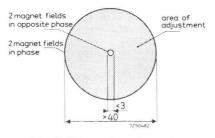
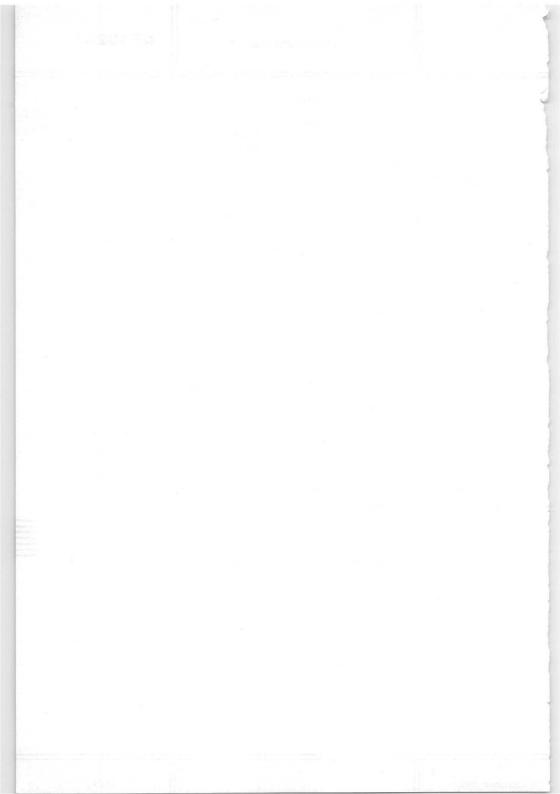
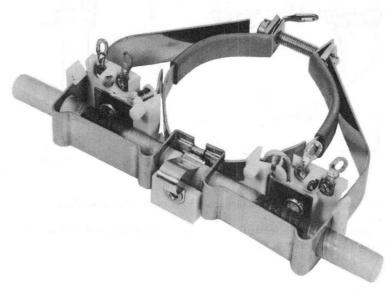


Fig.7 (Dimensions in mm)



### AT 1025/05

### **BLUE LATERAL UNIT**



RZ 22858-4

For series or parallel connection

### APPLICATION

This unit is intended for use with a 90° shadow mask colour picture tube in conjunction with a deflection unit AT 1027/.. and convergence units AT 4045/.. or AT 4046/.. for static and dynamic lateral adjustment, or in conjunction with a deflection unit AT 1022/.. and a convergence unit AT 1023/.. respectively.

### MECHANICAL DATA

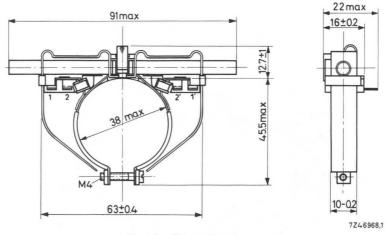


Fig. 1. Dimensions in mm

The unit must be positioned on the colour picture tube as close as possible to the convergence unit.

An assembly consisting of a deflection unit, a convergence unit and a blue lateral unit on a picture tube is given in Fig. 2.

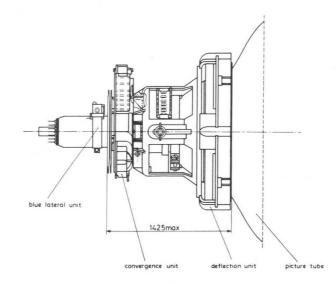


Fig. 2

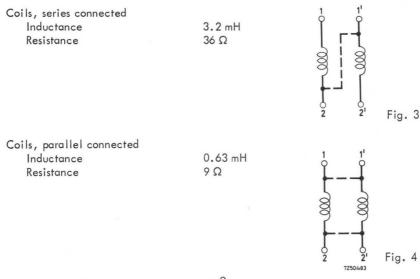
October 1968

3122 107 30020

BLUE LATERAL UNIT

AT 1025/05

### ELECTRICAL DATA



Maximum working temperature

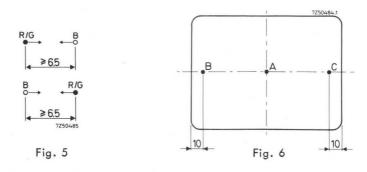
95 °C

#### Static lateral adjustment

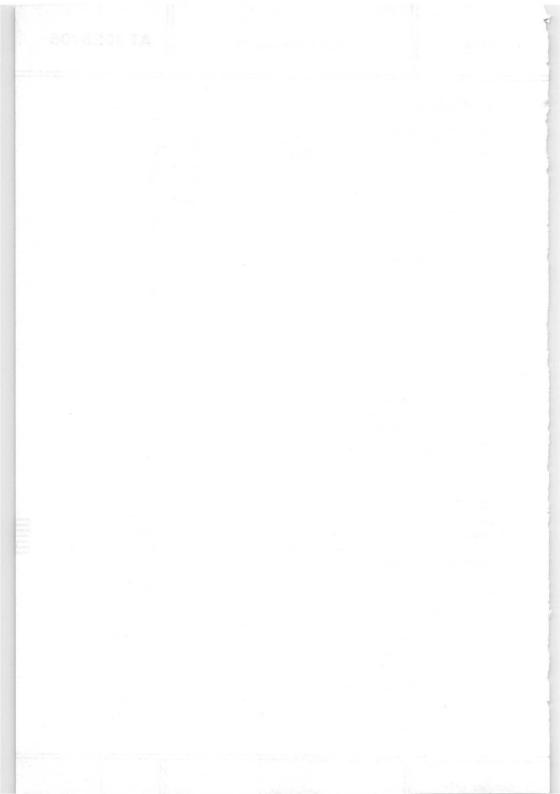
Static lateral adjustment in the centre can be obtained by turning the magnet holder. A turn of 360<sup>°</sup> gives a minimum adjustment range of 6.5 mm; red/green and blue are in opposite phase (see Fig. 5).<sup>-</sup>

### Dynamic lateral adjustment

A horizontal shift in the points B and C between red/green and blue of  $\geq$  3.5 mm can be obtained with a saw tooth current of 350 mA<sub>p-p</sub>, frequency 15 kHz, through the coils when they are series connected, a saw tooth current of 700 mA<sub>p-p</sub> when they are parallel connected (see Fig. 6).

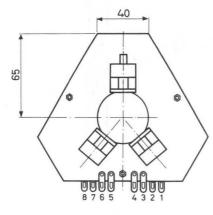


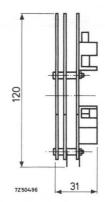
October 1968



### AT 1026

PURITY AND BLUE LATERAL UNIT





Dimensions in mm

### APPLICATION

This unit has been designed for <u>electrical</u> purity and blue lateral adjustment in monitors, etc.. It must be used in combination with the convergence unit AT 1023/...

### MOUNTING

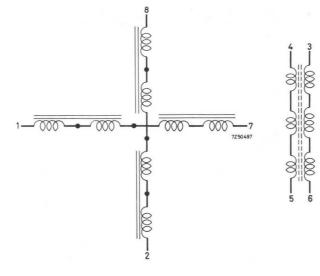
After removing the purity rings, convergence magnets and the cover of the AT 1023/.., this unit can be fixed onto the AT 1023/... by means of a snap-lock construction. The combination must be positioned on the deflection unit in such a way that the connections of the AT 1026 are opposite the blue gun.

AT 1026

### PURITY AND BLUE LATERAL UNIT

3122 108 62870

### ELECTRICAL DATA



Purity coils

Blue lateral coils

Horizontal shift 1 - 7 (R = 60  $\Omega$ ) Vertical shift 2 - 8 (R = 60  $\Omega$ ) Note: Static convergence can be achieved by means of a direct current through the frame coils of the AT 1023/...

NON-PREFERRED

### **DEFLECTION UNIT**



RZ 26059-4



RZ 26059-5

With built-in NTC thermistor of 50  $\Omega$  in parallel with a resistor of 33  $\Omega$ 

### APPLICATION

This deflection unit has been designed for use with 22in and 25in 90° shadow mask colour picture tubes, in conjunction with line-output transformer AT2053/.. 1) or line-deflection transformer AT2051/.. and E.H.T. transformer AT2052/.., and convergence units AT4045/.. or AT4046/.., blue lateral unit AT1025/.. or AT1028/.., linearity control unit AT4042/.. and transductor AT4041/...

1) future type

October 1968

#### DEFLECTION UNIT

3122 107 31510

### MECHANICAL DATA

The saddle-shaped line and frame deflection coils as well as the yoke ring are mounted in a polypropylene ring. This set is built in a polypropylene coaxial housing provided with a guidance in which the set is movable in axial direction over 20 mm. After the complete unit has been mounted on the colour tube the coils can be moved for purity adjustment and then secured by means of four winged nuts.

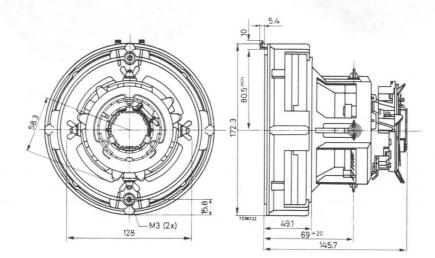
The housing also includes a construction in which the convergence units AT4045/.. or AT4046/.. easily fit.

The unit is equipped with a built-in NTC thermistor which can be connected in series with the frame deflection coils in order to compensate for temperature dependence of the coils. By this, in frame-output circuits with voltage feedback for linearising the saw-tooth voltage a constant deflection current and so a constant picture height can be obtained up to temperatures of 95  $^{\circ}$ C.

The line deflection coils have been connected in parallel.

The provision of separate connecting points makes it possible to connect the frame deflection coils either in series or in parallel.

### Dimensions in mm





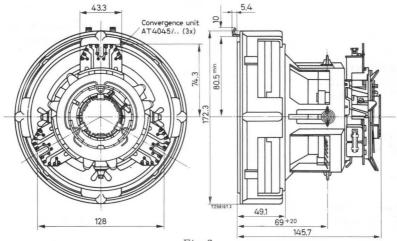
### Mounting

The housing should be mounted as far forward as possible on the neck of the picture tube, so that it touches the cone.

External circuit connection is made to soldering tags, positioned as indicated in Fig.3.

To orient the raster correctly, the housing may be rotated by hand on the neck of the picture tube, with which it makes a slip fit. A screw-tightened clamping ring, cooperative with rubber friction shoes, permits it to be locked radially in the desired position.

Subsequently the correct centre of deflection can be determined by moving the coil assembly in axial direction; it can be locked by means of the four winged nuts. In Fig.2 an assembly consisting of deflection unit AT1027/04 and three convergence units AT4045/... is given.





### ELECTRICAL DATA (typical values)

Line deflection coils, parallel connected	
Inductance	2.95 mH
Resistance at 25 °C	2.9 Ω
Deflection current at 25 kV, edge to	
edge scan in both directions	2.6 Ap-p
Frame deflection coils, series connected	
Inductance	114 mH
Resistance at 25 °C	$56 + 20^* \Omega$
Deflection current at 25 kV, edge to	
edge scan in both directions	0.415 Ap-p

\* NTC thermistor in parallel with a resistor of 33  $\Omega$ .

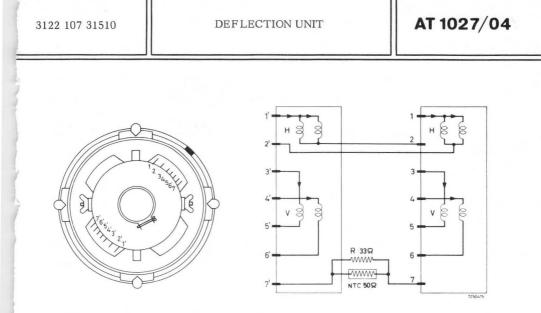
October 1968

### DEFLECTION UNIT

3122 107 31510

Frame deflection coils, parallel connec Inductance Resistance at 25 °C	ted 28 mH 14 Ω	
Deflection current at 25 kV, edge to		
edge scan in both directions	0.830 A	Ар-р
Maximum working temperature	95 °C	
<u>Connections</u> (see Fig.3)	connecting tags	tags which have to be interconnected
Line deflection coils,		
parallel connected	1 or 2 and 1' or 2'	1 and 2 1' and 2'
parallel connected with balancing		
coil (e.g. AT4040/57)	l or 2 and centre tap of balancing coil	l and 2 (balancing coil between 1' and 2')
	l' or 2' and centre tap of balancing coil	l' and 2' (balancing coil between 1 and 2)
Frame deflection coils,		
series connected, without		
NTC thermistor	3 and 3'	4 and 5
		4' and 5'
		6 and 6'
series connected, with *)		o unu o
NTC thermistor	3 and 3'	4 and 5
NTO thermistor	o and o	6 and 7
		4' and 5'
		6' and 7'
parallel connected, without		o and /
NTC thermistor	3 and 3'	3 and 4
NIC mermistor	5 and 5	5 and 6
		3' and 4'
		5' and 6'
		6 and 6'

\*) NTC-thermistor value is such that right compensation for temperature dependence is obtained with series connected frame coils.





#### Misconvergence (dynamic convergence tolerances)

Misconvergence is defined as the distance between the centres of the red, blue and green beams on the screen using rectangular coordinates (see Fig.4). The centre is defined as the centre of the brightest portion of the beam.

The misconvergences listed in the table below, are given for a nominal 25in  $90^{\circ}$  colour picture tube equipped with a deflection unit AT1027/04, convergence units AT4045/.. or AT4046/.. and a blue lateral unit AT1025/.. or AT1028/.., at 25 kV. The values in the table are only valid provided that these units have been adjusted to optimum convergence on the lines BC and DE (see Fig. 5).

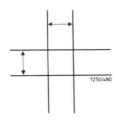


Fig.4

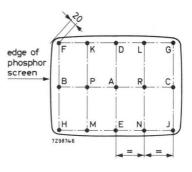


Fig.5 Dimensions in mm

3122 107 31510

		misconvergence (in mm)			
location	colour	typical horizontal vertical		maximum horizontal vertical	
А	R to G to B to R	0	0	0	0
B, C	R to G B to R/G	0 < 0.5	0 < 0.5	0 1	0 1
D, E	R to G B to R/G	0 < 0.5	0 0	0 1	0 0
K, L, P, R, M, N	R to G to B to R	< 0.5	< 0.5	1	1
F, G, H, J	R to B to G to R	< 1.5	< 1.5	2	2

### Purity adjustment

The purity can be adjusted by means of two independently movable magnets. These magnets are diametrically magnetised; when the notches of the magnets coincide the magnetic fields are in opposite phase. By turning the magnets with respect to each other the magnetic force of the resultant field of both magnets is adjusted. The direction of the resultant magnetic field is adjusted by turning the magnets simultaneously. The area of purity adjustment which can be obtained on the screen of the picture tube is given in Fig.7.

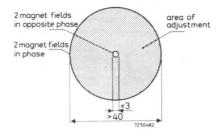


Fig.7

### **DEFLECTION UNIT**



RZ 26059-4



RZ 26059-5

With built-in NTC thermistor of 6  $\Omega$  in parallel with a resistor of 12  $\Omega$ 

### APPLICATION

This deflection unit has been designed for use with 22in and 25in 90° shadow mask colour picture tubes, in conjunction with line-output transformer AT2053/.. <sup>1</sup>) or line-deflection transformer AT2051/.. and E.H.T. transformer AT2052/.., and convergence units AT4045/.. or AT4046/.., blue lateral unit AT1025/.. or AT1028/.., linearity control unit AT4042/.. and transductor AT4041/...

1) future type

October 1968

### MECHANICAL DATA

The saddle-shaped line and frame deflection coils as well as the yoke ring are mounted in a polypropylene ring. This set is built in a polypropylene coaxial housing provided with a guidance in which the set is movable in axial direction over 20 mm. After the complete unit has been mounted on the colour tube the coils can be moved for purity adjustment and then secured by means of four winged nuts.

The housing also includes a construction in which the convergence units AT4045/.. or AT4046/.. easily fit.

The unit is equipped with a built-in NTC thermistor which can be connected in series with the frame deflection coils in order to compensate for temperature dependence of the coils. By this, in frame-output circuits with voltage feedback for linearising the saw-tooth voltage a constant deflection current and so a constant picture height can be obtained up to temperatures of 95  $^{\circ}$ C.

The line deflection coils have been connected in parallel.

The provision of separate connecting points makes it possible to connect the frame deflection coils either in series or in parallel.

### Dimensions in mm

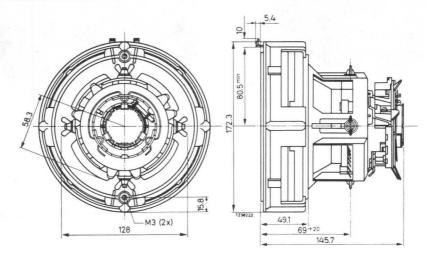


Fig.1

### Mounting

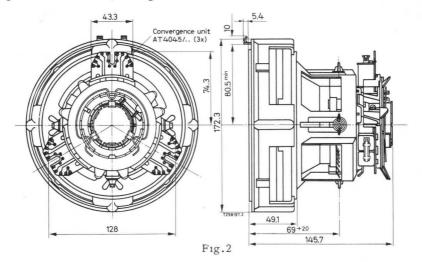
The housing should be mounted as far forward as possible on the neck of the picture tube, so that it touches the cone.

External circuit connection is made to soldering tags, positioned as indicated in Fig.3.

To orient the raster correctly, the housing may be rotated by hand on the neck of the picture tube, with which it makes a slip fit. A screw-tightened clamping ring, cooperative with rubber friction shoes, permits it to be locked radially in the desired position.

Subsequently the correct centre of deflection can be determined by moving the coil assembly in axial direction; it can be locked by means of the four winged nuts.

In Fig.2 an assembly consisting of deflection unit AT1027/06 and three conververgence units AT4045/... is given.



### ELECTRICAL DATA (typical values)

Line deflection coils, parallel connected	
Inductance	2.95 mH
Resistance at 25 °C	2.9 Ω
Deflection current at 25 kV, edge to	
edge scan in both directions	2.6 Ap-p
Frame deflection coils, series connected	
Inductance	114 mH
Resistance at 25 °C	56 Ω
Deflection current at 25 kV, edge to	
edge scan in both directions	0.415 Ap-p

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### DEFLECTION UNIT

3122 107 31580

Inductance Resistance at 25 °C	28 ml 14 +	
Deflection current at 25 kV, even edge scan in both directions	0	) A <sub>p-p</sub>
Maximum working temperature	95 °C	
Connections (see Fig. 3)		n. Laserte a ser se se se
	connecting tags	tags which have to be interconnected
Line deflection coils,	-	-
parallel connected	l or 2 and 1' or 2'	1 and 2 1' and 2'
parallel connected with balance	ing	
coil (e.g. AT4040/57)	l or 2 and centre tap of balancing coil	l and 2 (balancing coil between l' and 2')
	l'or 2' and centre tap of balancing coil	l'and 2'(balancing coil between 1 and 2)
Frame deflection coils,		
series connected, without NTC thermistor	3 and 3'	4 and 5 4' and 5' 6 and 6'
parallel connected, without		
NTC thermistor	3 and 3'	3 and 4 5 and 6 3' and 4' 5' and 6' 6 and 6'
parallel connected, with		
NTC thermistor **)	3 and 3'	3 and 4 5 and 6 6 and 7 3' and 4' 5' and 6' 6' and 7'

\* ) NTC thermistor in parallel with a resistor of 12  $\Omega.$ 

\*\* ) NTC thermistor value is such that right compensation for temperature dependence is obtained with parallel connected frame coils.



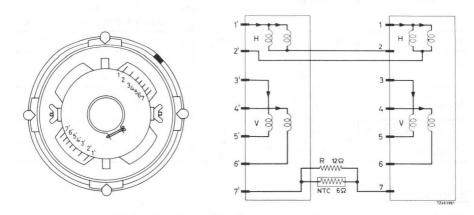
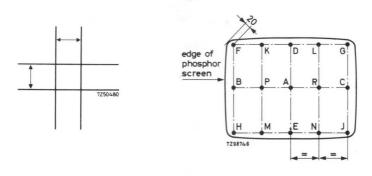


Fig.3

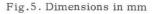
### Misconvergence (dynamic convergence tolerances)

Misconvergence is defined as the distance between the centres of the red, blue and green beams on the screen using rectangular coordinates (see Fig.4). The centre is defined as the centre of the brightest portion of the beam.

The misconvergences listed in the table below, are given for a nominal 25in 90° colour picture tube equipped with a deflection unit AT1027/06, convergence units AT4045/.. or AT4046/.. and a blue lateral unit AT1025/.. or AT1028/.., at 25 kV. The values in the table are only valid provided that these units have been adjusted to optimum convergence on the lines BC and DE (see Fig. 5).







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	colour	misconvergence (in mm)			
location		typic horizontal		maxir horizontal	
А	R to G to B to R	0	0	0	0
B, C	R to G B to R/G	0 < 0.5	0 < 0.5	0 1	0 1
D, E	R to G B to R/G	0 < 0.5	0 0	0 1	0 0
K, L, P, R, M, N	R to G to B to R	< 0.5	< 0.5	1	1
F, G, H, J	R to B to G to R	< 1.5	< 1.5	2	2

#### Purity adjustment

The purity can be adjusted by means of two independently movable magnets. These magnets are diametrically magnetised; when the notches of the magnets coincide the magnetic fields are in opposite phase. By turning the magnets with respect to each other the magnetic force of the resultant field of both magnets is adjusted. The direction of the resultant magnetic field is adjusted by turning the magnets simultaneously. The area of purity adjustment which can be obtained on the screen of the tube is given in Fig.7.

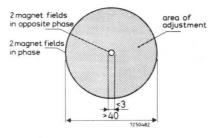


Fig.7

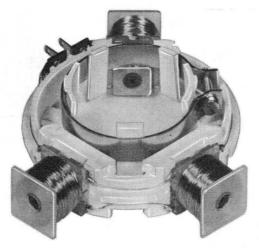
October 1968

3122 107 31460 3122 108 83000

# AT 1028/00 AT 1028/01

NON-PREFERRED

### **BLUE LATERAL UNIT**



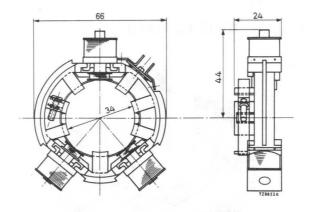
### APPLICATION

RZ 24284-15

This blue lateral unit is intended for use with a  $90^{\circ}$  shadow mask colour picture tube in conjuction with a deflection unit AT1022/.. and a convergence unit AT1023/.., or deflection unit AT1027/.. with convergence units AT4045/.. or AT4046/.. for electrical static and dynamic lateral adjustment.

A T 1000 (00	
AT 1028 / 00 BLUE LATERAL UNIT	3122 107 31460
	3122 108 83000

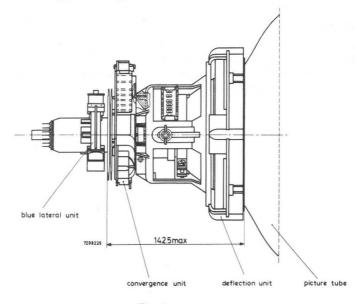
### MECHANICAL DATA





The unit must be positioned on the colour picture tube as close as possible to the convergence unit.

An assembly consisting of a deflection unit, a convergence unit and a blue lateral unit on a picture tube is given in Fig.2.





### ELECTRICAL DATA

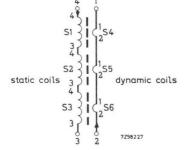
There are two versions of blue lateral unit: AT1028/00 and AT1028/01, which are different as regards the coils for static lateral adjustment. The electrical values of these coils are adapted to either a low d.c. voltage or a higher one.

Static lateral adjustment	AT1028/00	AT1028/01
Terminals	3 and 4	3 and 4
Resistance	175 Ω	18 Ω
D.C. current for minimum shift of 6.5 mm in centre *)	35 mA	110 mA

### Dynamic lateral adjustment

In points B and C a horizontal shift between red/green and blue of  $\geq 3.5$  mm can be obtained with a saw tooth current of 500 mAp-p, frequency 15 kHz. (See Fig. 4)

Terminals	1 and 2	
Resistance	5.8 Ω	▲ ≥ 6.5
Inductance	0.6 mH	B R/G ○→ ←●
		Fig.3 <sup>≥6.5</sup>



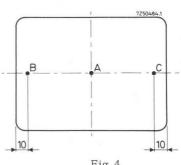
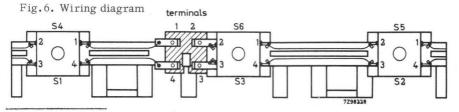


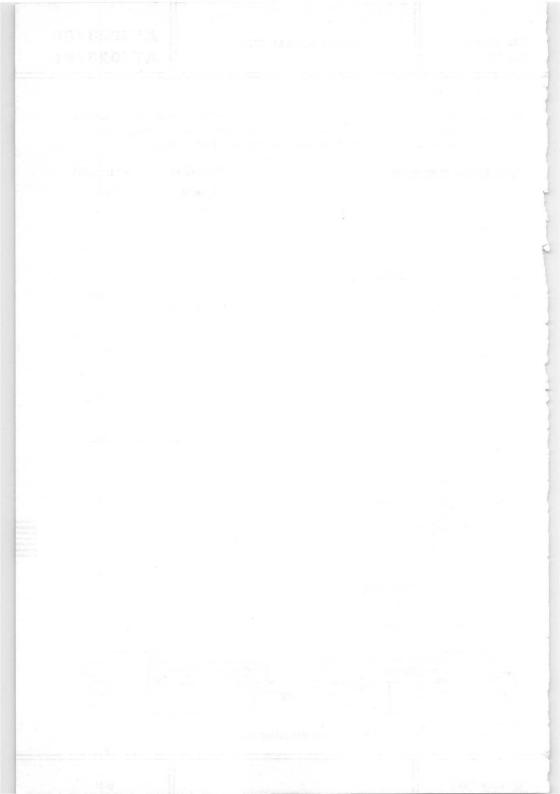
Fig.5. Circuit diagram

Fig.4



\*) red/green and blue move in opposite direction (see Fig.3)

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3122 108 87890 3122 108 87900

# AT 1029/04 AT 1029/06

## **DEFLECTION UNITS**



RZ 26059-4



RZ 26059-5

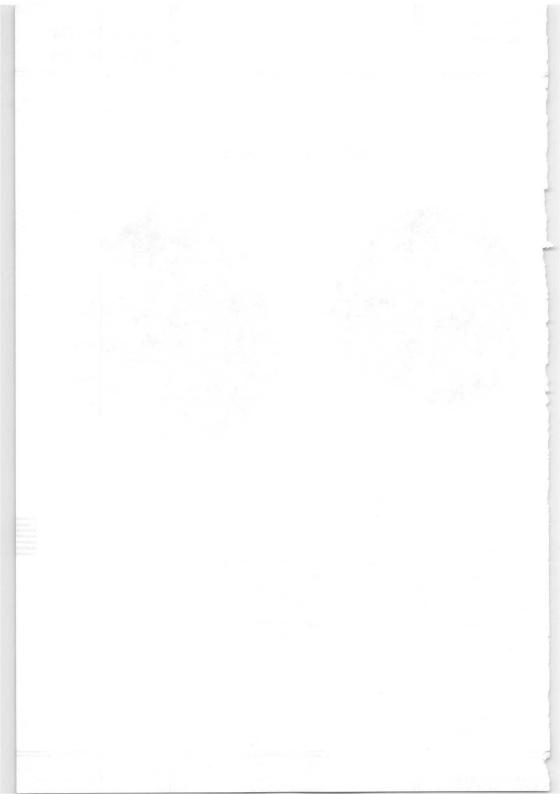
With built-in NTC thermistor of 6  $\Omega$  in parallel with a resistor of 12  $\Omega$ 

#### **APPLICATION**

This deflection unit has been designed for use with a 19in 90° shadow mask colour picture tube, in conjunction with line-output transformer AT2053/.. 1) or line-deflection transformer AT2051/.. and E.H.T. transformer AT2052/.., and convergence units AT4045/.. or AT4046/.., blue lateral unit AT1025/.. or AT1028/... linearity control unit AT4042/.. and transductor AT4041/...

For further information see AT1027/04 and AT1027/06 respectively. Misconvergence of the AT1029/.. is given for a nominal 19in 90° colour picture tube.

1) future type



### 3122 107 31270

## AT 2050 / 03

### LINE-OUTPUT TRANSFORMER



RZ 24284-3

### APPLICATION

This transformer has been developed for use in colour television receivers presenting 625 and 819 lines at 50 frames per second. It is intended for use in conjunction with deflection unit AT 1022/.. or AT 1027/.. , convergence unit AT 1023/.., AT 4045/.. or AT 4046/.. and linearity control unit AT 4042/02.

### MECHANICAL DATA

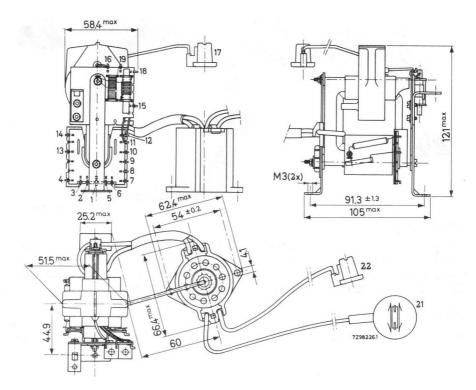
The primary coil is dipped, the  $\ensuremath{\mathsf{EHT}}$  coil is encapsulated in a flame retarding polyester.

AT 2050 / 03

### LINE-OUTPUT TRANSFORMER

### 3122 107 31270

Dimensions in mm



E

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#### Mounting instructions

#### 1. Temperature

- a. The operating temperature of the transformer coils and the core should not exceed 95  $^{\rm O}C$  under worst circumstances, i.e. taking into account:
  - overvoltage
  - low atmospheric pressure (at high altitudes) implying bad cooling by convection
  - high room temperature (up to  $45 \, {}^{\circ}C$ ).
- b. Direct heat radiation from the PL509 and PY500 to the transformer and the heater cable of the GY501 should be avoided by a screen. (If this screen is made from insulating material, it should be placed at least 20 mm from the coils.)
- c. The socket of the GY501 should not be exposed to any direct heat radiation from the PL509 and the PY500.
- d. Ample cool air circulation should be provided around the transformer.

### 2. Distances

It is important in the design of a line output and E.H.T. stage to maintain certain minimum distances between the transformer and the surrounding components and shields.

- a. The radial distance between the E.H.T. coils and any flat metal part (free from sharp edges) should be at least 30 mm. The axial distance from the E.H.T. coil should be at least 20 mm.
- b. The distance from the E.H.T. cap and lead should be at least 45 mm.
- c. The distance between the primary coil and any flat and smooth metal part should be at least 10 mm.
- d. The distance between the upper edge of the GY501 socket and the primary coil should be at least 15 mm.
- e. The distances between the caps of PL509 and PY500 and any flat and smooth metal part should be at least 15 mm.
- f. The transformer and the leads and components carrying high tension pulses should be kept free from metal particles, solder drops etc.

3. The metal bracket must be connected to the chassis.

AT 2050 / 03

3122 107 31270

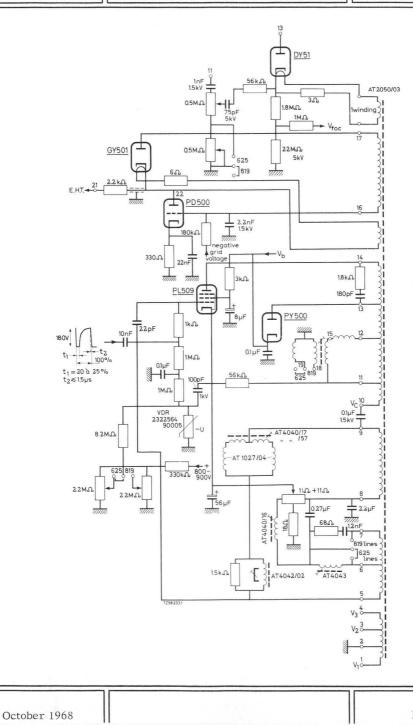
### ELECTRICAL DATA (see circuit diagram)

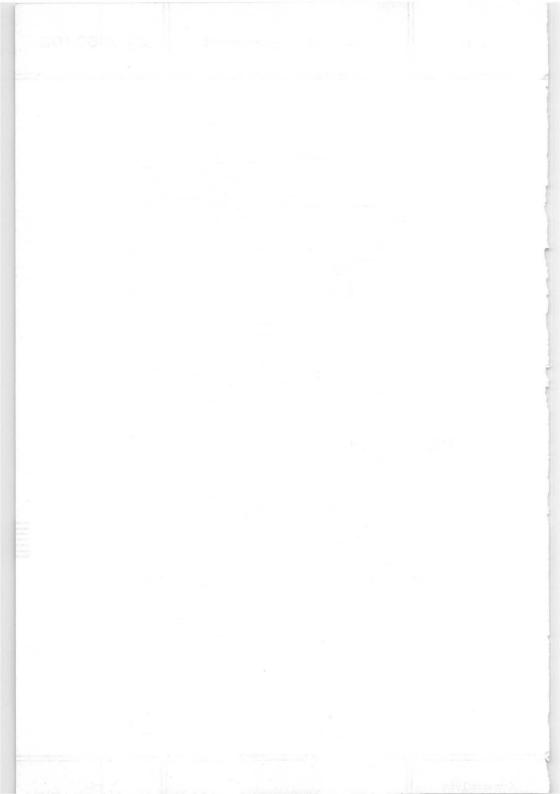
	625 lines	819 lines
V <sub>b</sub>	315 V	315 V
V boost	590 V	590 V
E.H.T.	24.7 kV	24.1 kV
I load	312 mA	330 mA
Overscan	+ 9%	+ 9%
Stabilisation	V <sub>b</sub> - 15%	V <sub>b</sub> - 12%
V <sub>1</sub> p-p	- 135 V	- 125 V
V <sub>2</sub> p-p	+ 135 V	+125 V
V <sub>3</sub> p-p	+ 310 V	+ 280 V
PL 509		
V <sub>bg2</sub>	315 V	315 V
V <sub>a</sub> p-p	6.9 kV	6.6 kV
I <sub>a</sub> p-p	620 mA	630 mA
W <sub>a</sub>	27 W	29 W
PY 500		
Ik	510 mA	600 mA
V <sub>k</sub>	5.4 kV	5.1 kV
I <sub>k</sub> rest (end of scan)	80 mA	80 mA

October 1968

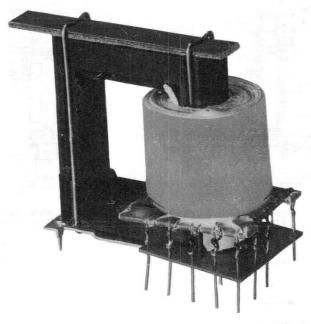
3122 107 31270

AT 2050 / 03





## LINE-DEFLECTION TRANSFORMER



RZ 22830-7B

### APPLICATION

This transformer has been designed to be used in combination with the E.H.T. transformer AT 2052/... to drive a colour picture tube with a deflection angle of  $90^{\circ}$  and an E.H.T. of 25 kV.

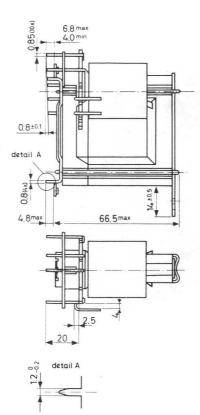
It is intended for use in conjunction with deflection unit AT 1027/.. or AT 1022/.., linearity control AT 4042/.., transductor AT 4041/.., line-output tube PL500, focus voltage rectifier DY51 and booster diode PY88.

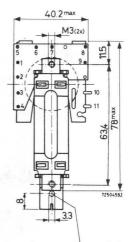
### 3122 108 39390

### MECHANICAL DATA

The coil is dipped in a flame retarding polyester.

Dimensions in mm







#### Mounting

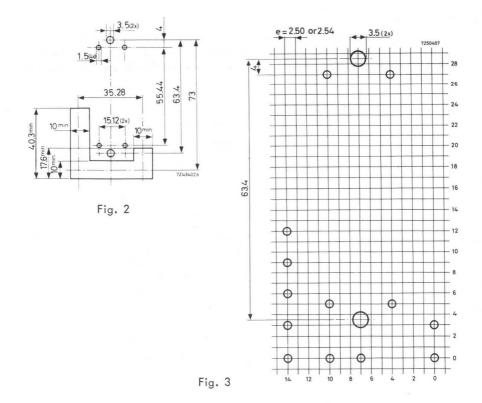
The transformer can be mounted on either a printed-wiring board or a metal chassis. If a metal chassis is used, holes for the pins must be cut in it in accordance with Fig. 2. The transformer must be secured with two 3mm screws. The mounting pins can be bent or soldered.

For mounting on a printed-wiring board the fit of the connecting and mounting pins in a printed-wiring grid with a pitch of 2.54 or 2.50 mm is illustrated in Fig. 3. The metal bracket must be connected to the chassis.

Like the other connections, those to the PL500 and PY88 can be soldered to the printedwiring board. If bent upwards (as supplied) they are very suitable for direct connection to the top caps of these tubes.

H46

AT 2051/00



The distance between the primary coil and any flat and smooth metal part should be at least 10mm.

The transformer and the leads and components carrying high tension pulses should be kept free from metal particles, solder drops etc.

The operating temperature of the transformer coils and the core should not exceed 95 °C under worst circumstances, i.e. taking into account:

- overvoltage

- low atmospheric pressure (at high altitudes) implying bad cooling by convection

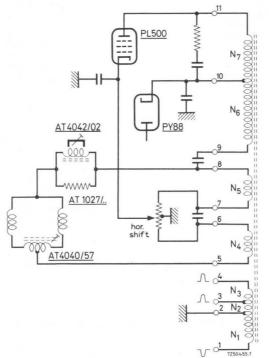
- high room temperature (up to  $45 ^{\circ}C$ )

Direct heat radiation from the PL500 and PY88 anodes to the transformer and the heater cable should be avoided by a screen. (If this screen is made from insulating material, it should be placed at least 15 mm from the coils).

Ample cool air circulation should be provided around the transformer.

### ELECTRICAL DATA

The following data are based on a circuit with a convergence load of about 10W (on the input side) and about 4W (on the output side) for stabilisation, burst suppression, blanking, synchronisation, frame output, etc. For more details see corresponding application information (e.g. A.I. 238).



### Fig. 4

Flyback time 18%	PY88	PL500	
Stabilisation V <sub>b</sub> - 12% <sup>1)</sup> Overscan 6%	Vb = 240 V	V <sub>g2</sub> = 203 V	
Deflection current 2.8 A <sub>p-p</sub>	V <sub>boost</sub> (between point 9 and	I <sub>a p-p</sub> = 410 mA	
	anode) = 580 V	I <sub>k p-p</sub> = 435 mA	
<sup>1)</sup> The stabilisation can be	l <sub>a</sub> (av) = 180 mA l <sub>a</sub> end-of-scan	$V_{a p-p} = 6.2 \text{ kV}$	
improved to V <sub>b</sub> – 15% with the PL504 (instead of PL500)	= 30 mA	$W_a = 11.5 W$	
at $V_b = 255 V$ .	l <sub>a p-p</sub> = 390 mA V <sub>a p-p</sub> = 5 kV	$W_{g2} = 2 W$	

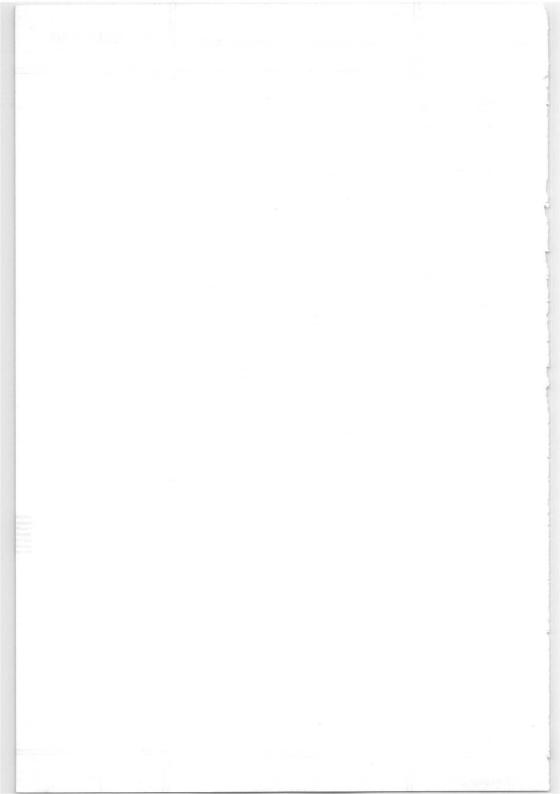
3122 108 39390

### Auxiliary windings

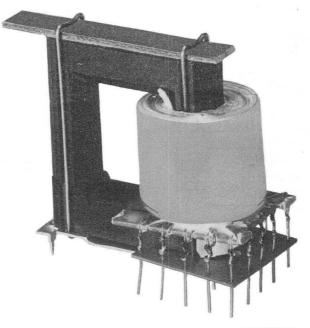
Connection 2 to c	chassis: + 110	) V <sub>p-p</sub> between	3 and 2
	+ 250	) V <sub>p-p</sub> between	4 and 2
	- 250	) V <sub>p-p</sub> between ) V <sub>p-p</sub> between	1 and 2
Connection 3 to c	chassis: + 140	Vp-p between	4 and 3
	- 360	) V <sub>p-p</sub> between	1 and 3
	- 110	) V <sub>p-p</sub> betweer ) V <sub>p-p</sub> betweer	2 and 3

### Notes

- 1. With a view to the total load of the transformer the average booster current (PY88,  $\rm I_a)$  must not exceed 200 mA .
- 2. An excessive additional capacitive load on a connection point of the transformer may increase the ringing just after flyback.
- 3. For adjustment of the amplitude V may be set to within ±4% of the given nominal value.



## LINE-DEFLECTION TRANSFORMER



RZ 22830-7A

### APPLICATION

This transformer has been designed to be used in combination with the E.H.T. transformer AT 2052/.. to drive a colour picture tube with a deflection angle of 90° and an E.H.T. of 25 kV.

It is intended for use in conjunction with deflection unit AT1027/.. or AT1022/.., linearity control AT4042/.., transductor AT4041/.., line-output tube PL500, focus voltage rectifier DY51 and booster diode PY88.

### AT 2051 / 01

### 3122 108 39400

40.2 max

F

to secure tube socket of focus rectifier

3.3

M3(2x)

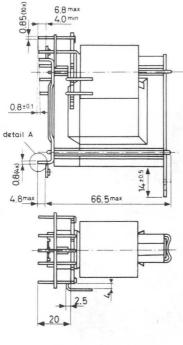
63.4

7249402.1

### MECHANICAL DATA

The coil is dipped in a flame retarding polyester.

Dimensions in mm







# Fig.

Mounting

The transformer can be mounted on either a printed-wiring board or a metal chassis. If a metal chassis is used, holes for the pins must be cut in it in accordance with Fig. 2. The transformer must be secured with two 3mm screws. The mounting pins can be bent or soldered.

For mounting on a printed-wiring board the fit of the connecting and mounting pins in a printed-wiring grid with a pitch of 2.54 or 2.50mm is illustrated in Fig. 3. The metal bracket must be connected to the chassis.

Like the other connections, those to the PL500 and PY88 can be soldered to the printedwiring board. If bent upwards (as supplied) they are very suitable for direct connection to the top caps of these tubes.

AT 2051/01

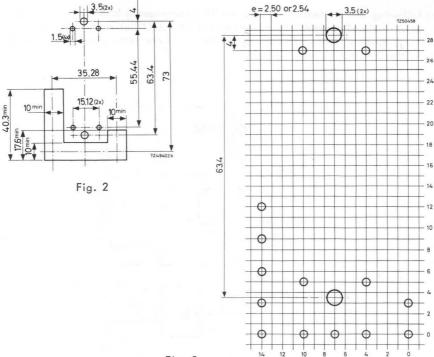


Fig. 3

The distance between the primary coil and any flat and smooth metal part should be at least 10mm.

The transformer and the leads and components carrying high tension pulses should be kept free from metal particles, solder drops etc.

The operating temperature of the transformer coils and the core should not exceed 95 °C under worst circumstances, i.e. taking into account:

- overvoltage

- low atmospheric pressure (at high altitudes) implying bad cooling by convection high area to respect to  $45^{\circ}$ 

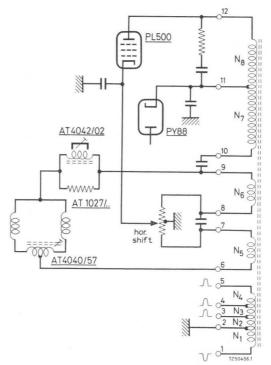
- high room temperature (up to 45  $^{\circ}C$ )

Direct heat radiation from the PL500 and PY88 anodes to the transformer and the heater cable should be avoided by a screen. (If this screen is made from insulating material, it should be placed at least 15 mm from the coils).

Ample cool air circulation should be provided around the transformer.

### ELECTRICAL DATA

The following data are based on a circuit with a convergence load of about 10W (on the input side) and about 4W (on the output side) for stabilisation, burst suppression, blanking, synchronisation, frame output, etc. For more details see corresponding application information (e.g. A.I. 238).



### Fig. 4

Flyback time 18% 1)	PY88	PL500
Stabilisation V <sub>b</sub> - 12% <sup>1)</sup> Overscan 6%	V <sub>b</sub> = 240 V	$V_{g2} = 203 V$
Deflection current 2.8 A <sub>p-p</sub>	V <sub>boost</sub> (between point 10 and	$I_{a p-p} = 410 \text{ mA}$
7.)	anode) = 580 V	$I_{k p-p} = 435 \text{ mA}$
1) The stabilisation can be	l <sub>a</sub> (av) = 180 mA l <sub>a</sub> end-of-scan	$V_{a p-p} = 6.2  kV$
improved to V <sub>b</sub> - 15%with the PL504 (instead of PL500)	= 30 mA	$W_{\alpha} = 11.5 W$
at $V_b = 255 V$ .	l <sub>a p-p</sub> = 390 mA V <sub>a p-p</sub> = 5 kV	$W_{g2} = 2 W$

3122 108 39400

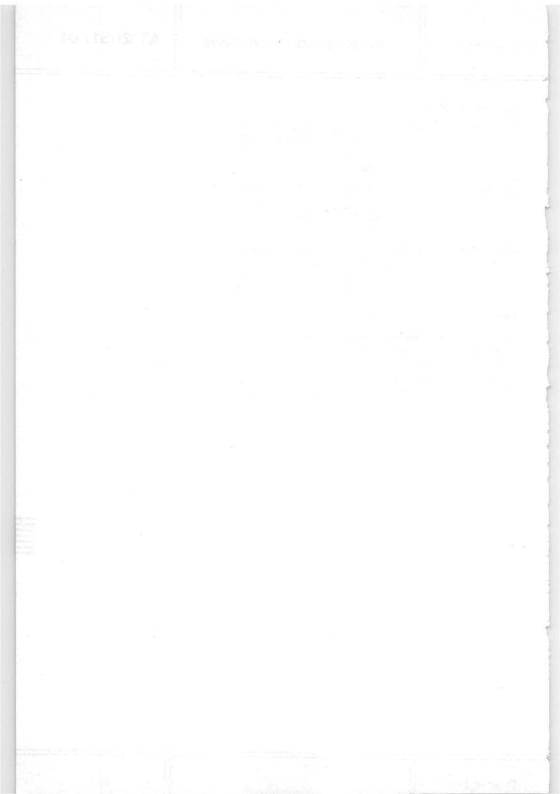
### Auxiliary windings

Connection 2 to chassis:	+ 55 V <sub>p-p</sub> between 3 and 2 + 110 V <sub>p-p</sub> between 4 and 2 + 405 V <sub>p-p</sub> between 5 and 2 - 295 V <sub>p-p</sub> between 1 and 2
Connection 3 to chassis:	+ 55 V <sub>p-p</sub> between 4 and 3 + 350 V <sub>p-p</sub> between 5 and 3 - 350 V <sub>p-p</sub> between 1 and 3 - 55 V <sub>p-p</sub> between 2 and 3
Connection 4 to chassis:	+ 295 V <sub>p-p</sub> between 5 and 4 - 405 V <sub>p-p</sub> between 1 and 4 - 110 V <sub>p-p</sub> between 2 and 4 - 55 V <sub>p-p</sub> between 3 and 4

### Notes

- 1. With a view to the total load of the transformer the average booster current (PY88,  $\rm I_{a})$  must not exceed 200 mA .
- 2. An excessive additional capacitive load on a connection point of the transformer may increase the ringing just after flyback.
- 3. For adjustment of the amplitude V<sub>boost</sub> may be set to within ± 4% of the given nominal value.

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### AT 2052/03

## E.H.T. TRANSFORMER



RZ 22830-1

### APPLICATION

This transformer is intended for use in combination with the line deflection transformer AT2051/... to generate the E.H.T.

### MECHANICAL DATA

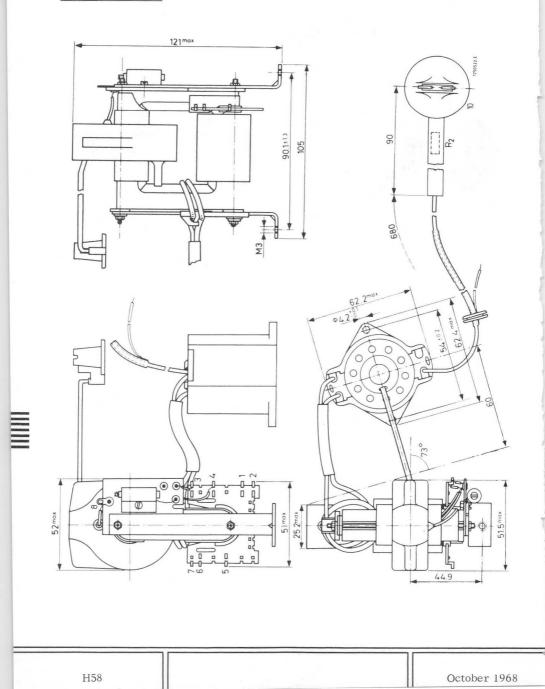
The primary coil is dipped and the  ${\rm E.H.T.}$  coil is encapsulated in flame retarding polyester.

# AT 2052/03

### E.H.T. TRANSFORMER

3122 108 39850

Dimensions in mm



### Mounting instructions

### 1. Temperature

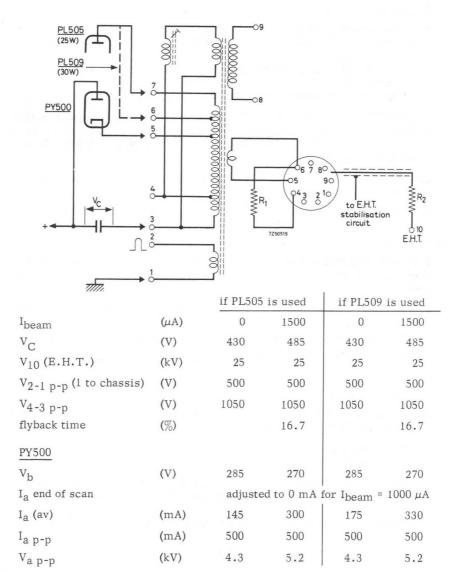
- a. The operating temperature of the transformer coils and the core should not exceed 95 <sup>o</sup>C under worst circumstances, i.e. taking into account:
   - overvoltage
  - low atmospheric pressure (at high altitudes) implying bad cooling by convection
  - high room temperature (up to 45 °C).
- b. Direct heat radiation from the PL505 and PY500 to the transformer and the heater cable of the GY501 should be avoided by a screen. (If this screen is made from insulating material, it should be placed at least 20 mm from the coils.)
- c. The socket of the GY501 should not be exposed to any direct heat radiation from the PL505 and the PY500.
- d. Ample cool air circulation should be provided around the transformer.
- 2. Distances

It is important in the design of a E.H.T. stage to maintain certain minimum distances between the transformer and the surrounding components and shields.

- a. The radial distance between the E.H.T. coils and any flat metal part (free from sharp edges) should be at least 25 mm.
   The axial distance from the E.H.T. coil should be at least 20 mm.
- b. The distance from the E.H.T. cap and lead should be at least 45 mm.
- c. The distance between the primary coil and any flat and smooth metal part should be at least 10 mm.
- d. The distance between the upper edge of the GY501 socket and the primary coil should be at least 15 mm.
- e. The distances between the caps of PL505 and PY500 and any flat and smooth metal part should be at least 15 mm.
- f. The transformer and the leads and components carrying high tension pulses should be kept free from metal particles, solder drops etc.
- 3. The metal bracket must be connected to the chassis.

## AT 2052/03

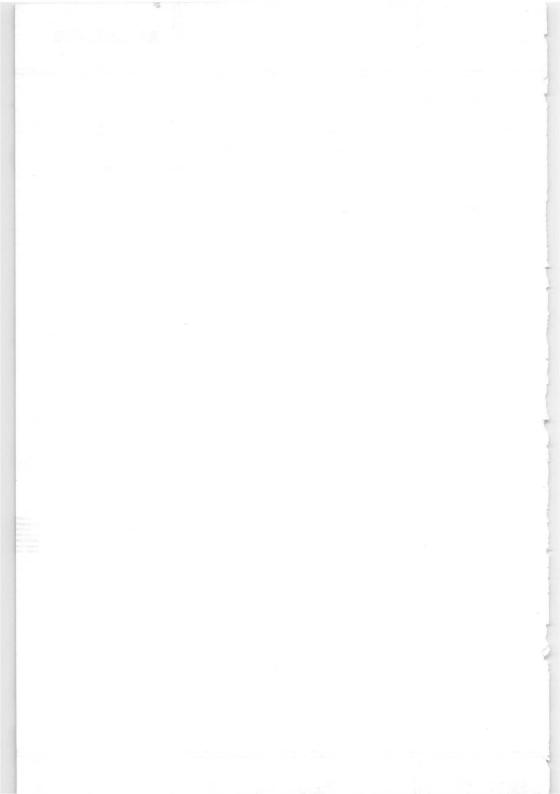
### ELECTRICAL DATA



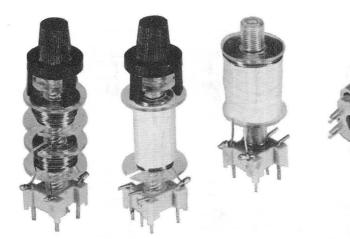
3122 108 39850

### ELECTRICAL DATA (continued)

			if PL505 is used		if PL509 is used			
	I <sub>beam</sub>	(µA)	0	1500	0	1500		
	I <sub>a</sub> p-p	(mA)	430	730	430	730		
	Ig2 p-p	(mA)	45	70	45	70		
	$I_{g2}$ (av)	(mA)	12	25	12	25		
	I <sub>k p-p</sub>	(mA)	475	800	475	800		
	V <sub>a p-p</sub>	(kV)	5.5	6.8	5.5	6.8		
	Wa	(W)	25	21	27.5	28.5		
	Wg2	(W)	3	5.5	3	5.5		
	stabilisation to	(V)		230		215		



## CONVERGENCE AND PIN-CUSHION ADJUSTORS



RZ 24284-5

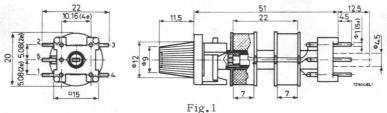
RZ 24284-6

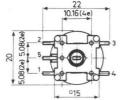
### APPLICATION

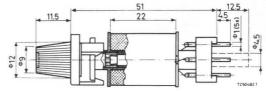
The convergence adjustors are intended for use in conjunction with the convergence unit AT1023/.., AT4045/.. or AT4046/.. for convergence adjustment. The pin-cushion adjustors are intended for use in conjunction with the transductor AT4041/.. (for pin-cushion adjustment), and deflection unit AT1027/.. or AT1022/..; the adjustor AT4040/50 for deflection units with parallel connected frame coils, the adjustor AT4040/55 for deflection units with series connected frame coils.

### MECHANICAL DATA

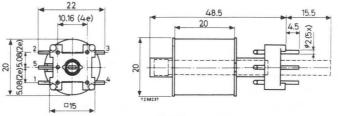
The convergence adjustors are provided with pins for mounting on printed-wiring boards and have a knob at the top for adjustment. Except for the AT4040/17 which can easily be soldered directly on the soldering tags of the deflection unit and can be adjusted by means of a screw-driver. Also the pin-cushion adjustors can be adjusted by means of a screw-driver and are suitable for mounting on printed-wiring boards.



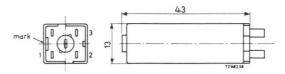














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# CONVERGENCE AND PIN-CUSHION ADJUSTORS

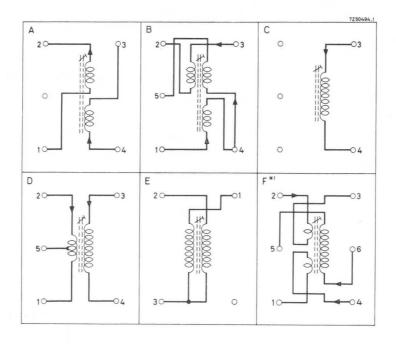
AT 4040/..

type number 1)	circuit diagram	Fig.	ter- minals	L-range *) (mH)	d.c. *) resistance (Ω)	catalog number
Convergence	adjustors	2)				
(AT4040/17)	Е	4	1-3 2-3	0.1-0.32	0.66	3122 107 30740
AT4040/49	A	1	1-2 3-4	0.32-1.08	2.4	3122 107 30030
(AT4040/52)	С	2	3-4	0.925-5.0	4.1	3122 107 30050
AT4040/53	D	2	3-4	0.635-3.725	3.65	3122 107 30060
(AT4040/54)	С	2	3-4	0.035-0.275	0.88	3122 107 30070
AT4040/56	В	1	1-4 5-4	0.00575-0.0225	0.11	3122 107 30080
			2-3	0.0295-0.0105	0.165	
AT4040/57	А	1	1-2 3-4	0.1-0.32	0.66	3122 107 30090
(AT4040/58)	А	1	1-2 3-4	2.5-8.25	20.7	3122 107 30100
(AT4040/59)	С	2	3-4	10-45	28	3122 107 30110
(AT4040/61)	D	2	3-4	7.2-33.5	23.1	3122 107 30130
AT4040/63	А	1	1-2 3-4	0.117-0.44	1.35	3122 107 30480
(AT4040/67)	F	2**)	5-6	0.7-3.6	3.65	3122 107 30570
Pin-cushion a	adjustors					
AT4040/50	C	3	3-4	0.9-3.2	1.1	3122 107 31210
(AT4040/55)	С	3	3-4	3-10	4.1	3122 107 31220

\* ) Typical values.

- \*\*) However, with a 6-pins socket.
- 1) Type numbers between brackets for non-preferred types.
- <sup>2</sup>) At a frequency of 15 kHz, the current through the convergence adjustment coils has to be such that the formula  $I^2_{\rm RMS}$ .  $R_{\rm dc} \leq 0.3$  W remains in force.

### ELECTRICAL DATA

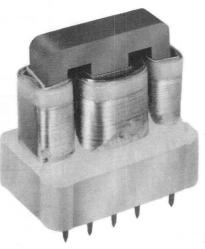


\*) The socket has a colour dot near pin 5.

H66

NON-PREFERRED

# TRANSDUCTOR



RZ 22830-6

### APPLICATION

The AT4041/05 is intended for use in conjunction with deflection unit AT1027/.., line output transformer AT2050/.., pin-cushion adjustor AT4040/.. and a frame output transformer to correct pin-cushion distortion.

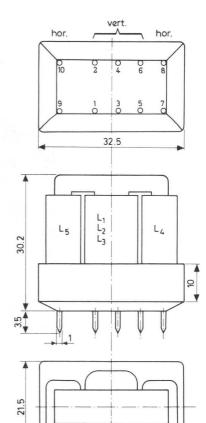
## AT 4041/05

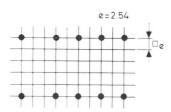
### TRANSDUCTOR

3122 107 30610

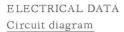
### MECHANICAL DATA

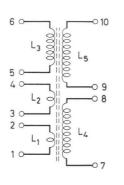
Dimensions in mm





Hole pattern for mounting on a printed-wiring board.



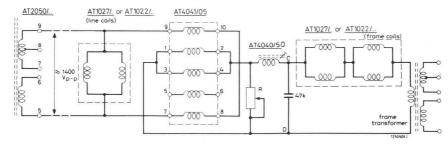


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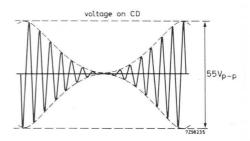
7249397.3

Connections

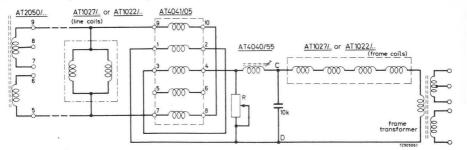
For AT1027/.. or AT1022/.. with parallel connected frame coils



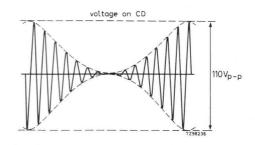
R = potentiometer of 47  $\Omega$ , adjusted to 20  $\Omega$  (typical value)



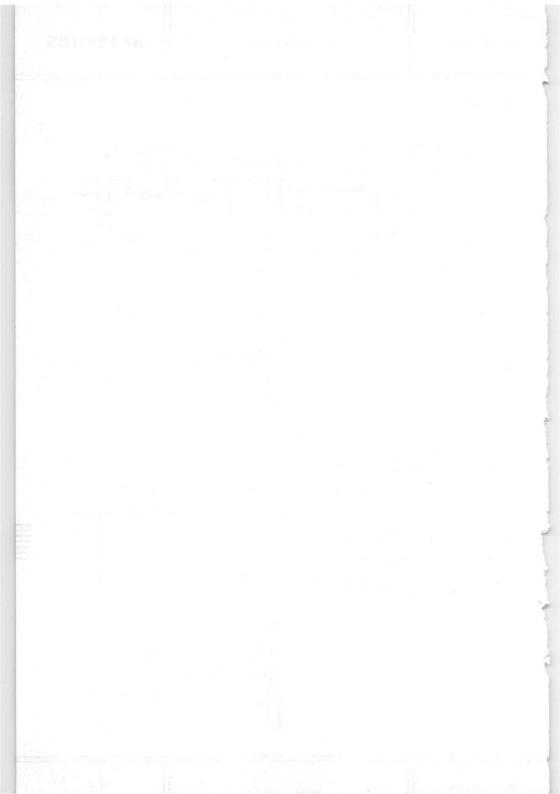
For AT1027/.. or AT1022/.. with series connected frame coils



R = potentiometer of 150  $\Omega$ 

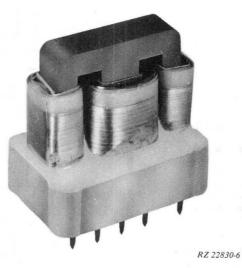


October 1968



## AT 4041/06

## TRANSDUCTOR



### APPLICATION

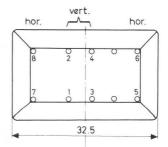
The AT4041/06 is intended for use in conjunction with deflection unit AT1027/.. or AT1022/.., line deflection transformer AT2051/.., pin-cushion adjustor AT4040/.. and a frame output transformer to correct pin-cushion distortion.

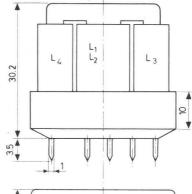
## AT 4041/06

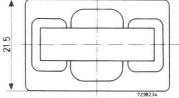
### TRANSDUCTOR

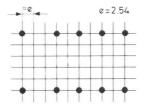
### MECHANICAL DATA

### Dimensions in mm





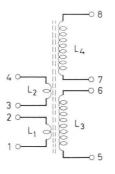




Hole pattern for mounting on a printed-wiring board.

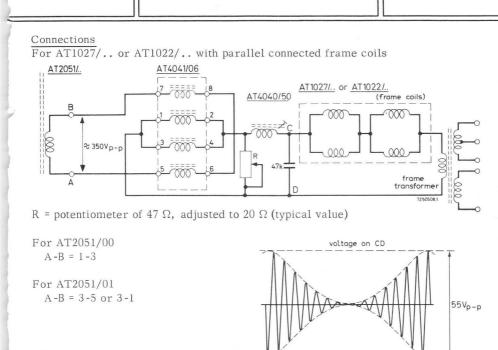
ELECTRICAL DATA

Circuit diagram

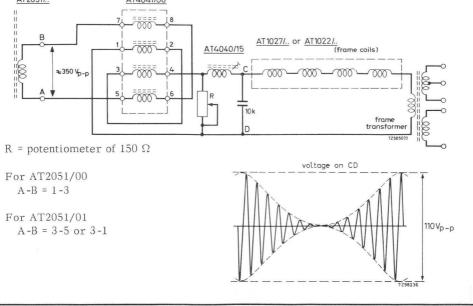




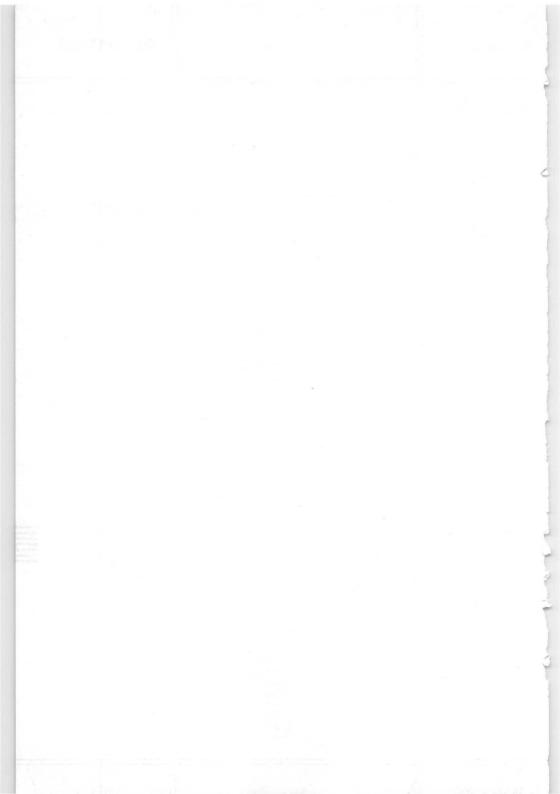
7298235



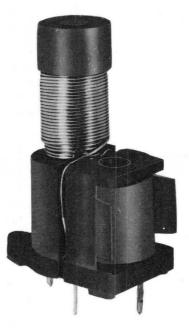
For AT1021/.. or AT1022/.. with series connected frame coils <u>AT2051/.</u> <u>AT4041/06</u>



October 1968



## ADJUSTABLE LINEARITY CONTROL UNIT



RZ 22858-8

#### APPLICATION

This unit is intended to be used in black and white, and in colour TV sets equipped with tubes, to adjust the linearity of the line-deflection. In colour TV sets it can be used in combination with deflection unit AT 1027/.. or AT 1022/.. and line-output transformer AT 2050/.. or AT 2051/...

#### CONSTRUCTION

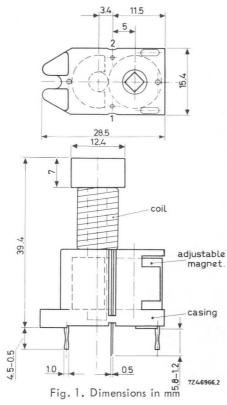
This control unit consists of a coil wound on a ferroxcube rod, and three ferroxdure magnets. One magnet is placed around the ferroxcube rod, above the coil. One of the magnets has the shape of a half ring, it is placed around the ferroxcube rod under the coil. The third ferroxdure magnet is cylindrical, it is positioned parallel to and clamped against the ferroxcube rod opposite the second. It is provided with a square hole to facilitate turning to adjust the biasing field and so the linearity of the line deflection.

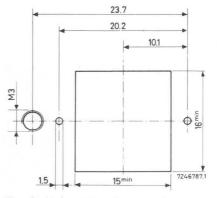
October 1968

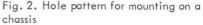
### AT4042/02

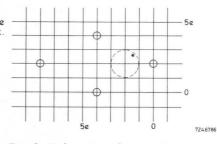
#### ADJUSTABLE LINEARITY CONTROL UNIT

#### 3122 108 39450











#### ELECTRICAL DATA

When a saw-tooth current (without S-correction) of  $2.8A_{p-p}$ , frequency 15,625 Hz, flyback ratio 18%, flows through the linearity control unit (one connection point to earth), the correction voltage is adjustable between 15V and 26V.

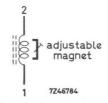


Fig. 4. Circuit diagram

#### MOUNTING

The unit can be mounted either on printed-wiring boards by means of its two connection pins and two mounting pins (see Fig. 3), or on metal chassis, by bending of the two mounting pins and/or by means of a screw through an aperture in the casing (see Fig. 2). To prevent distortion of the magnetic field no iron part should approach the magnetic parts anywhere nearer than 3 mm. The coil should be shunted with a carbon resistor to damp ringing phenomena(value of resistor depends on applied line-deflection transformer).

\*Hole only necessary for bottom adjustment.

AT4042/02

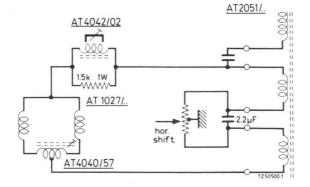
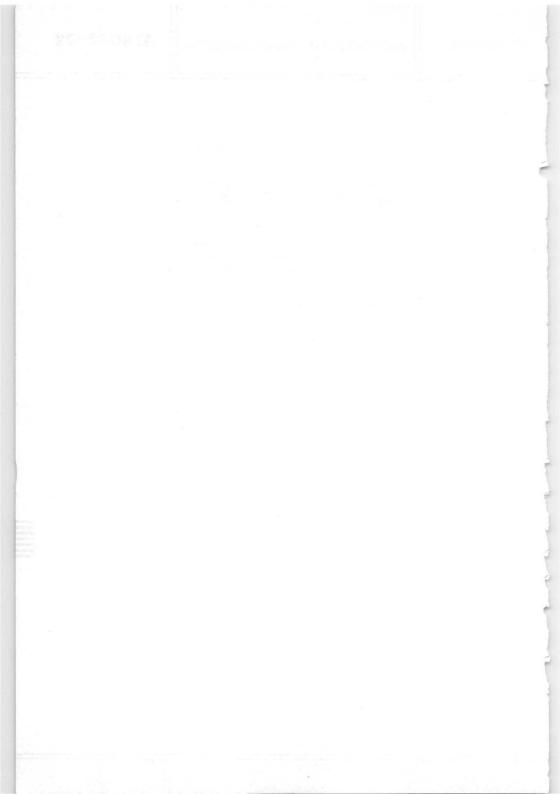


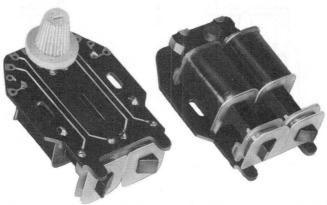
Fig. 5. Line-output circuit



3122 108 83130 3122 108 83150

## AT 4045/07 AT 4046/07

## **CONVERGENCE UNITS**



RZ 26110-4

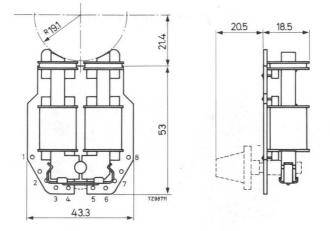
#### APPLICATION

These units are intended to be used with a  $90^{\circ}$  shadow mask colour picture tube, in conjunction with the deflection unit AT1027/.. and the blue lateral unit AT1025/05 or AT1028/.. to converge the three colour pictures statically and dynamically and to adjust the purity.

3122 108 83130 3122 108 83150

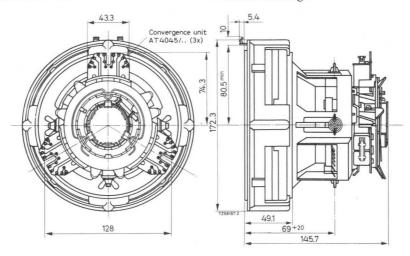
#### MECHANICAL DATA

#### Dimensions in mm



#### Mounting

The housing of the deflection unit AT1027/... is so constructed that the convergence units can easily slide in and then, after they have been properly pushed back, lock. The units have to be put into the housing with the printed wiring up (see drawing below). To take out the units the locks must be released; this can be done by pushing a screwdriver or the like between each unit and the housing.



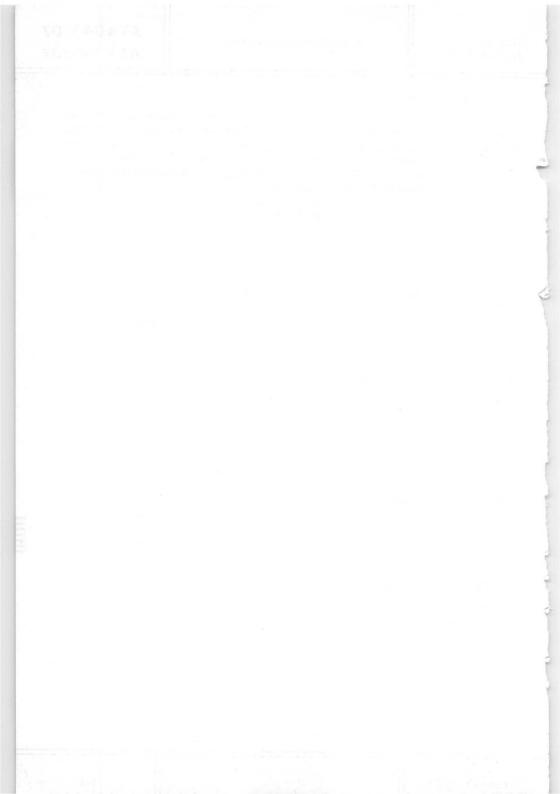
Assembly consisting of a deflection unit AT1027/.. and three convergence units AT4045/...

3122 108 83130 3122 108 83150

#### ELECTRICAL DATA

The units have 4 coils, two for horizontal and two for vertical deflection. They are mounted on a printed-wiring board. The coils can be connected either by soldering to the printed-wiring pads or by pushing a plug over the pins. The convergence unit AT4046/07 is provided with a permanent magnet for static convergence with which a shift of  $\pm > 20$  mm can be obtained. Static convergence with the AT4045/07 is effected by a d.c. current through its frame coils.

Series connected line coils	5 8 7 7 5 AT4045/07	AT4046/07
Inductance Resistance Connecting tags Tags to be interconnected	0.40 mH 2.5 Ω 3 and 7 2 and 6	0.43 mH 2.5 Ω 3 and 7 2 and 6
Parallel connected line coils		×
Inductance Resistance Connecting tags Tags to be interconnected	0.10 mH 0.6 Ω 2 and 3 2 and 7, 3 and 6	0.11 mH 0.6 $\Omega$ 2 and 3 2 and 7, 3 and 6
Series connected frame coils		
Inductance Resistance Connecting tags Tags to be interconnected	1.40 H 155 Ω 1 and 5 4 and 8	1.48 H 194 Ω 1 and 5 4 and 8
Parallel connected frame coils		
Inductance Resistance Connecting tags Tags to be interconnected	0.35 H 38.8 Ω 1 and 4 1 and 8, 4 and 5	0.37 H 48.5 Ω 1 and 4 1 and 8, 4 and 5

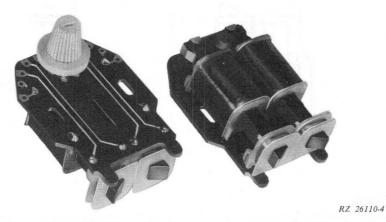


3122 108 83140 3122 108 83160

## AT 4045/08 AT 4046/08

NON-PREFERRED

## CONVERGENCE UNITS



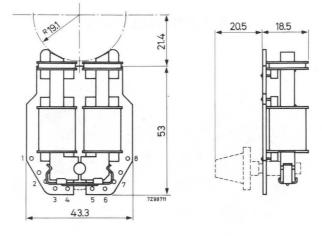
#### APPLICATION

These units are intended to be used with a  $90^{\circ}$  shadow mask colour picture tube, in conjunction with the deflection unit AT1027/.. and the blue lateral unit AT1025/05 or AT1028/.. to converge the three colour pictures statically and dynamically and to adjust the purity.

3122 108 83140 3122 108 83160

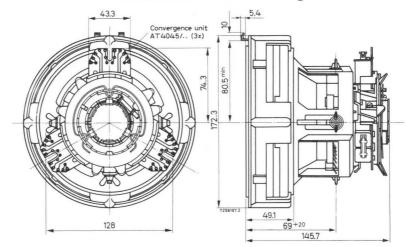
#### MECHANICAL DATA

Dimensions in mm



#### Mounting

The housing of the deflection unit AT1027/... is so constructed that the convergence units can easily slide in and then, after they have been properly pushed back, lock. The units have to be put into the housing with the printed wiring up (see drawing below). To take out the units the locks must be released; this can be done by pushing a screwdriver or the like between each unit and the housing.



Assembly consisting of a deflection unit AT1027/.. and three convergence units  $\rm AT4045/\ldots$ 

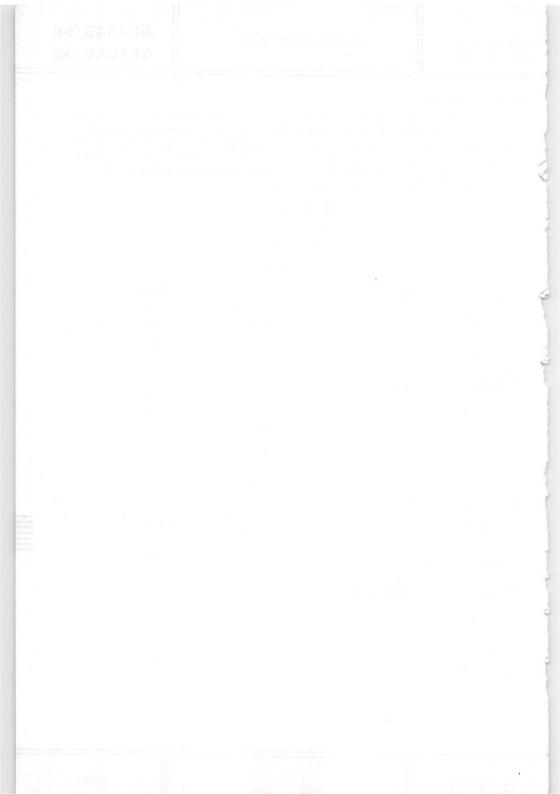
October 1968

3122 108 83140 3122 108 83160

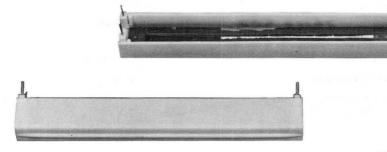
#### ELECTRICAL DATA

The units have 4 coils, two for horizontal and two for vertical deflection. They are mounted on a printed-wiring board. The coils can be connected either by soldering to the printed-wiring pads or by pushing a plug over the pins. The convergence unit AT4046/08 is provided with a permanent magnet for static convergence with which a shift of  $\pm > 20$  mm can be obtained. Static convergence with the AT4045/08 is effected by a d.c. current through its frame coils.

Series connected line coils	AT4045/08	AT4046/08
Inductance Resistance Connecting tags Tags to be interconnected	4.8 mH 22.6 Ω 3 and 7 2 and 6	5.2 mH 22.6 Ω 3 and 7 2 and 6
Parallel connected line coils		
Inductance Resistance Connecting tags Tags to be interconnected	1.2 mH 5.7 Ω 2 and 3 2 and 7, 3 and 6	1.3 mH 5.7 Ω 2 and 3 2 and 7, 3 and 6
Series connected frame coils		
Inductance Resistance Connecting tags Tags to be interconnected	1.40 H 155 Ω 1 and 5 4 and 8	1.52 H 194 Ω 1 and 5 4 and 8
Parallel connected frame coils		
Inductance Resistance Connecting tags Tags to be interconnected	0.35 H 38.8 Ω 1 and 4 1 and 8, 4 and 5	0.38 H 48.5 Ω 1 and 4 1 and 8, 4 and 5



## LUMINANCE DELAY LINE



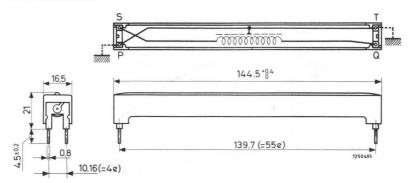
RZ 22858-3

#### APPLICATION

This delay line is intended for use in the luminance video amplifier of colour  $\ensuremath{\mathrm{TV}}$  sets.

#### MECHANICAL DATA

#### Dimensions in mm



e = 2.54 mm

October 1968

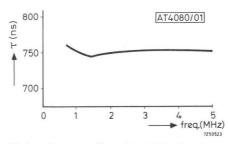
AT 4080 / 01

#### LUMINANCE DE LAY LINE

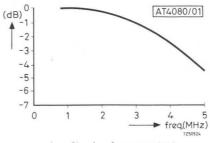
3122 107 31580

#### ELECTRICAL DATA

Delay time ( $\tau$ )	750 ns <u>+</u> 5 %
Rise time	85 ns
Impedance	1000 $\Omega$ ±10 $\%$
Temperature coefficient of the delay time	0.04 %/deg C
Maximum permissible temperature	90 °C
Maximum d.c. working voltage (between SQ and PT)	75 V
Pre-shoot	5 %



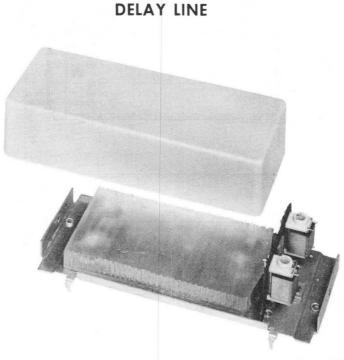
Delay time as a function of the frequency



Amplitude characteristic

DL1 E

NON-PREFERRED



#### RZ 24284-9

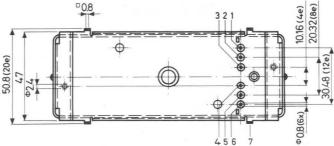
#### APPLICATION

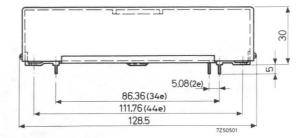
This delay-line is intended for use in the decoder circuits of television receivers. It consists of a glass delay-line, appropriate transductors and coils which are accurately adjusted during manufacture to provide the correct overall phase delay-time when fed by a source with an internal impedance of 100  $\Omega$  and terminated with a load of 100  $\Omega$ .

2722 121 00051

#### MECHANICAL DATA

Dimensions in mm



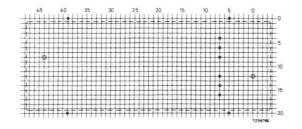


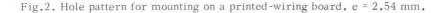


#### Weight 310 g

#### Mounting

The unit is intended for insertion directly into a printed-wiring board. Additionally, two holes are provided in the underside for the purpose of fixing the unit by means of self-tapping screws, if so required.





#### 2722 121 00051

#### DELAY LINE

DL1 E

#### ELECTRICAL DATA

Nominal frequency f<sub>nom</sub> Nominal phase delay-time (V1 - V2)at f<sub>nom</sub> (unmodulated sinewave voltage) Accuracy of adjustment -3 dB points (bandwidth)

Insertion loss Temperature drift (relative to 25  $^{\rm O}{\rm C}$ )

phase delay insertion loss Maximum input at  $f_{nom}$ (terminals 4 and 6) Termination impedances Unwanted reflections at  $3\tau$ other reflections

Operating temperature range Asymmetry of the coils at  $f_{\text{nom}} \left| \frac{V_0}{V_2} \right|$ 

#### 4.433619 MHz

63.943  $\mu$ s  $\pm$  5 ns one below 3.43 MHz, the other above 5.23 MHz 13  $\pm$  4 dB at f<sub>nom</sub> measured while temperature is made to rise linearly ( $\pm$  1 °C) in an interval of 3 h from 20 to 50 °C, after which it is kept constant at 50 °C for 2 h. max.  $\pm$  5 ns, typical value 3 ns typical  $\pm$  < 0.3 dB

#### 10 Vp-p 100 Ω

- < 22 dB with respect to  $1\tau$  signal - < 27 dB with respect to  $1\tau$  signal measured at  $f_{\rm nOM}$  with a burst of  $25\mu s$  length and a repetition frequency of 2.6 kHz  $-20~^{\rm o}{\rm C}/+70~^{\rm o}{\rm C}$ 

#### < 0.05 (see Fig. 4)

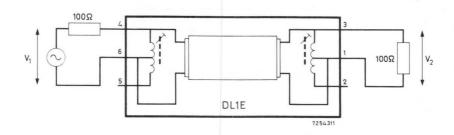
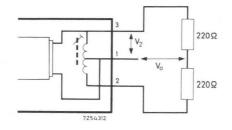


Fig.3. Circuit diagram and connections

DL1E

2722 121 00051





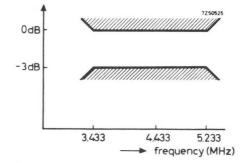
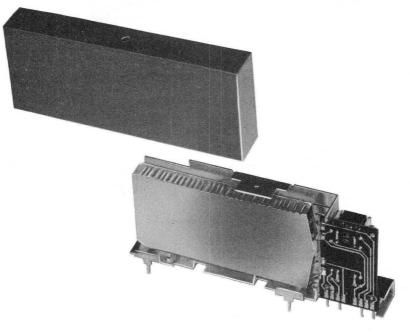


Fig.5. Amplitude limits of V<sub>2</sub>

October 1968

## DELAY LINE



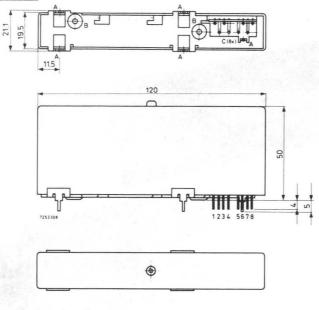
RZ 26110-2

#### APPLICATION

This delay-line is intended for use in the decoder circuits of television receivers. It consists of a glass delay-line, appropriate transductors and coils which are accurately adjusted during manufacture to provide the correct overall phase delay-time when fed by a source with an internal impedance of 100  $\Omega$  and terminated with a load of 100  $\Omega$ .

#### MECHANICAL DATA

#### Dimensions in mm



A = Fastening pins

B = Fixing holes

C = Connecting pins (0.8 mm diam.)

#### Weight 165 g

#### Mounting

The unit is intended for insertion directly into a printed-wiring board. Additionally, two holes are provided in the underside for the purpose of fixing the unit by means of M3 screws, if so required.

 40 35	5 30	25	20	15	10	5	0
•					┝┿┾╉┿	++++-	
					0		
				A		¢ (8+)	

Fig.2. Hole pattern for mounting on a printed-wiring board. e = 2.54 mm.

H94

October 1968

#### 2722 121 00061

DELAY LINE

**DL 20** 

#### ELECTRICAL DATA

Nominal frequency  $f_{nom}$ Nominal phase delay-time (V1 - V2)at  $f_{nom}$  (unmodulated sinewave voltage) Accuracy of adjustment -3 dB points (bandwidth)

Insertion loss Temperature drift (relative to  $25 \ ^{\circ}C$ )

phase delay insertion loss Maximum input at f<sub>nom</sub> (terminals 3 and 4) Termination impedances Unwanted reflections at 3τ other reflections

Operating temperature range Asymmetry of the coils at  $f_{nom} \left| \frac{V_0}{V_2} \right|$ 

#### 4.433619 MHz

63.943  $\mu$ s  $\pm$  5 ns one below 3.43 MHz, the other above 5.23 MHz 11  $\pm$  3 dB at f<sub>nom</sub> measured while temperature is made to rise linearly ( $\pm$  1 °C) in an interval of 3 h from 20 to 50 °C, after which it is kept constant at 50 °C for 2 h. max.  $\pm$  5 ns, typical value 3 ns typical  $\pm$  < 0.3 dB

10  $V_{p-p}$ 100  $\Omega$ - < 22 dB with respect to  $1\tau$  signal - < 27 dB with respect to  $1\tau$  signal measured at f<sub>nom</sub> with a burst of 25µs lenght and a repetition frequency of 2.6 kHz -20 °C/+ 70 °C

< 0.05 (see Fig.4)

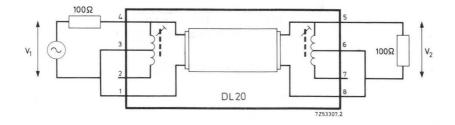
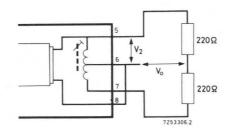
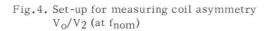


Fig.3. Circuit diagram and connections

**DL 20** 





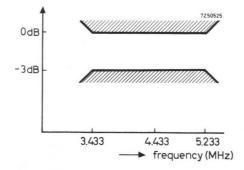
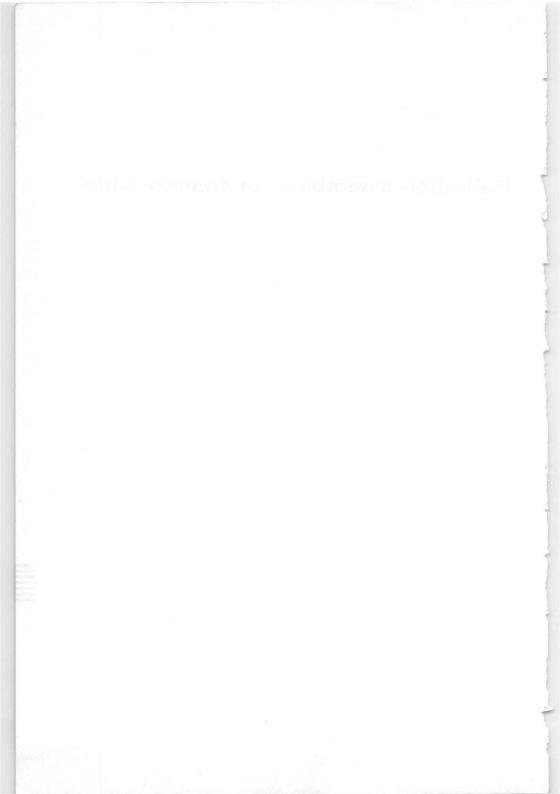


Fig.5. Amplitude limits of  $V_2$ 

# Deflection assemblies for camera tubes



3122 107 30580

AT1102

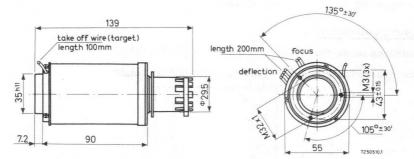
## VIDICON DEFLECTION UNIT

#### APPLICATION

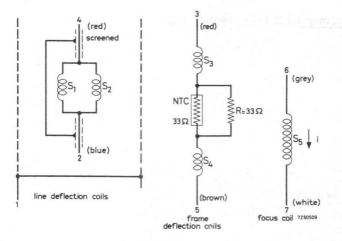
Deflection assembly, consisting of deflection and focus coils and alignment ring magnets, for a 1" Vidicon.

#### MECHANICAL DATA

Dimensions in mm



#### ELECTRICAL DATA (typical values)



January 1968

K3

AT1102

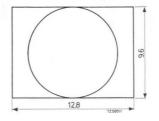
coils	measuring points	earth points	inductance (mH)	resistance (Ω)
$S_1 + S_2$	2 - 4	2	0.75	2.5
$s_3 + s_4$	3 - 5	5	23	80
S <sub>5</sub>	6 - 7	-	-	4200

Required currents for normal operation ( $V_{g4}$  = 300 V)

Line deflection current	:	170 mA p-p
Frame deflection current	:	24 mA p-p
Focus current	:	17 mA

Geometric distortion

Distortions inside the circle : about 1 % of picture height Distortions outside the circle : about 2 % of picture height



Alignment range:  $\pm \ge 10\%$  of picture height

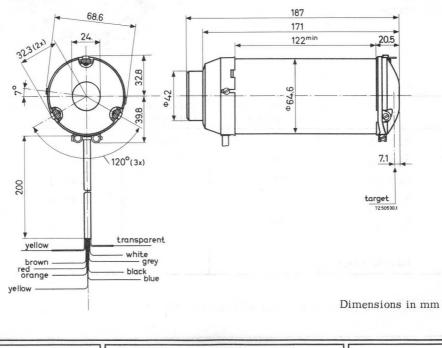
## PLUMBICON DEFLECTION UNIT



#### APPLICATION

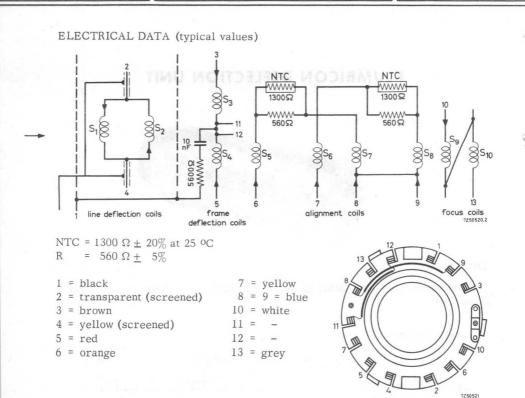
Deflection assembly, consisting of deflection, focus and alignment coils, for a Plumbicon.

MECHANICAL DATA



AT1113/01

3122 108 84401



coils	measuring points	inductance $(mH) \pm 3.5\%$	resistance at 25 °C (Ω) ±10%
$s_1 + s_2$	2 - 4	0.995	2.6
$s_3 + s_4$	3 - 5	22.1	63.8
$s_5 + s_7$	6 - 8	1. A 1.	2143 1)
$s_{6} + s_{8}$	7 - 9		2143 1)
$S_9 + S_{10}$	10 - 13		148
		1.1.4.162	Second States
Internal shield	1	0.00	North In

1) Resistance drift between 25 and 60 °C is < 0.75%

## AT1113/01

#### Required currents for normal operation

:

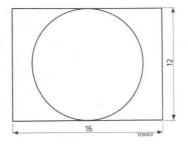
Line deflection current	
Frame deflection current	
Focus current	

V <sub>g3</sub> = 300 V	V <sub>g3</sub> = 600 V	
160 mA p-p	225 mA p-p	
25 mA p-p	35 mA p <b>-</b> p	
75 mA (S9+S <sub>10</sub> in series)	100 mA	
± 5 mA	<u>+</u> 5 mA	

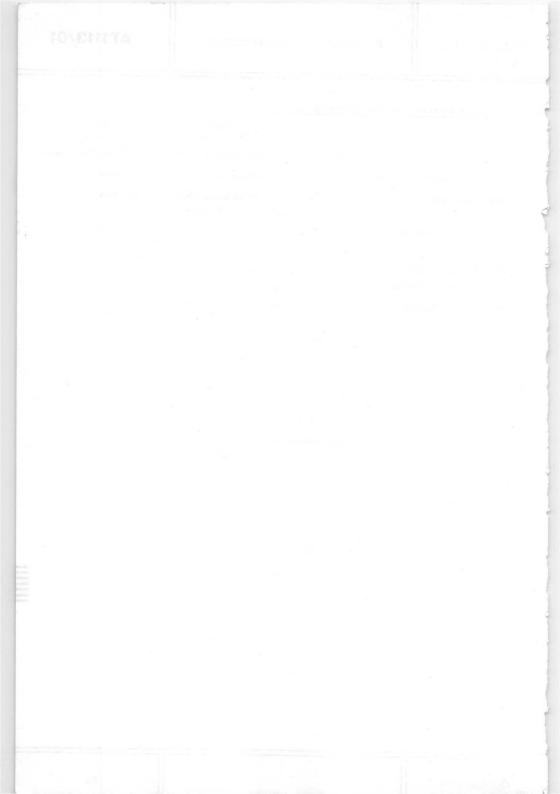
#### Maximum alignment currents :

#### Geometric distortion

Distortions inside the circle Distortions outside the circle max. 0.5 % of picture height
max. 1 % of picture height



October 1968



## **PLUMBICON DEFLECTION UNIT**



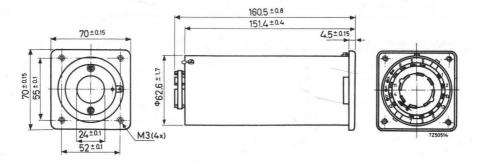
RZ 18033-18

#### APPLICATION

Deflection assembly, consisting of deflection, focus and alignment coils for a Plumbicon.

#### MECHANICAL DATA

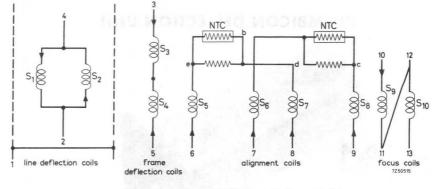
#### Dimensions in mm



AT1122

3122 108 39350

ELECTRICAL DATA (typical values)



NTC resistor: 1300  $\Omega$   $\pm 20$  % at 25 °C R : 560  $\Omega$   $\pm$  5 %

coils	measuring points	inductance (mH)	resistance (Ω)
$S_1 + S_2$	2 - 4	0.99	2.6
$s_3 + s_4$	3 - 5	22.1	63.8
$S_5 + S_7$	6 - 8		2390
$S_{6} + S_{8}$	7 - 9		2390
S <sub>9</sub>	12 - 13		1100
s <sub>10</sub>	10 - 11		1650
Internal shield	1		

Requi	red currents for normal operat	ion	(Vg <sub>3</sub> = 300 V)	$(V_{g_3} = 600 \text{ V})$	
	line deflection current	:	160 mA p-p	235 mA p-p	
	frame deflection current	:	25 mA p-p	35 mA p-p	
	focus current	:	17 mA (S <sub>9</sub> + S in serie		
	maximum alignment currents	:	±5 mA	$\pm 5 \text{ mA}$	

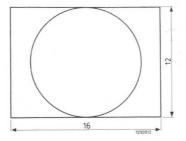
January 1968

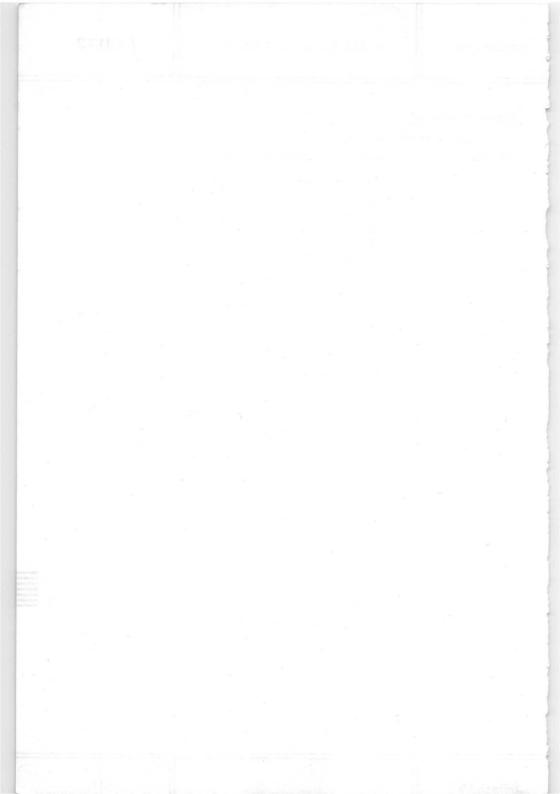
K10

AT1122

#### Geometric distortion

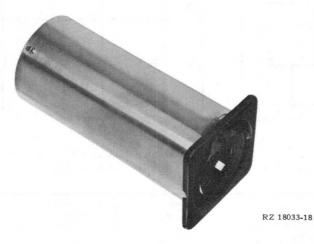
Distortions inside the circle : max. 1 % of picture height Distortions outside the circle : max. 2 % of picture height





# AT1132

# **PLUMBICON DEFLECTION UNIT**

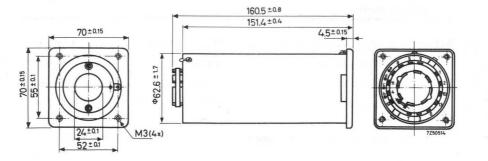


## APPLICATION

Deflection assembly, consisting of deflection, focus and alignment coils for a Plumbicon.

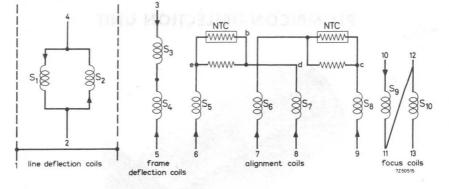
#### MECHANICAL DATA

# Dimensions in mm



AT1132

## ELECTRICAL DATA (typical values)



NTC resistor:  $1300 \Omega \pm 20 \%$  at 25 °C R : 560  $\Omega \pm 5 \%$ 

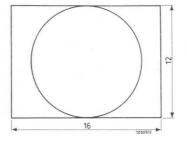
coils	measuring points	inductance (mH)	resistance (Ω)
$S_{1} + S_{2}$	2 - 4	0.99	2.6
$s_3 + s_4$	3 - 5	22.1	63.8
$S_5 + S_7$	6 - 8		2390
$S_{6} + S_{8}$	7 - 9		2390
S9	12 - 13		1100
s <sub>10</sub>	10 - 11		1650
Internal shield	1		

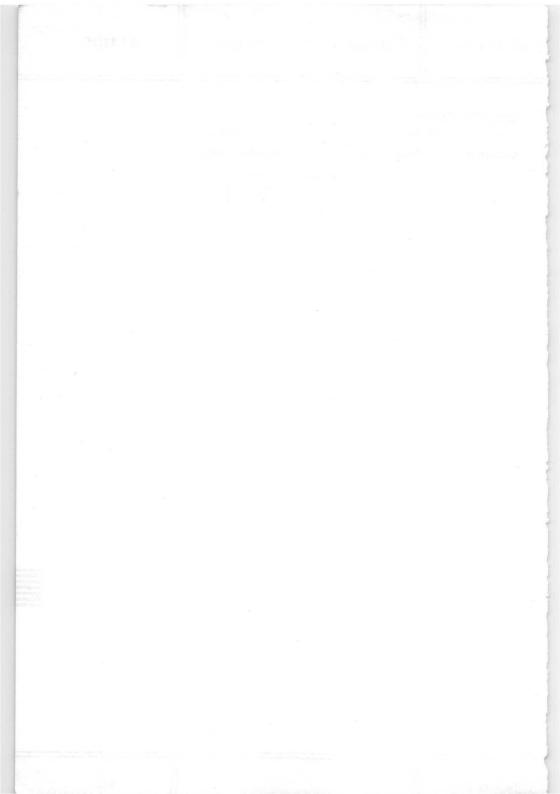
Required currents for normal oper	ation	(V <sub>g3</sub> = 300 V)	(V <sub>g3</sub> = 600 V)
line deflection current	:	160 mA p-p	235 mA p-p
frame deflection current	:	25 mA p-p	35 mA p-p
focus current	:	17 mA (S <sub>9</sub> + S <sub>10</sub> in series)	25 mA
maximum alignment curren	its:	$\pm 5 \text{ mA}$	$\pm 5 \text{ mA}$

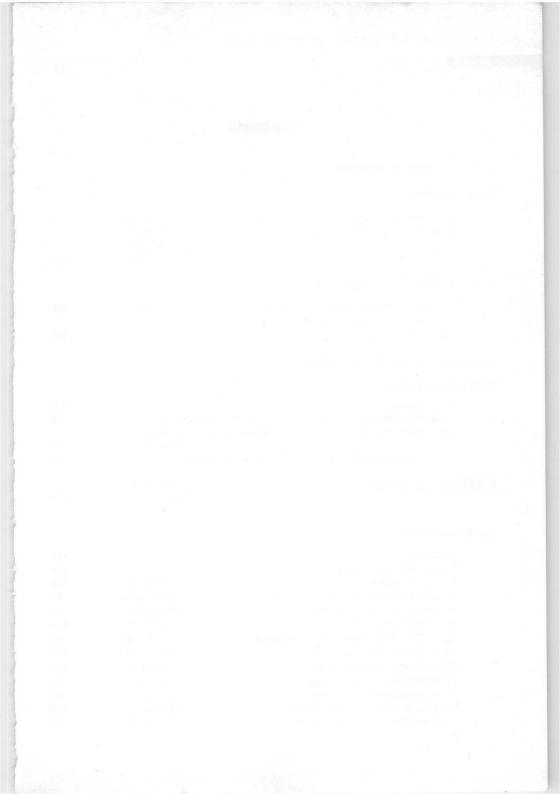
3122 108 39360

# Geometric distortion

Distortions inside the circle : max. 0.5 % of picture height Distortions outside the circle : max. -1~% of picture height







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