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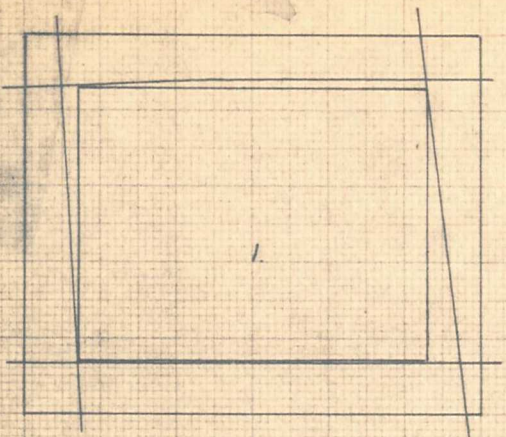
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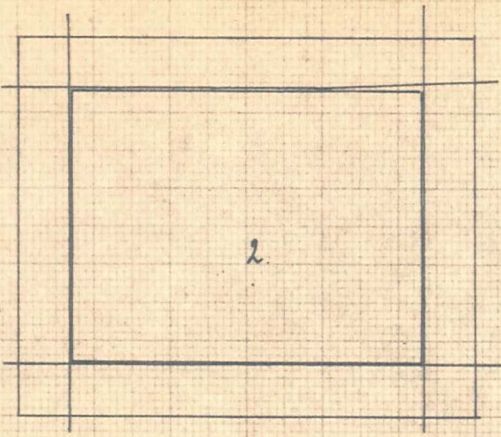
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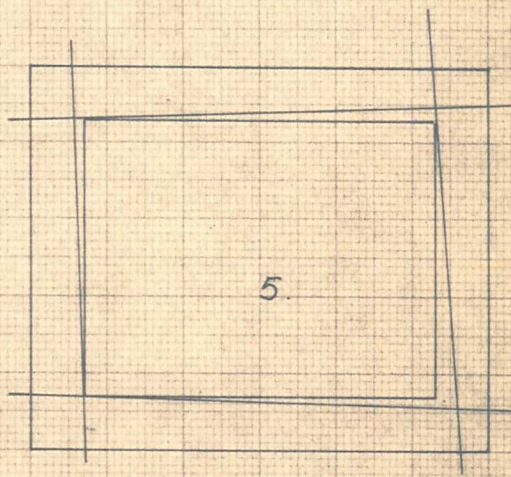
FVAR		STEMPEL:						ONTVANGEN OP:		VOOR:		GEZIEN:				D 10-160.	
KONTROLE - TEST		(V=)	7	7	7	7	7	7									
KONTROLE - CONTROLE		(V=)	150	150	300	300	300	300.									
N.V. PHILIPS' GLOEILAMPENFABRIEKEN		ISOLATIES.															
		METING	+K/-F	-K/+F	I	II	III	IV									
		OPM (T)	36	36	37	37	37	37									
		SCHEMA (T)	A2	A2	A2	A2	A2	A2.									
SERIE 1		1	0.6	6.2	0.2	0.2	0.2	6.8	238	17	99.8	51	132	94	41	5060	
		2	2.0	2.4	0.2	0.2	0.2	4.6	237	15.5	99.8	51	131	94	42	"	
		3	0.4	4.5	0.2	0.2	0.2	5.2	237	16	99.9	51	130	94	41	"	
		4	0.8	3.0	0.2	0.2	0.2	4.2	238	15	100.0	51	130	94	41	"	
		5	1.2	2.6	0.2	0.2	0.2	6.8	237	16.5	100.0	51	131	94	42	"	
		$\bar{x}$	1.0	3.7	0.2	0.2	0.2	5.3	237.4	16	99.9	51	130.8	94	41.4		
		R.	1.6	3.8	0	0	0	2.6	1	2	0.2	0	2	0	1		
SERIE 2		1	0.6	3.0	0.4	0.4	0.4	4.0	236	16	100.3	51	127	94	44	5060	
		2	2.0	6.4	0.4	0.4	0.4	4.2	234	15	100.2	51	127	94	44.5	"	
		3	0.2	3.0	0.4	0.4	0.4	4.2	236	16	100.0	51	136	94	45	"	
		4	1.4	3.0	0.4	0.4	0.4	3.8	235	16	100.3	51	126	94	43.5	"	
		5	1.6	6.2	0.4	0.4	0.4	5.4	235	16	101.0	51	127	94	44	"	
		$\bar{x}$	1.2	4.1	0.4	0.4	0.4	4.3	235.2	15.8	100.4	51	126.6	94	44.2		
		R.	1.8	3.4	0	0	0	1.6	2	1	1	0	1	0	1.5		
SERIE 3		1	1.6	4.0	0.4	0.4	0.4	4.6	236	17	100	51	129.5	94	44.5	5060	
		2	1.2	6.0	0.4	0.4	0.4	5.6	236	18	100	51	129	94	42	"	
		3	1.0	3.0	0.4	0.4	0.4	4.2	236	16	100.2	51	130	94	43.5	"	
		4	6.2	0.6	0.4	0.4	0.4	8.0	236	17	100.3	51	130	94	42.2	"	
		5	2.0	2.6	0.4	0.4	0.4	3.0	236.5	17	100.3	51	131	94	42.5	"	
		$\bar{x}$	2.4	3.0	0.4	0.4	0.4	5.1	236.1	17	100.2	51	129.9	94	42.1		
		R.	5.2	6.6	0	0	0	5.0	0.5	2	0.3	0	1.5	0	1		
SERIE 4		1	0.6	1.2	0.2	0.2	0.2	2.4	235.5	17.5	101	51	130	94	41	5060	
		2	2.4	6.0	0.2	0.2	0.2	6.2	237	17	100.8	51.2	129	94	41	"	
		3	2.2	6.2	0.2	0.2	0.2	4.8	236	16.5	100.6	50.9	130	94	41	"	
		4	1.4	4.8	0.2	0.2	0.2	5.2	236	16	100.5	51	129.5	94	42	"	
		5	1.2	6.0	0.2	0.2	0.2	5.0	236	16	101	51	130	94	41	"	
		$\bar{x}$	1.6	5.0	0.2	0.2	0.2	4.7	236.1	16.6	100.8	51	129.7	94	41.2		
		R.	1.8	5.0	0	0	0	3.8	1.5	1.5	0.5	0.8	1	0	1		
SERIE 5		1	0.2	1.4	0.2	0.2	0.2	6.0	236	16	100	51	130	94	41.2	5060	
		2	2.4	3.6	0.2	0.2	0.2	4.0	235	15.5	100.5	51	129	94	41.1	"	
		3	0.2	1.0	0.2	0.2	0.2	2.6	235	16	100.4	51	130	94	41.0	"	
		4	0.8	3.2	0.2	0.2	0.2	4.2	236	16	100.4	51.2	130	94	41.0	"	
		5	0.4	1.8	0.2	0.2	0.2	2.8	236	17	100.8	50.9	129	94	41.0	"	
		$\bar{x}$	0.8	2.2	0.2	0.2	0.2	4.1	235.6	16.1	100.4	51	129.6	94	41.1		
		R.	2.2	2.6	0	0	0	3.4	1	1.5	0.8	0.8	1	0	0.2		
SERIE 6		1	1.4	1.6	0.2	0.2	0.2	2.8	235	16	100.4	51	130	94	42	5060	
		2	0.8	7.4	0.2	0.2	0.2	5.4	235	16	101.0	51	129.5	94	41.5	"	
		3	1.6	6.0	0.2	0.2	0.2	5.6	235.5	16.5	100.0	51	129	94	41.5	"	
		4	1.2	9.4	0.2	0.2	0.2	5.4	235.5	17	100.0	51.1	129	94	41	"	
		5	0.8	4.0	0.2	0.2	0.2	4.6	236	16	100.7	51	130	94	41.5	"	
		$\bar{x}$	1.2	5.7	0.2	0.2	0.2	4.8	235.4	16.3	100.2	51	129.5	94	41.5		
		R.	0.8	7.8	0	0	0	2.8	1	1	0.7	0.1	1	0	1		
EISEN		S P. 5 STUKS 100"															
		MAX	45	45	3	3	3	3	9	232							
		MIN							1.0	15	0.6	0.1	0.1	0	0.1		
		MAX							232			49.5	120	85	30		
		MIN							140	10.5	102	52.5	140		50		
		MAX															
EENHEDEN		mm mm mm mm mm mm mm mm mm mm mm mm mm mm mm mm															
CONCLUSIE:																	



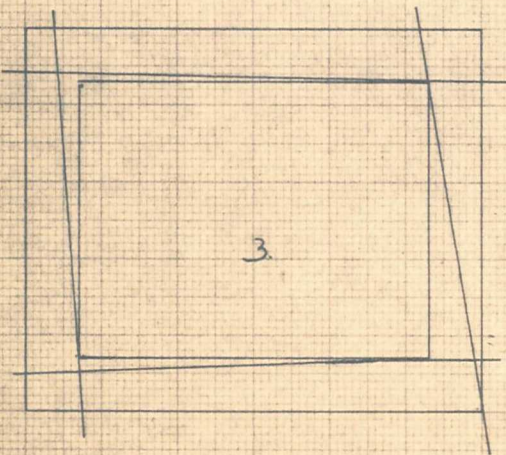
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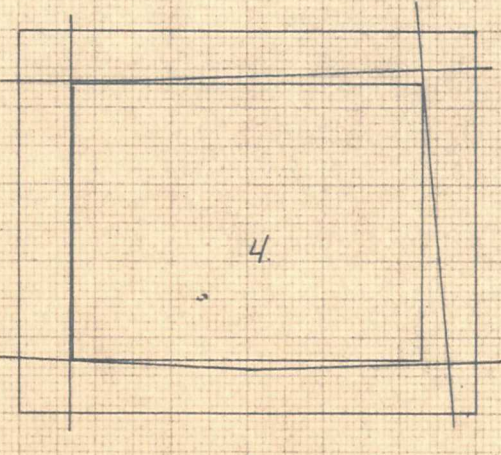
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5



3

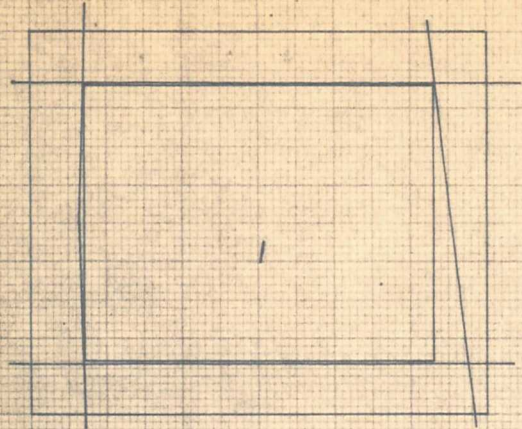


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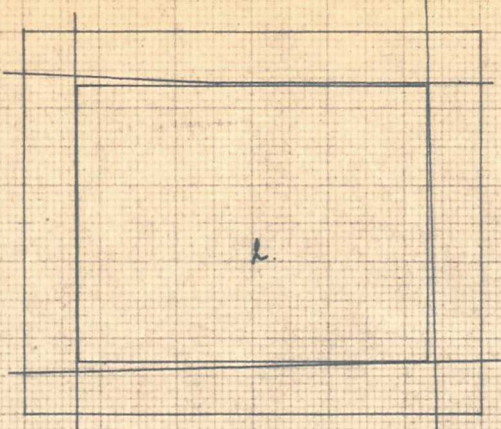
D 10-160 qH

MNI  
m 8 H 3.

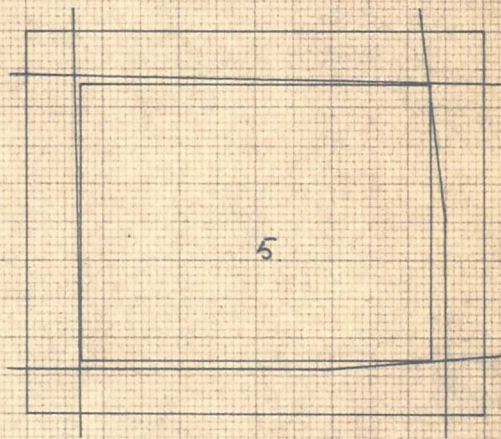
SERIE 1



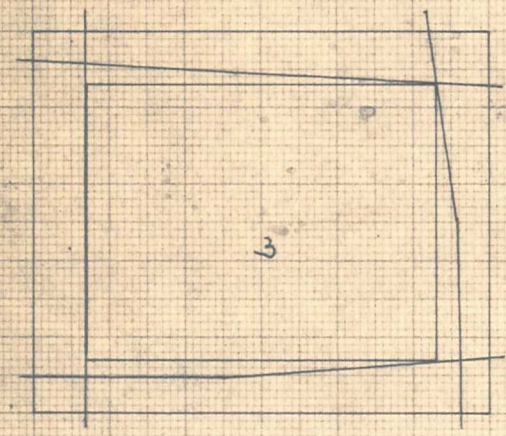
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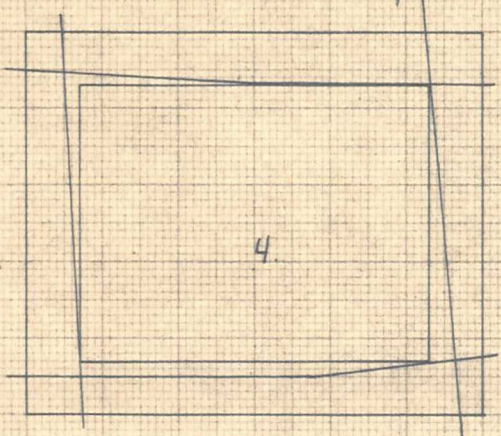
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5



3

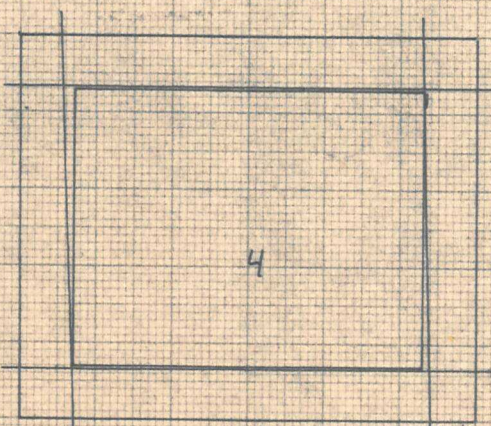
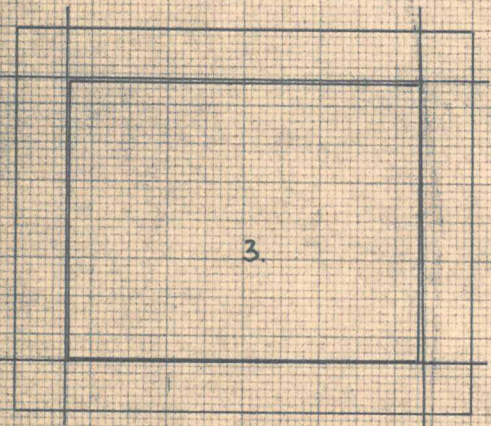
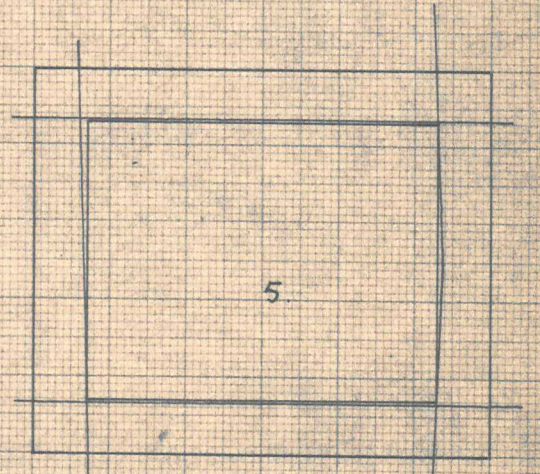
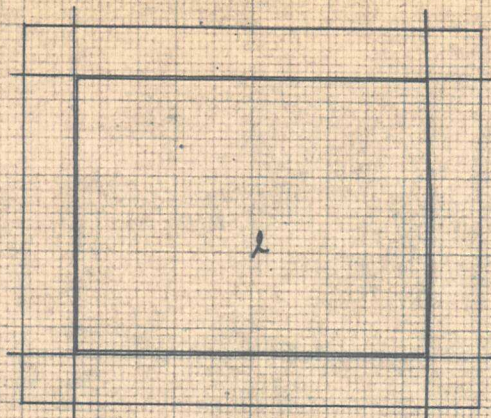
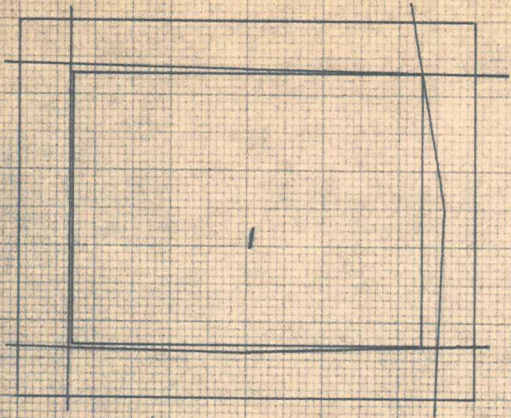


4

MNI 3.  
m 8 H

D 10-160 qH

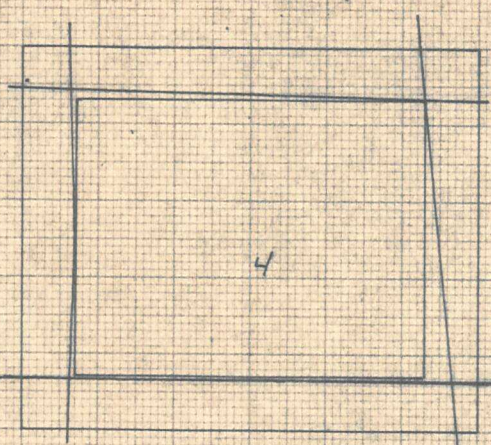
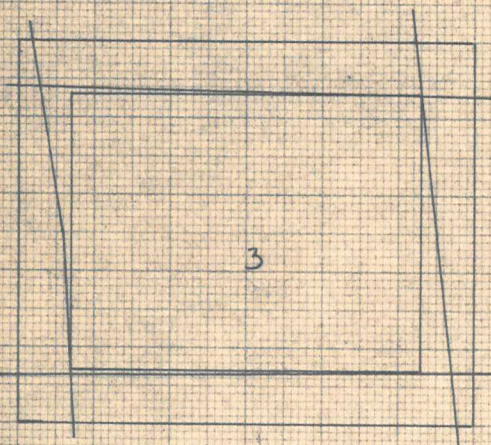
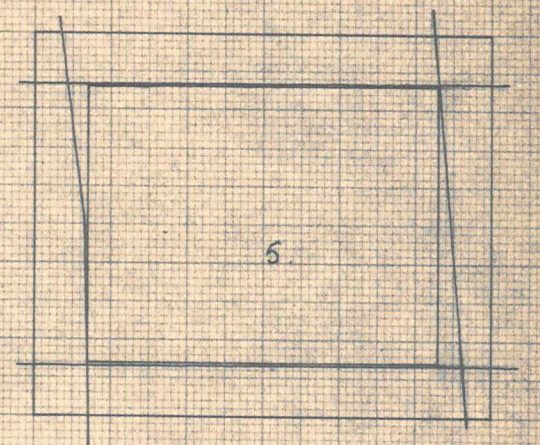
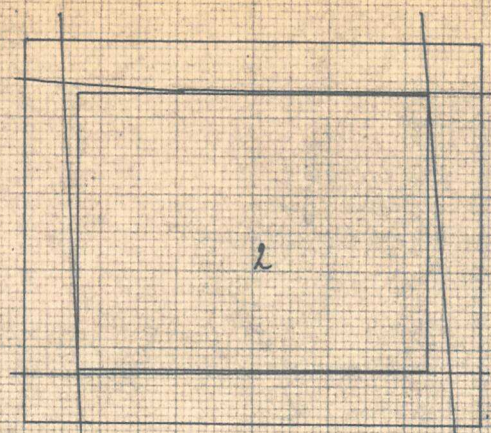
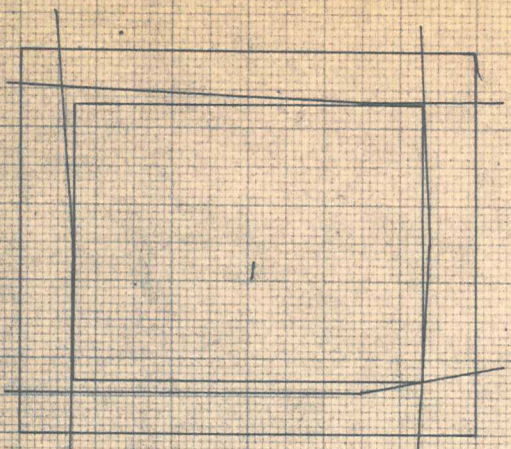
SERIE 2.



D 10 - 1609H.

$\frac{MN1}{m81}$  1

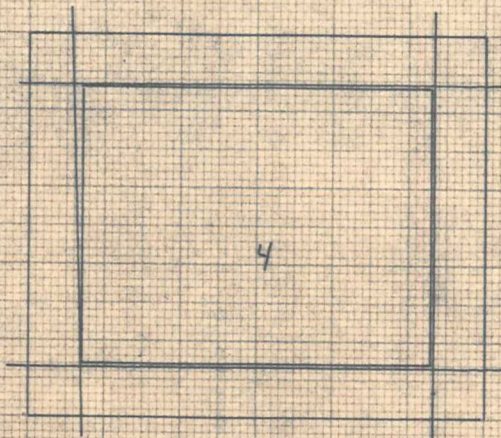
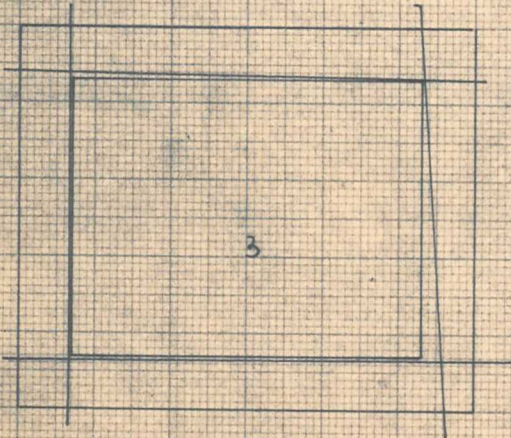
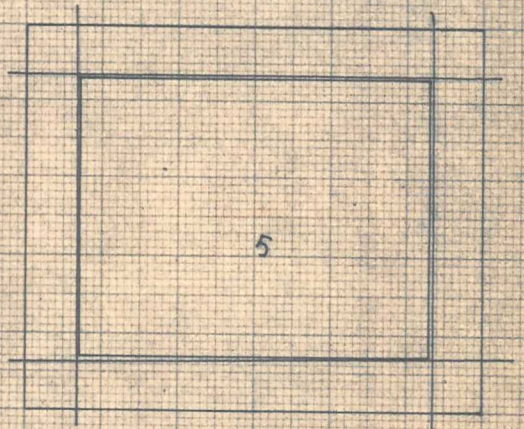
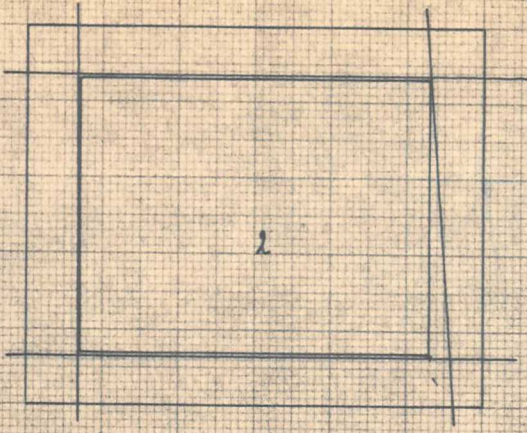
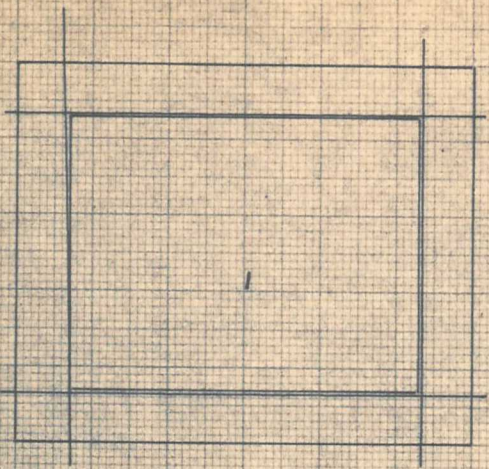
SERIE 3.



$\frac{MN1}{m81}$  1

D 10 - 1609H.

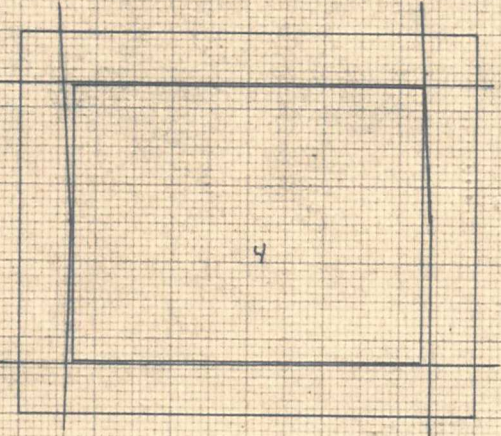
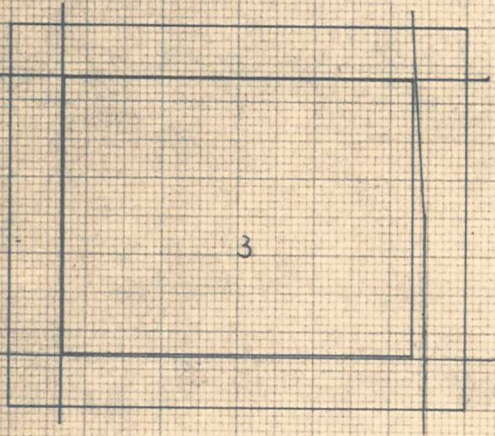
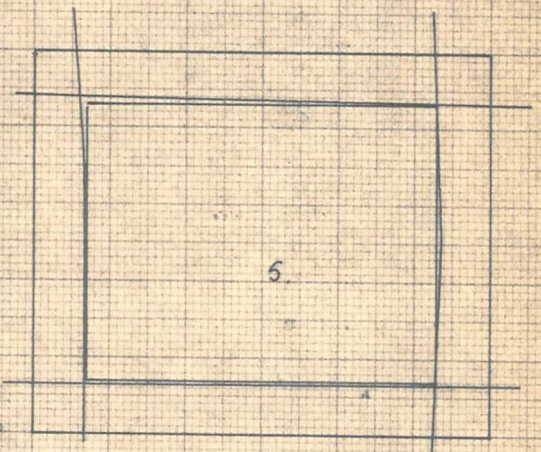
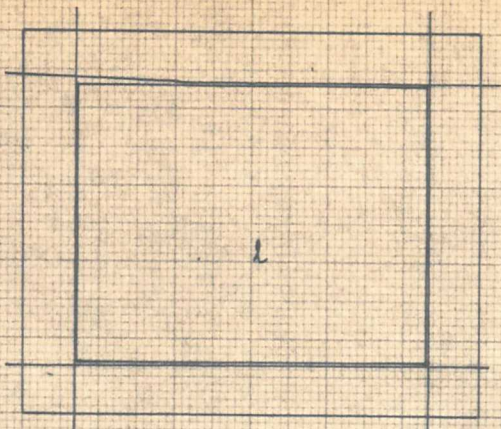
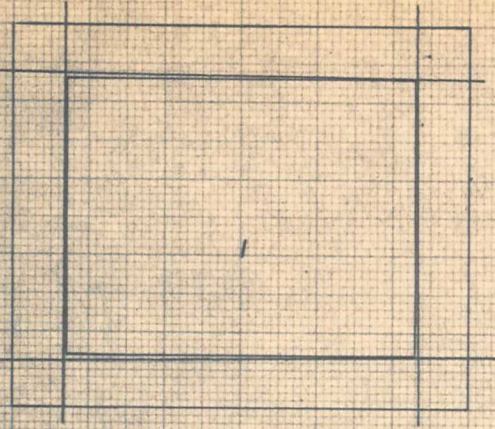
SERIE 4.



D 10-160 qH

$\frac{MN1}{m\theta 1}$  3

SERIE 5



$\frac{MN1}{m\theta 1}$  4

D 10-160 qH

SERIE 6